

Stormwater Management Plan
St. Juan Diego Pilgrim House
City of La Crosse, Wisconsin

Prepared For:
Shrine of Our Lady of Guadalupe,
Inc.
5250 Justin Road, PO 1237
La Crosse, WI 54601

Prepared By:
Vierbicher
999 Fourier Drive, Suite 201
Madison, Wisconsin 53717

Prepared On:
September 13, 2024
Project #200196

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vierbicher
planners | engineers | advisors



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Narrative

NARRATIVE

1.1 Introduction

The project site is located at 6025 County Road MM in the City of La Crosse (NE ¼ of the NW ¼ of Section 26 Town 15N Range 7W). The site is east of Mormon Creek and bound by County Road MM on the west. The existing site is home to the Shrine of Our Lady of Guadalupe Church with associated drive lanes, sidewalks, and utilities. The existing parcel contains 74.7 acres but the project site only includes 0.88 acres. The church is proposing a building addition to create a 6-story retreat center that will replace some of the existing pavement areas.

Existing drainage patterns will be maintained for this project. The site drains internally to private storm sewer which flow to three small detention ponds near the entrance of the site. The detention ponds outlet to a culvert under CTH MM with all site runoff eventually making its way to Mormon Creek. There are no floodplains located on the site. There are no wetland indicators present on the site per DNR's Surface Water Data Viewer.

The site is required to meet City of La Crosse post construction stormwater management requirements for new development as requested by the City. These requirements include sediment control, runoff rate control, and infiltration. These requirements will be met to the maximum extent practicable with a proposed underground detention system.

1.2 Soils Description

The U.S. Department of Agriculture (USDA), Natural Resources Conservation Service (NRCS) online Web Soil Survey, indicates the proposed project site primarily contains Churchtown Silt Load (116E2), Hydrologic Soil Group "B".

Chosen Valley Testing (CVT) completed a soils evaluation May 14, 2021. This report is located in section 3.2. In it, CVT concludes the underlying soils are dominated by loessial (wind deposited) silts and clays. To avoid settlement and collapse of the loessial soils, infiltration of runoff must not be permitted.

1.3 Design Criteria

| Stormwater Management Requirements | |
|------------------------------------|--|
| Design Frequency | 2 and 10-Year, 24-hour storm events using the MSE3 or MSE4 NRCS Rainfall Distribution |
| Rainfall Data | 3.00, 4.44-inch/24-hour |
| Curve Number | Pre-Developed Maximum: Woodland 55 Post-Developed: Impervious 98, Grass/Landscape 61 |
| Peak Rate Control | Meet the pre-developed runoff rate for the 2 and 10-year, 24-hour events |
| Sediment Control | 80% Reduction, as compared to no controls |
| Infiltration | Infiltrate 75% of the pre-developed volume of average annual rainfall |



1.4 Summary of Results

Peak Runoff Rate Control

The site must maintain the pre-developed peak runoff rate control for the 2 and 10-year, 24-hour events. This requirement is met with an underground detention system.

The runoff from the site is routed to an underground detention system and discharges to an on-site wooded ravine. Because the project is located on a hill, fringe area within the disturbed limits of the site will not be able to be detained. Because of this, the peak runoff under proposed conditions is slightly higher than the peak runoff under predeveloped conditions. Undetained fringe area consists of pervious grass and landscape area and utility pads. All other impervious surfaces, including driveways, parking, and roof, are detained. The peak runoff rate control calculations are in section 4 of this report. The following two tables summarize routing through the detention facility.

Run-on into the detention facility has been taken into account in the modeling. The run-on consists of 0.15 acre of nearby roof and landscape area.

The site must maintain the pre-developed peak runoff rate control for the 2, and 10-year, 24-hour events. The site meets these requirements to the maximum extent practicable. The table below summarizes the peak runoff rate control calculations for the development.

| Storm Frequency (Year) | Pre-Developed (0.99 acres) CFS | No Controls Post-Developed (0.99 acres) CFS | Controls Post-Developed (0.99 acres) CFS | Controls Post-Developed, From Detention Only (0.99 acres) CFS |
|------------------------|--------------------------------|---|--|---|
| 2 | 0.15 | 2.67 | 0.16 | 0.06 |
| 10 | 0.85 | 4.50 | 0.90 | 0.78 |

Sediment Control

The site will be required to reduce TSS from the site by eighty percent (80%), as compared to no controls. The table below summarizes the results of the TSS modeling.

| No Controls (lbs) | After Stormwater w/ Controls (lbs) | TSS Removed from Site (lbs) | % Reduction |
|-------------------|------------------------------------|-----------------------------|-------------|
| 280.4 | 48.01 | 232.39 | 82.88% |

The site is required to meet 80% TSS reduction from a no control standpoint. The stormwater management facilities have been designed to treat runoff and will achieve an 82.88% TSS removal rate. TSS was modeled with WinSLAMM v. 10.5 and calculations are within section 5 of this report.

Infiltration

The site is considered to have moderate imperviousness and is required to infiltrate 75% of the pre-developed infiltration volume in the post-developed condition for the average annual rainfall. However, due to the nature of the project, the geotechnical report states that infiltration must not be permitted in order to avoid settlement and collapse of the loessial soils. Therefore, no infiltration is designed for the site.



Erosion Control

The project is anticipated to begin November 2024 and will be restored by Spring 2026. Erosion control measures will consist of a double row of silt fence downstream of all construction activity, a tracking pad located at the entrance/exit of the project site, and erosion mat over slopes 4:1 or greater. All erosion control measures will be in place prior to land disturbing activities.

1.5 Conclusions

All stormwater management design criteria that were required by the City and State up are met by an underground detention system. The site should be exempt from infiltration per recommendation in the geotechnical report.

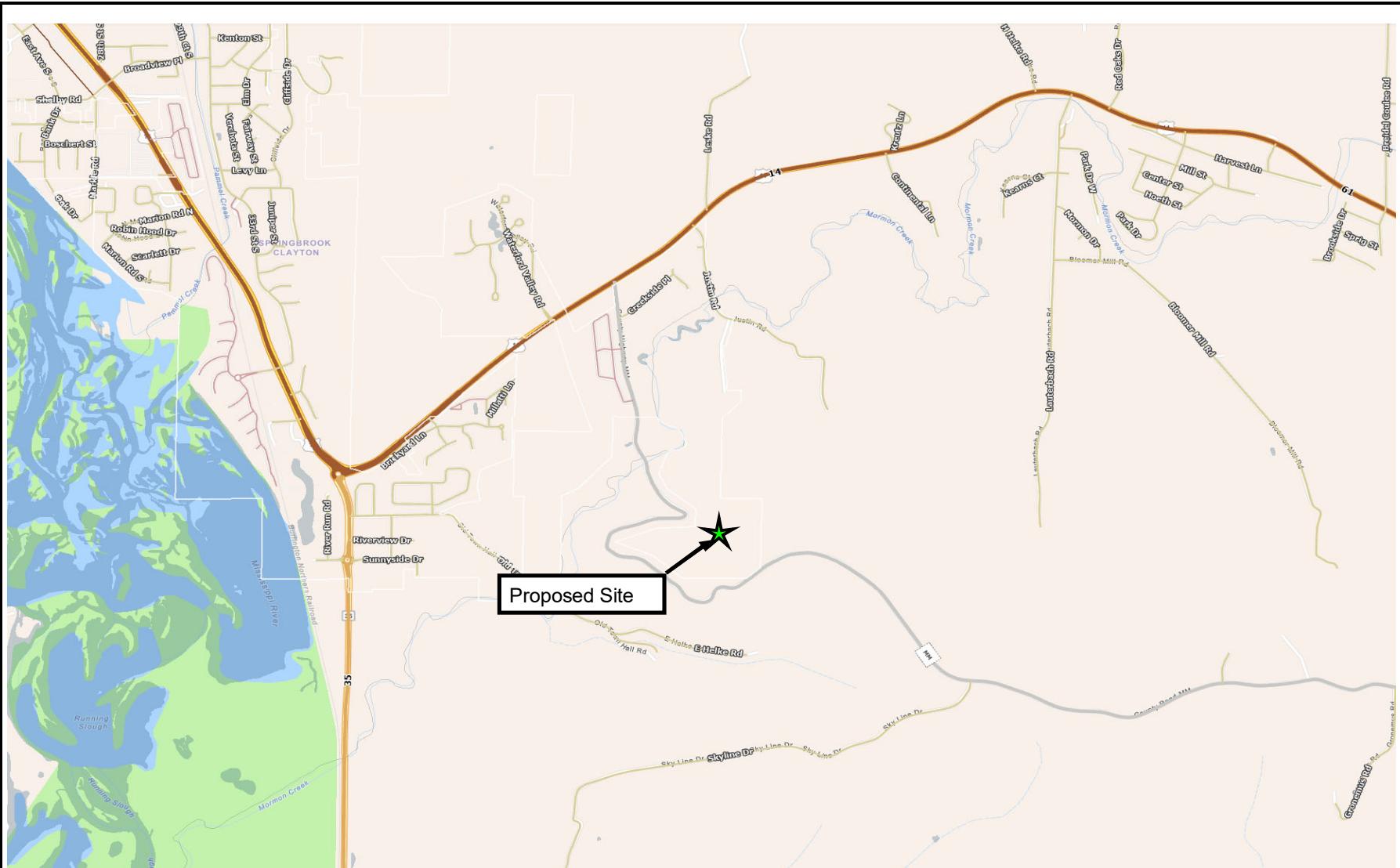
1.6 Permits

The following is a list of anticipated stormwater permits or reviews that have been or will be applied for:

- City of La Crosse Stormwater Permit
- La Crosse Sewer Service Area Water Quality Management Plan Sewer Service Extensions & Conformance Review.

Maps

2.1 Location Map



Source: La Crosse County Interactive Map Viewer



Map 2.1: Location Map

Project Name: SOLOG La Crosse Retreat Center
Project Location: 5250 Justin Rd, La Crosse, WI 54601

2.2 Aerial Map



Source: La Crosse County Interactive Map Viewer



Map 2.2: Aerial Map

Project Name: SOLOG La Crosse Retreat Center
Project Location: 5250 Justin Rd, La Crosse, WI 54601

2.3 USGS Quad Map



Source: La Crosse County Interactive Map Viewer



Map 2.2: Aerial Map

Project Name: SOLOG La Crosse Retreat Center
Project Location: 5250 Justin Rd, La Crosse, WI 54601

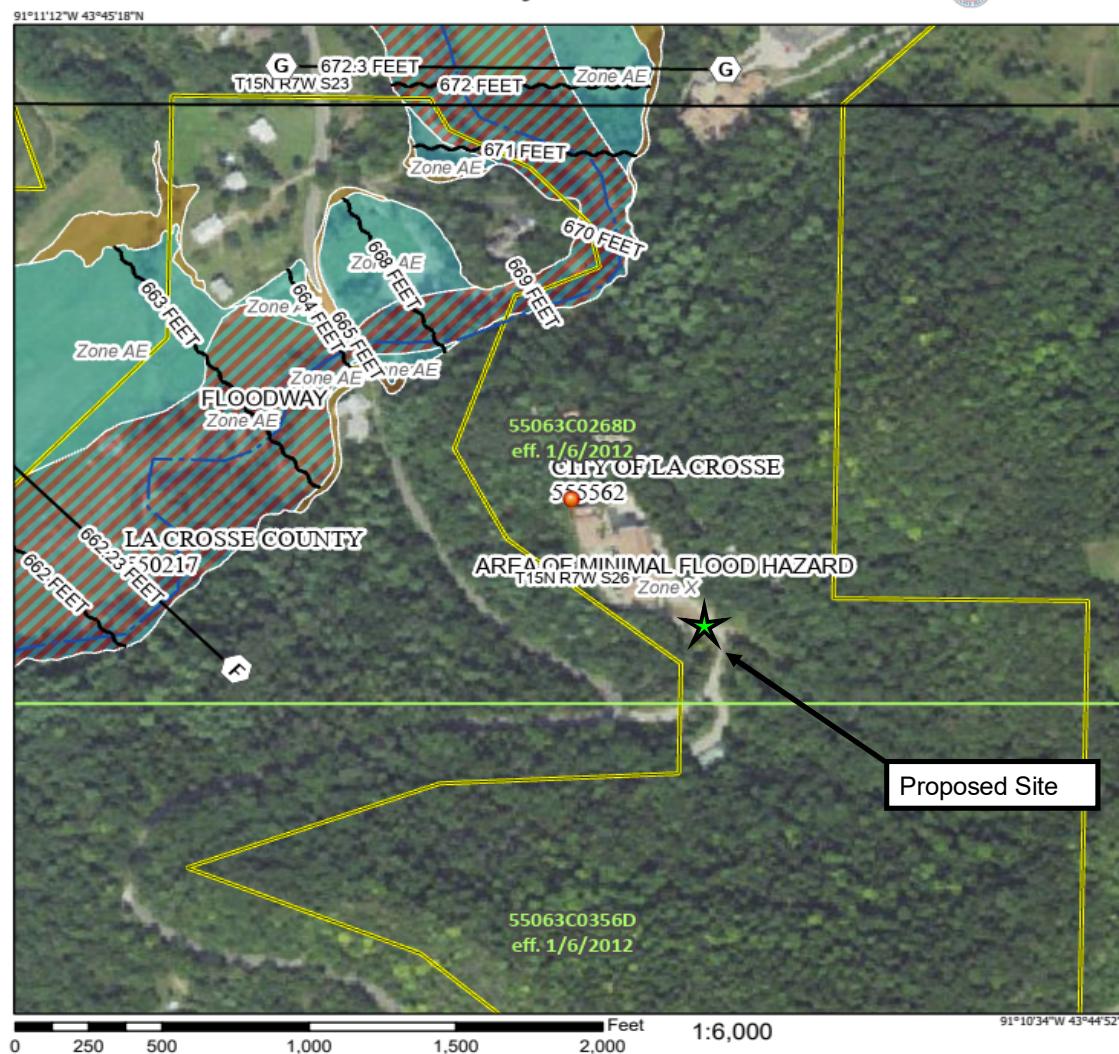
2.4 FEMA Map

National Flood Hazard Layer FIRMette



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



SPECIAL FLOOD HAZARD AREAS

- Without Base Flood Elevation (BFE)
- Zone A, V, A99
- With BFE or Depth Zone AE, AO, AH, VE, AR
- Regulatory Floodway

OTHER AREAS OF FLOOD HAZARD

- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
- Future Conditions 1% Annual Chance Flood Hazard Zone X
- Area with Reduced Flood Risk due to Levee, See Notes, Zone X
- Area with Flood Risk due to Levee Zone D

NO SCREEN Area of Minimal Flood Hazard Zone X
Effective LOMRs

OTHER AREAS Area of Undetermined Flood Hazard Zone D

GENERAL STRUCTURES

- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

OTHER FEATURES

- 29.2 Cross Sections with 1% Annual Chance
- 17.5 Water Surface Elevation
- Coastal Transect
- Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

MAP PANELS

- Digital Data Available
- No Digital Data Available
- Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/18/2024 at 12:28 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodeled areas cannot be used for regulatory purposes.

Source: FEMA Flood Map



Map 2.4: FEMA Flood Map

Project Name: SOLOG La Crosse Retreat Center
 Project Location: 5250 Justin Rd, La Crosse, WI 54601

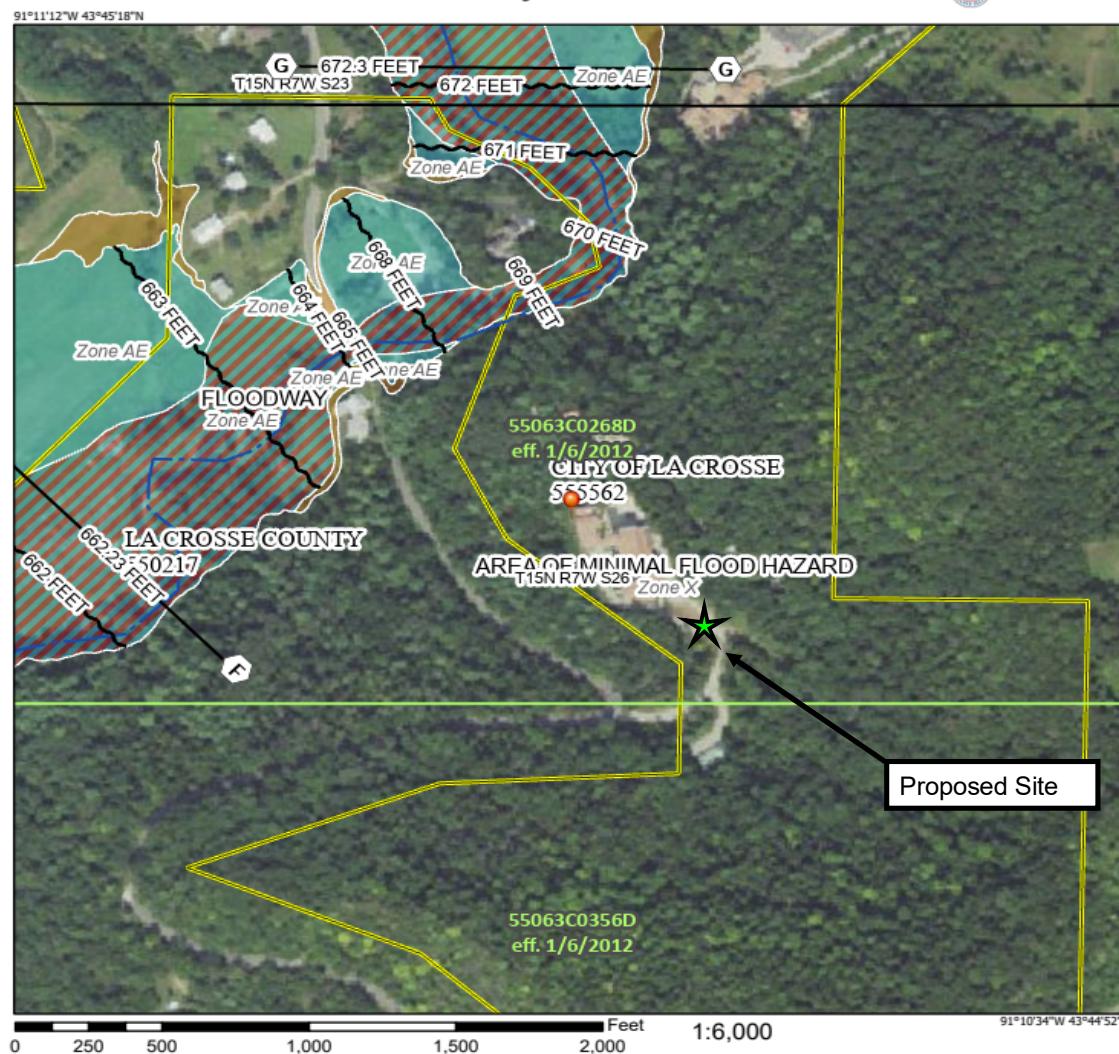
2.5 Wetland Indicators Map

National Flood Hazard Layer FIRMette



Legend

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SPECIAL FLOOD HAZARD AREAS

- Without Base Flood Elevation (BFE) Zone A, V, A99
- With BFE or Depth Zone AE, AO, AH, VE, AR
- Regulatory Floodway

OTHER AREAS OF FLOOD HAZARD

- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
- Future Conditions 1% Annual Chance Flood Hazard Zone X
- Area with Reduced Flood Risk due to Levee, See Notes, Zone X
- Area with Flood Risk due to Levee Zone D

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Effective LOMRs

OTHER AREAS Area of Undetermined Flood Hazard Zone D

GENERAL STRUCTURES

- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

OTHER FEATURES

- 29.2 Cross Sections with 1% Annual Chance
- 17.5 Water Surface Elevation
- Coastal Transect
- Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
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Source: FEMA Flood Map

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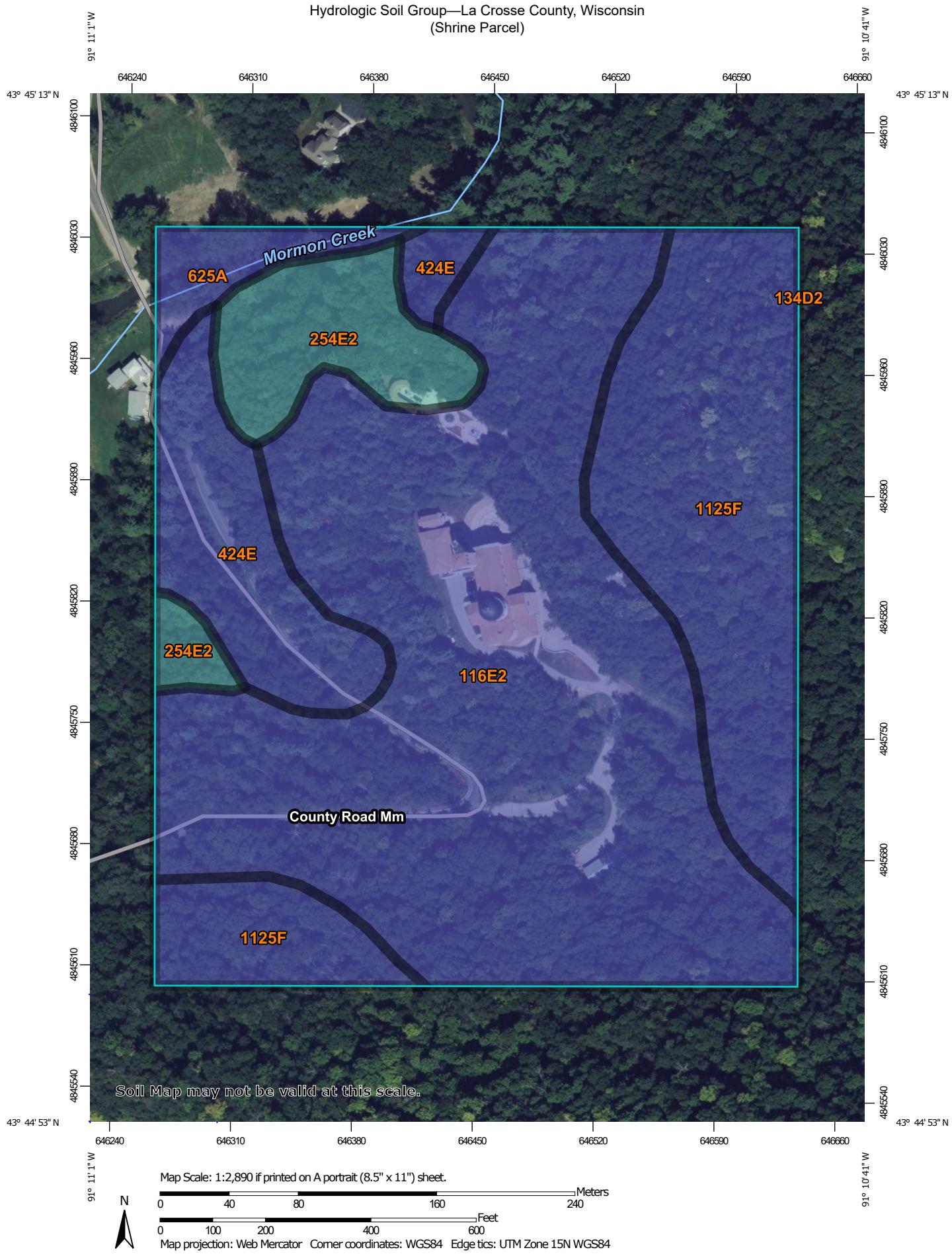
Map 2.4: FEMA Flood Map

Project Name: SOLOG La Crosse Retreat Center
 Project Location: 5250 Justin Rd, La Crosse, WI 54601

Soils Information

3.1 Soils Map

Hydrologic Soil Group—La Crosse County, Wisconsin
(Shrine Parcel)



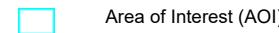
Natural Resources
Conservation Service

Web Soil Survey
National Cooperative Soil Survey

5/29/2024
Page 1 of 4

MAP LEGEND

Area of Interest (AOI)



Soils

Soil Rating Polygons

| | |
|--|----------------------------|
| | A |
| | A/D |
| | B |
| | B/D |
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Soil Rating Lines

| | |
|--|----------------------------|
| | A |
| | A/D |
| | B |
| | B/D |
| | C |
| | C/D |
| | D |
| | Not rated or not available |

Soil Rating Points

| | |
|--|-----|
| | A |
| | A/D |
| | B |
| | B/D |

C

C/D

D

Not rated or not available

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: La Crosse County, Wisconsin

Survey Area Data: Version 22, Sep 8, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 31, 2020—Sep 2, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

| Map unit symbol | Map unit name | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| 116E2 | Churchtown silt loam, 20 to 30 percent slopes, moderately eroded | B | 22.6 | 55.9% |
| 134D2 | Lamoille silt loam, 12 to 20 percent slopes, moderately eroded | C | 0.0 | 0.0% |
| 254E2 | Norden silt loam, 20 to 30 percent slopes, moderately eroded | C | 3.1 | 7.7% |
| 424E | Merit silt loam, 20 to 45 percent slopes | B | 4.0 | 9.8% |
| 625A | Arenzville silt loam, channeled, 0 to 2 percent slopes, occasionally flooded | B | 1.1 | 2.8% |
| 1125F | Dorerton, very stony-Elbaville complex, 30 to 60 percent slopes | B | 9.6 | 23.8% |
| Totals for Area of Interest | | | 40.5 | 100.0% |

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

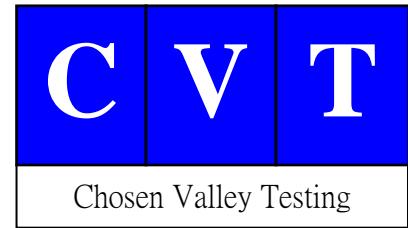
Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

3.2 Geotechnical Report



Design Phase Geotechnical Report:

Proposed Retreat Center
Shrine of Our Lady of Guadalupe
CTH MM
La Crosse, Wisconsin

Prepared for:

Shrine of Our Lady of Guadalupe
c/o Thomas Stroka
Duncan G. Stroik Architects LLC

July 28 14, 2021
17665.20.WIL

I hereby certify that this report was prepared by me or under my direct supervision, and that I am a duly registered engineer under the laws of the State of Wisconsin.

A handwritten signature in black ink, appearing to read "Colby T. Verdegan".

Colby T. Verdegan, PE
Geotechnical Engineer
Registration Number 36326
Date: July 28, 2021



Chosen Valley Testing, Inc.

Geotechnical Engineering and Testing • 1019 2nd Ave. SW, Onalaska, WI 54650 • Phone (608) 782-5505 • Fax (608) 785-2818
E-mail: lacrosse@chosenvalleytesting.com

Mr. Thomas Stroka
Duncan G. Stroik Architect LLC
218 West Washington Street, Suite 1200
South Bend, IN 46601
thomas@stroik.com

July 28, 2021

**Re: Geotechnical Exploration and Evaluation
Proposed Retreat Center
Our Lady of Guadalupe
CTH MM
La Crosse, Wisconsin
CVT Proposal Number: 17665.20.WIL**

Mr. Stroka:

As requested, we have completed the additional exploration for the Proposed Retreat Center for the Shrine of Our Lady of Guadalupe on CTH MM in La Crosse, Wisconsin. We have updated our previously issued report to include the new information as well as to incorporate comments from the prior report. To expedite planning, the preliminary logs were issued in advance. If you have any questions about our report, please feel free to contact us at (608) 782-5505.

Sincerely,
Chosen Valley Testing, Inc.



Frederick Schuster, PE
Geotechnical Engineer



Colby T. Verdegan, PE
Sr. Geotechnical/Materials Engineer

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**Design Phase Geotechnical Evaluation
Proposed Retreat Center
Our Lady of Guadalupe
CTH MM
La Crosse, Wisconsin**

CVT Project Number: 17665.20.WIL
Date: July 28, 2021

A. Introduction

The intent of this report is to present our results to the client in the same logical sequence that led us to arrive at the opinions and recommendations expressed. Since our services must often be completed before the design, assumptions are sometimes needed to prepare a proper evaluation and to analyze the data. A complete and thorough review of this entire document, including the assumptions and the appendices, should be undertaken immediately upon receipt.

A.1. Purpose

This report was prepared for proposed Retreat Center for the Shrine of Our Lady of Guadalupe on CTH MM in La Crosse, Wisconsin. Our services were authorized by the Diocese of La Crosse. This report replaces our report issued May 14, 2021, and updated the report to include the results of the additional borings and as well as additional design information.

A.2. Scope

To obtain data for analysis, we were initially authorized to perform six standard penetration test borings and two manual borings. The machine borings were drilled to depths of about 35 to 50 feet while the manual borings were performed to depths of about 15 feet. After these borings were completed, four additional borings were authorized to be drilled to depths of 100 feet or at least 30 feet into bedrock. Our scope consisted of providing our opinions and recommendations for the various geotechnical aspects of the project per the RFP.

A.3. Boring Locations and Elevations

The general boring locations were indicated to Chosen Valley Testing on site plans provided by Duncan G. Stroik Architect LLC within the RFP. Some locations were offset due to site access and utility location constraints – such as Boring B-1A which was shifted because of overhead interference from trees and B-3A because of the proximity of a gas line and other utilities. The ***Boring Location Sketch*** in the Appendix shows the approximate boring locations as drilled. The borings drilled earlier in 2021 are labelled S-1 through S-8, while the borings added in July are labelled B-1A through B-4A. The estimated relative locations of prior borings in or near the improvements by CVT are also indicated and are labelled A, D, E, B-3 and B-5. Copies of Logs sheets from the prior borings are also included in the Appendix and are also reference in discussions.

Ground surface elevations were estimated using a laser level. Finished floor of the existing building at the southeast door was used as a benchmark, and was understood to be at elevation 806.5 feet.

A.4. Geologic Background

A geotechnical report is based on subsurface data collected for the specific structure or problem. Available geologic data from the region can help interpretation of the data and is briefly summarized in this section.

Geologic maps and our prior exploration suggest that the natural soils in the area are primarily dominated by loessial (wind deposited) silts and silty clays with some colluvial (gravity deposited) mixtures of clays, silts, sands and gravels, overlying highly weather residual materials derived from the bedrock. Significant earthwork is occurred across the much of the site associated with the construction of the existing Shrine and Rectory. This consisted primarily of removing the loessial soils from the support zone of the buildings and replacing it with compacted limestone screenings, as well as necessary grading for paving and utilities.

Geologic maps indicate underlying bedrock is from the Prairie du Chien Group. From a review of well logs in the area, the bedrock is mostly likely from the bottom of Oneota Formation (the Stockton Hill Member) of the Prairie du Chien Group. This material is rather variable and tends to be of dolomitic sandstone, silty and sandy dolomite and dolomite. This is underlain by the much more uniform Jordan Sandstone Formation. From the well logs, the contact between the bottom of the Oneota and the top of the Jordan was crudely interpolated as being near elevation 740 feet.

B. Subsurface Data

Methods: Most of the borings were performed using penetration test procedures (Method of Test D1586 of the American Society for Testing and Materials). This procedure allows for the extraction of intact soil specimen from deep in the ground. With this method, a hollow-stem auger is drilled to the desired sampling depth. A 2-inch OD sampling tube is then screwed onto the end of a sampling rod, inserted through the hole in the auger's tip, and then driven into the soil with a 140-pound hammer dropped repeatedly from a height of 30 inches above the sampling rod. The sampler is driven 18-inches into the soil unless the material is too hard. The samples are generally taken at 2½ to 5-foot intervals. The core of soil obtained is classified and logged by the driller and a representative portion is then sealed in a jar and delivered to the soils engineer for review.

The manual borings were drilled with a 3-inch bucket auger. Prior to sampling a manual DCP was used to obtain strength data, and the resulting values were converted to estimated N-values.

B.1. Stratification

The surficial materials at most locations consisted of paving materials.

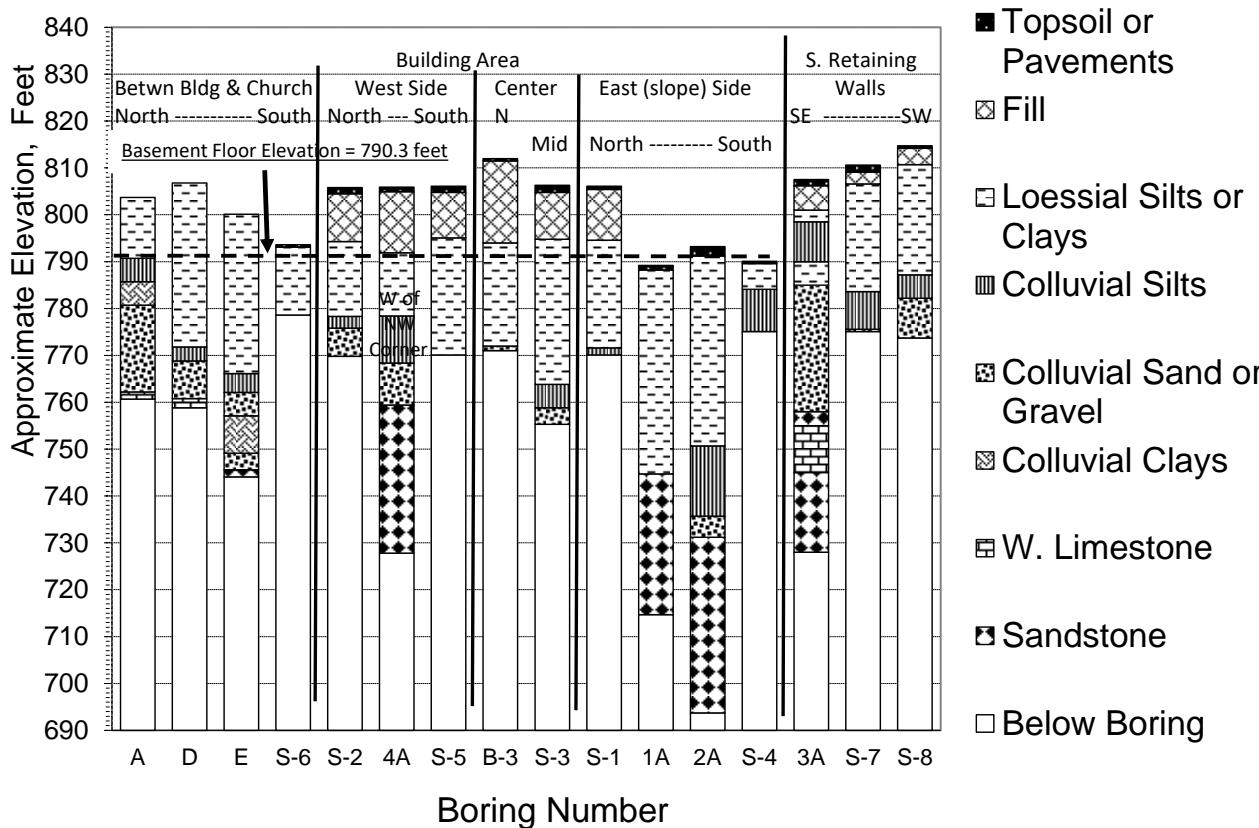
As expected from the site history, the uppermost soils at most of the boring locations drilled in 2021 consisted of fill materials which extended to depths ranging from about 5 to 18 feet.

The underlying soils were then dominated by loessial silts and clays. As might be expected, the bottom of the loessial soils appeared to become lower progressing downhill to the west, but also somewhat towards the south. The boring closest to the planned southeast building corner terminated in these soils at about 36 feet. The southwest building area boring encountered the loessial materials to a depth of about 44 ½ feet.

A couple borings terminated in the loessial soils. Most extended deeper and penetrated into firmer colluvial soils consist of silts, clay, sands, silty sand and gravel.

The four most recent borings, B-1A through B-4A, were extended deeper to penetrate into the underlying rock materials. These borings encountered materials judged to be bedrock at depths of about 45 to 62 feet. The rock materials consisted primarily of sandstone. The uppermost rock in the boring drilled for the retaining wall, south of the Retreat Center, met about 10 feet of limestone near the top of the bedrock profile.

For the readers convenience, the boring data has been summarized on the cross-section following this paragraph. The results of the prior borings referenced have been including for illustration purposes and terminated in or on materials judged to be bedrock. Most of prior borings were done largely before any grading, in which case the loessial soils were partly or completely replaced by fill. The reader is referred to the Log of Boring sheets in the Appendix for location specific information. The ground surface elevations at the older borings are shown at estimated elevations, relative to the datum for this project.



B.2. Penetration Test Results

The number of blows needed for the hammer to advance the penetration test sampler is an indicator of soil characteristics. The number of blows to advance the sampler 1 foot is called the penetration resistance or "N"-value. The results tend to be more meaningful for natural mineral soils, than for fill soils. In fill soils, compaction tests are more meaningful.

Penetration resistance values (N-values) of 2 to 21 Blows per Foot (BPF) were encountered in the fill

materials, indicating they were somewhat variable and possibly at times uncompacted. The loessial soils returned values of 2 to 15 BPF, indicating they were very soft to rather stiff, but mostly rather soft and potentially collapsible.

The colluvial silts and clays returned values of 7 to 32 BPF with most values indicating relatively stiff or dense materials. The colluvial or residual sands and gravels had values ranging from 8 BPF to 5 blows for 5 inches of penetration indicating they were loose to very dense but mostly medium dense to dense.

Penetration test values in the weathered rock materials ranged from about 50 blows for 9 inches of penetration to 50 blows for 0 inches of penetration.

A key to the descriptors used to qualify the relative density of soil (such as *soft*, *stiff*, *loose*, and *dense*) can be found on the Legend to Soil Description in the Appendix.

B.4. Groundwater Data

During the drilling operation, the drillers may note the presence of moisture on the sampling instrument, in the cuttings, or within the boreholes. These observations are recorded on the boring logs. The water level may vary with weather; time of year and other factors and the presence or absence of water during the drilling is subject to interpretation and is not always conclusive.

Water was not observed in all any of the borings and none of the samples appeared to be overly wet or saturated. Water is often observed seeping along the surface of bedrock materials but was not noted. A piezometer installed at the was dry when installed, and still dry when checked a week later.

C. Design Data

Because each structure has a different loading configuration and intensity, different grades, and different structural or performance tolerances, the results of a geotechnical exploration will mean different things for different facilities. If the design of the facility changes, the soils engineer should be contacted to discuss the possible implications of the changes. Without a chance to review such changes, the recommendations of the soils engineer may no longer be valid or appropriate.

Our current understanding is that the new facility is planned to be about 6 stories tall with an additional story below grade. The building perimeter is to be constructed primarily of structural masonry and concrete with post-tensioned concrete slabs. Maximum structural loads were estimated to be on the order of 660 kips per column. Maximum wall loads were estimated to be about 43 kips per foot. Our understanding is the 7 ½-inch diameter micro-piles are planned and would have typical capacities on the order of 100 kips.

Lowest level slab elevation is indicated to be at about elevation 790.3 feet. This is about 16 feet below existing grades.

Retaining wall are planned at the perimeter of the site. Maximum exposed wall heights are expected to be on the order of 16 feet.

Surface water drainage is planned to be temporarily storage in below grade vault type structures between the existing building and the addition. The water will presumably be drained away by pumping or gravity.

D. Analysis

D.1. Building and Retaining Wall Foundation Support

D.1.a. General Support: Based on the data, the soils at bearing conditions for the structure are expected to be dominated by highly compressible and potentially collapsible loessial soils. Allowable bearing pressures on these soils are normally limited to 1,500 psf. Use of such low pressures is not feasible and does not significant impact potential for collapse. Under the circumstances, we are of the opinion that all foundations will need to be supported on/in the underlying bedrock.

Allowable bearing pressures for footings on the bedrock materials are commonly limited to about 20 to 40 tons per square foot and are complicated by depositional and erosional variations in the rock. Based on the information collected for the prior structures, the rock materials appear to be at least 20 feet and potentially 50 feet or more below low planned slab grades, so spread footings are not feasible and deep foundation options would be needed. Due to the nature of the existing structure and site conditions, driven piling and other options with significant vibrations (including rammed aggregates) are not recommended.

D.1.b. Support Options: The bedrock materials encountered in our prior exploration were rather variable, appeared to be sloping rather sharply, and are believed to be near a stratification change in the geology. For these reasons, if drilled piers were used, they would need to be socketed to provide added assurance against changing support issues at depth – unless additional probing is done at virtually all location to confirm support conditions.

Because of the impracticalities of implementing investigative assurances below drilled piers, we are of the opinion that micropiles are likely the most feasible alternative for all columns bearing locations, at the perimeter foundations and retaining walls. These can be more easily deepened than driller piers and disturbance caused by deepening should be limited. Micro piles have a much smaller diameter in relation to their expected length than drilled piers. The design will need to consider the limited lateral support afforded by the loessial soils. The bottom of the micropiles should be socketed into the weather sandstone encountered below the site. Negative skin friction is not a significant concern and, in our opinion, does not need to be considered.

The anticipated foundation loads are not particularly large in relation to expected capacities derived from bonding between the micropile system and the bedrock materials. With the present information, we would anticipate such piling could plausibly attained the desired capacities at rather short embedments into the rock. With the present information, we would anticipate all such piling extending at least 10 feet into the rock. The micropiles should be subjected to load testing during construction.

D.2. Slab Areas

D.2.a. Pile Support to Address Collapse Potential: Due to the long-term potential for collapse, slabs areas would also ideally be supported on deep foundations. Whereas the loessial soils were removed from below the existing structures, those slabs were laid directly on the replacement limestone screening fill or a layer of sand over the screenings.

D.2.b. Alternative Slab Support and Surficial Protection of Loessial Soils: The consequences of slab settlement is much less than that of foundations, to the extent that “floating” the slabs over these soils could be considered depending on the function of the lower-level areas. This being said, if the slab areas are not supported on deep foundations (and even if they are), precautionary grading at the surface is recommended to prevent rutting and disturbance of the sensitive loessial soils when exposed to weather and traffic. To this end, we would recommend removing the loessial soils to a depth of at least 2 feet below bottom of slab elevation. A high strength geosynthetic or geogrid should then be laid, followed a protective layer of sand or aggregate. If utilities will be placed below the slab, we suggest increasing the depth of the layer as needed so that the utility work will be accomplished above the geosynthetic materials.

D.2.c. Filling and Compaction: For ease in compaction, the protective layer is recommended to consist primarily of gravelly sand having less than 12% particles passing a #200 sieve or possibly a thick layer of WisDOT dense graded base over sand. As noted before, the fill beneath the existing structures consists primarily of limestone screenings. Such materials could plausibly be used as protective fill but would have to be reviewed. The fill should be compacted to at least 95% of its standard Proctor density.

D.3.Additional Design and Grading Considerations

D.3.a. Frost Protection: The dominant silty soils are highly frost susceptible. We recommend placing foundations for heated structures at least 48 inches below the exposed ground surface for frost protection. For unheated structures, we recommend 60 inches of frost cover. Surface water should be directed away from the foundations to limit the potential for frost action.

D.3.b. Lateral Support/Resistance: We recommend using clean sands or gravels having less than 10% particles passing a #200 sieve as fill against below-grade walls. All backfill should be compacted to at least 95% of its maximum standard Proctor density (ASTM D 698). The sand should be capped with a layer of clay topsoil or pavement and sloped away from foundations to prevent water from infiltrating and collecting behind walls. The table below includes recommended support values for clean sands.

| Poorly Graded Sands (SP) 95% standard Proctor density | |
|---|------|
| Internal Friction Angle (degrees) | 34 |
| Cohesion (psf) | 0 |
| Coefficient of Friction between Concrete and Soil | 0.50 |
| Moist Unit Weight (pcf) | 120 |

Some of the basement walls or retention systems will presumably be formed against existing loessial soils or silty fill. The table below includes estimated strength parameter for the silty materials.

| Silt | |
|-----------------------------------|-----|
| Internal Friction Angle (degrees) | 22 |
| Cohesion (psf) | 0 |
| Moist Unit Weight (pcf) | 110 |

Some tendons or anchors retention systems may extend into the compacted limestone screening fill below the existing structures. If such materials are detected during installation, the following parameters have been estimated for those materials.

| Compacted Limestone Screening | |
|-----------------------------------|-----|
| Internal Friction Angle (degrees) | 30 |
| Cohesion (psf) | 0 |
| Moist Unit Weight (pcf) | 130 |

D.3.c. Stormwater/Infiltration

Due to the collapse potential of the loessial soils, infiltration of ground water on the site must be avoided, lest it result in collapse and settlement. Our understanding is that the final design calls for stormwater to be stored below grade in a fashion which will prevent infiltration. During construction, the surface grades should be protected in a fashion which similarly limits localized infiltration.

E. General Recommendations

E.1. Excavation

The existing loessial soils and silty fill are extremely sensitive soil types and will become very unstable and rut under traffic or if exposed to traffic. If that occurs, the softened and rutted soils will likely have to be removed. Soil removals will ideally be done using a backhoe with a smooth lipped buck, and back-casting excavated soils into trucks for removal. Replacement fill will ideally be pushed ahead of dozers, so that traffic including compactors doesn't operate directly on the surface of the silty soils and encourage instability.

E.2. Sideslopes

The contractor will be required to slope or shore the excavations as needed to meet OSHA requirements for safety. The dominant soils will likely classify as Type C soils as defined by OSHA. Trench boxes or other stabilization methods may be necessary when excavating close to property limits or structures.

E.3. Groundwater/Dewatering

Ground water is not expected to be encountered in the excavations, though the sloping terrain and existing fill and construction is plausibly conducive to perched water. Such moisture would likely be of nominal volume and could likely be removed with sumps, though we believe such moisture would more likely consist of pockets of saturated soils.

E.4. Reuse of On-site Materials

The excavated soils are not expected to be reusable to any significant degree and site limits would likely prevent on-site storage of reserve materials.

E.5. Filling and Compacting

Fill should be placed in lifts adjusted to the compactor being used and the material being compacted. We recommend limiting lifts to no more than 1/2-foot – assuming most fill will have to be placed by small equipment.

E.6. Cold Weather Construction

If earthwork occurs during freezing temperatures, good winter construction practices should be used. Frozen fill should not be used and fill should not be placed on frozen ground. Slab areas should be completely thawed prior to placing any concrete.

E.7. Construction Testing and Documentation

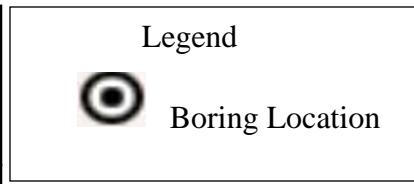
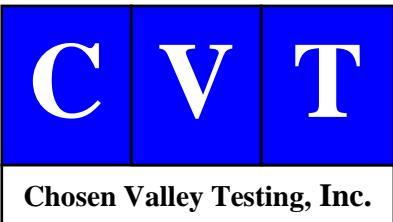
Excavations, grading and deep foundation installations should be evaluated and documented by geotechnical personnel. Proposed engineered fill should be evaluated for conformance to the project gradation recommendations before its use and should be tested for compaction during construction. If the construction proceeds during periods of freezing weather, full-time testing and observations should be considered to help confirm that imported fill is thawed prior to and during compaction, that all snow/ice has been removed before placement of the fill, and that other materials affected by temperatures are being properly protected.

Although our firm offers testing services relating to civil and structural components of the building (such as concrete testing, reinforcement observations, etc.) specification of such services is beyond our work scope and the designer should be consulted as to such requirements.

F. Level of Care

The services provided for this project have been conducted in a manner consistent with that level of care and skill ordinarily exercised by members of the profession currently practicing in this area, under similar budget and time constraints. This is our professional responsibility. No other warranty, expressed or implied, is made.

Appendix

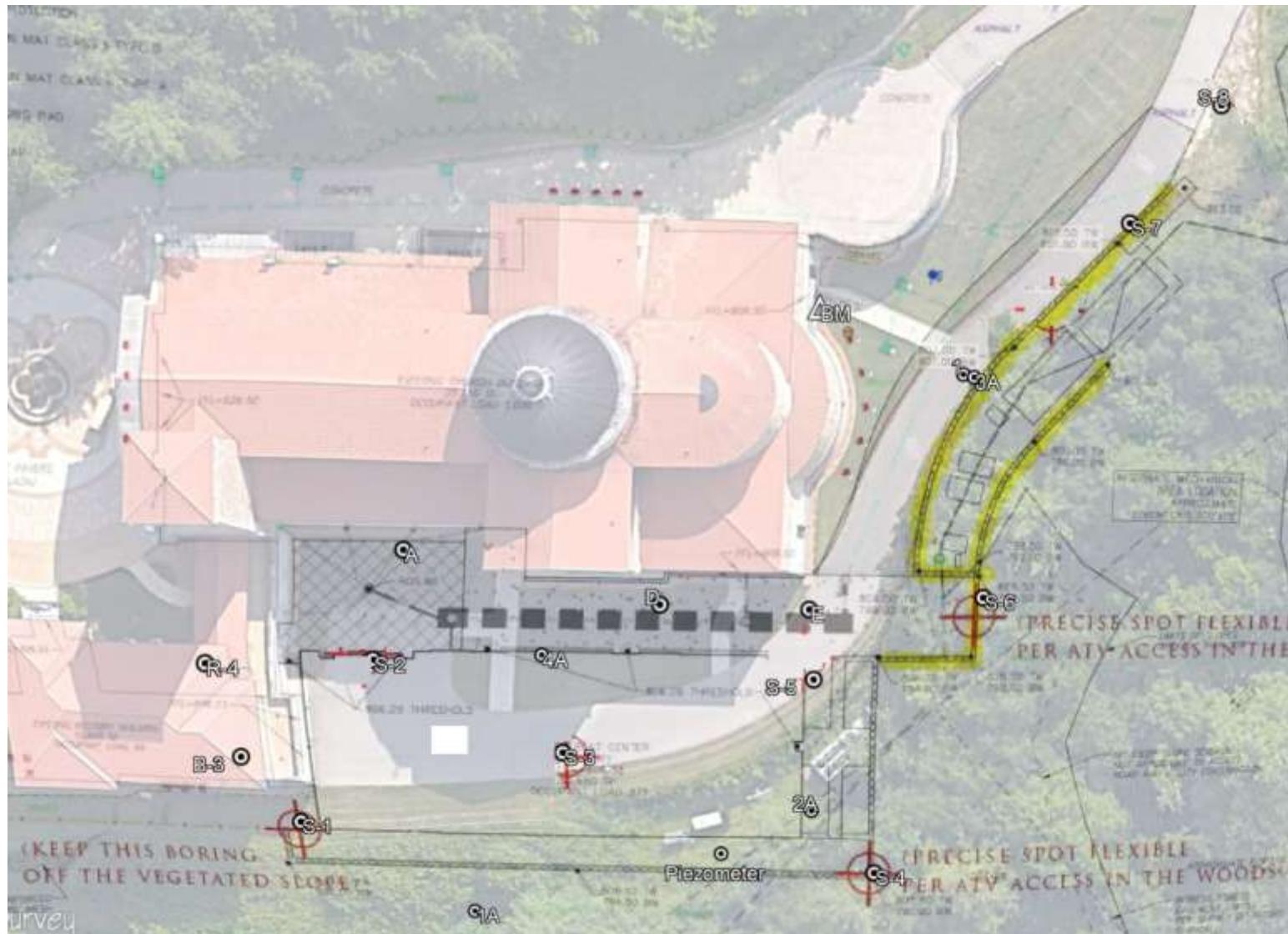


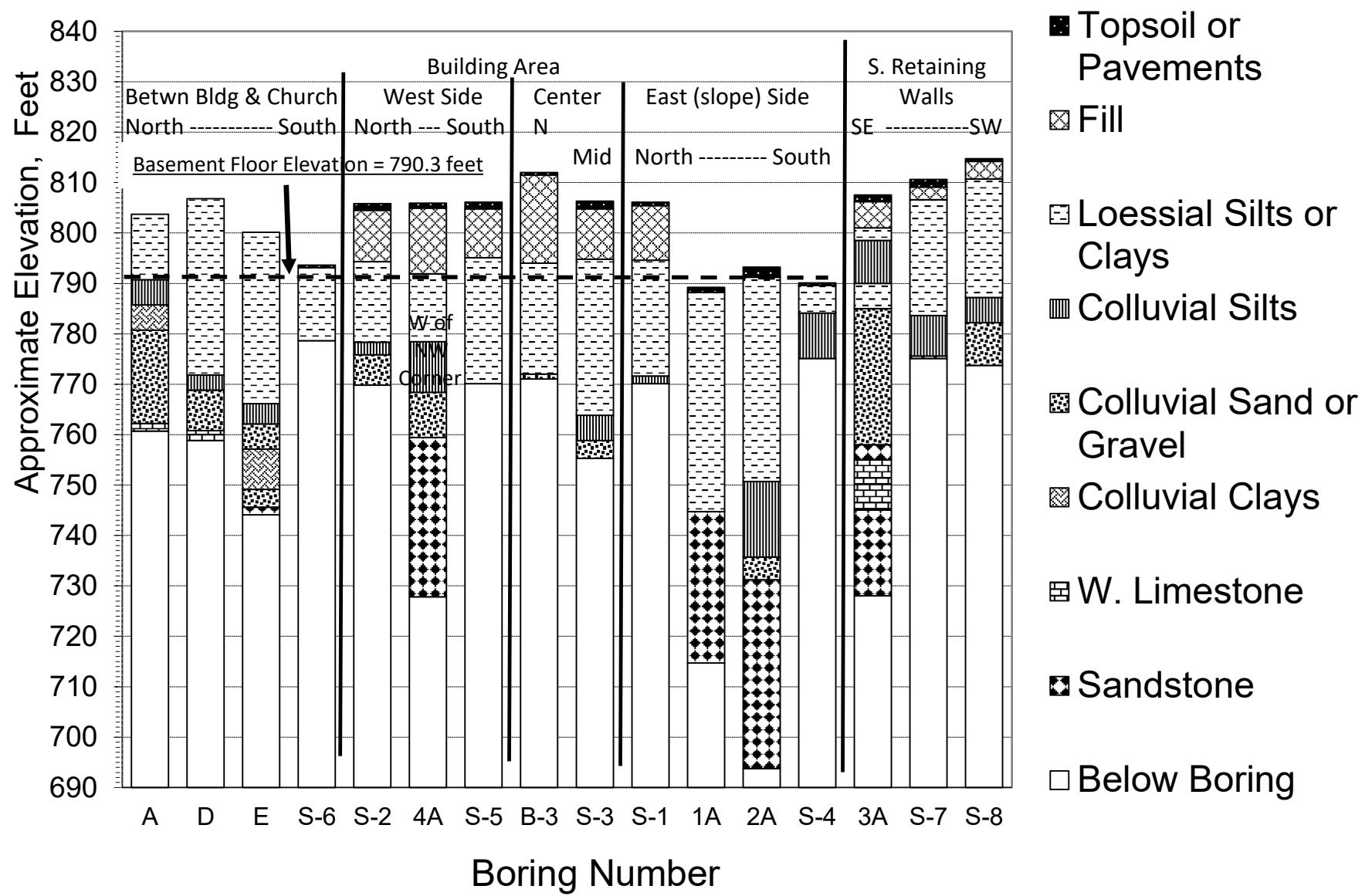
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Boring Location Sketch

Proposed Retreat Center
Our Lady of Guadalupe

CTH MM
La Crosse, Wisconsin
17665.20.WIL





LOG OF BORING

CHOSEN VALLEY TESTING

| | | | | | | | |
|--|--------------|-------------------------|---|----------------------------------|---------------------|--------------|---|
| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | | B-1A | |
| | | | | LOCATION: See attached sketch | | DATE: 7/8/21 | |
| Elev. 789.2 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | | BPF | WL | Tests or Notes |
| 788.2 | 1.0 | ML OL ML | Slightly Organic SILT dark brown. (Topsoil) SILT brown, wet, medium to rather stiff. (Loess) | | 12 8 7 | | Benchmark: Top nut of the fire hydrant southwest of boring B-4A, understood elevation 809.9 feet. PP = 3.0 tsf, MC = 16.1% PP = 2.0 tsf |
| 780.2 | 9.0 | ML | SILT with SAND light brown, wet, medium to very stiff. (Loess) | | 6 13 13 16 | | PP = 1.0 tsf, MC = 13.3% |
| 766.7 | 22.5 | ML | SILT light brown, wet, rather stiff to very stiff. (Loess) | | 17 18 15 | | PP = 2.25 tsf, MC = 16.3% |
| | | | Gray below 37.5'. Very wet below 37.5'. | | 9 | | PP = 1.5 tsf |
| 744.7 | 44.5 | SP SM | WEATHERED SANDSTONE , poorly graded sand with silt, fine grained, yellowish brown, very dense. White below 47.5'. | | * | | * 28 / 50 = 5" Hard drilling below 45.5'. |
| | | | | | * | | * 50 = 4" (set) |
| 731.7 | 57.5 | SP | WEATHERED SANDSTONE , poorly graded sand, fine grained, yellowish brown, very dense. | | * | | * 50 = 0.5" (set) |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT & STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | B-1A (cont.) | |
|--|-------|-------------------|--|-----------|---------------------|---|
| | | | | LOCATION: | See attached sketch | |
| | | | | DATE: | 7/8/21 | SCALE: 1" = 8' |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | | BPF | WL |
| 714.7 | 74.5 | | End of boring. Boring sealed upon completion. | | * | * 50 = 0.5" (set) * 50 = 0.5" (set) * 50 = 0.25" (set) * 50 = 0" (set) |

L.O.B. 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | | B-2A | | | |
|--|--------------|-------------------------|---|----------------------------------|--|---------------|--|--|--|
| | | | | LOCATION: See attached sketch | | DATE: 7/12/21 | | | |
| Elev. 793.2 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | | | BPF | WL | | |
| | | | | | | Tests | or Notes | | |
| 791.2 | 2.0 | ML OL | <u>Slightly Organic SILT</u> dark brown. (Topsoil) | | | 8 | Benchmark: Top nut of the fire hydrant southwest of boring B-4A, understood elevation 809.9 feet. PP = 1.25 tsf, MC = 14.7% | | |
| | | ML | <u>SILT</u> brown, wet, medium. (Loess) | | | 6 | | | |
| 784.2 | 9.0 | ML | <u>SILT with SAND</u> light brown, wet, rather stiff. (Loess) | | | 8 | PP = 0.25 tsf | | |
| | | ML | | | | 9 | | | |
| | | ML | | | | 10 | PP = 0.5 tsf, MC = 10.3% | | |
| | | ML | | | | 9 | PP = 1.0 tsf | | |
| 765.7 | 27.5 | ML | <u>SILT</u> light brown, wet, rather stiff. (Loess) | | | 11 | | | |
| | | ML | | | | 11 | PP = 1.0 tsf, MC = 12.9% | | |
| 750.7 | 42.5 | ML | <u>SILT</u> trace gravel, brown, wet, stiff. (Colluvium) | | | 10 | | | |
| | | ML | | | | 10 | | | |
| 745.7 | 47.5 | ML | <u>SANDY SILT</u> trace gravel, brown, wet, medium to rather stiff. (Colluvium) | | | 12 | PP = 1.25 tsf, MC = 15.5% | | |
| | | ML | | | | 13 | | | |
| 735.7 | 57.5 | SM | <u>SILTY SAND with GRAVEL</u> fine to medium grained, brown, moist, medium dense. | | | 7 | PP = 1.25 tsf, MC = 17.6% | | |
| | | SM | | | | 10 | | | |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: B-2A (cont.) | | |
|--|-------|-------------------|---|-------------------------------|----|---|
| | | | | LOCATION: See attached sketch | | |
| | | | | DATE: 7/12/21 | | SCALE: 1" = 8' |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 731.2 | 62.0 | | (Colluvium) | X | 18 | |
| | | SP | WEATHERED SANDSTONE , poorly graded sand, fine grained, white, very dense. | * | | Hard drilling below 62'. * 50 = 1" (set) |
| | | | Yellowish brown below 67.5'. | * | | * 50 = 0.5" (set) |
| | | | | * | | * 50 = 0" (set) |
| | | | | * | | * 50 = 0.5" (set) |
| | | | | * | | * 50 = 0" (set) |
| | | | | * | | * 50 = 0.25" (set) |
| | | | White below 92.5'. | * | | * 50 = 0" (set) |
| 693.7 | 99.5 | | End of boring. Boring sealed upon completion. | * | | * 50 = 0" (set) |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: B-3A |
|--|--------------|-------------------------|--|----------------------------------|
| | | | | LOCATION: See attached sketch |
| | | DATE: 7/8/21 | | SCALE: 1" = 8' |
| Elev. 807.5 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF WL Tests or Notes |
| 807.2 | 0.3 | | 4" ASPHALT | |
| 806.2 | 1.3 | SM | 12" AGGREGATE BASE FILL , silty sand, trace asphalt, trace gravel, fine to medium grained, light brown, moist, loose to medium dense. | 8 10 |
| 801.0 | 6.5 | | | |
| 798.5 | 9.0 | ML | SILT gray, wet, stiff. (Loess) | 13 |
| | | ML | SANDY SILT trace gravel, brown, wet, rather stiff to very stiff. (Colluvium) Seams of sand around 10'. | 12 22 24 |
| 790.0 | 17.5 | ML | SILT with SAND light brown, wet, very stiff. (Loess) | 17 |
| 785.0 | 22.5 | SM | SILTY SAND with GRAVEL fine to medium grained, light brown, moist, very dense. (Colluvium) | 52 |
| 780.0 | 27.5 | SP | POORLY GRADED SAND with GRAVEL fine grained, yellowish brown, moist, very dense. (Colluvium) | * |
| 775.0 | 32.5 | SM | SILTY SAND with GRAVEL seams of sandy silt, fine to medium grained, light brown, moist, medium dense to dense. (Colluvium) | 36 10 |
| 765.0 | 42.5 | SM | SILTY SAND trace gravel, fine grained, greenish brown. (Colluvium) | 24 |
| 758.0 | 49.5 | SM | WEATHERED SANDSTONE , silty sand, greenish brown, very dense. | * |
| 755.0 | 52.5 | GP | WEATHERED LIMESTONE , poorly graded gravel, light brown, very dense. | * |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: B-3A (cont.) | | |
|--|-------|-------------------|--|-------------------------------|----|--------------------|
| | | | | LOCATION: See attached sketch | | |
| | | | | DATE: 7/8/21 | | SCALE: 1" = 8' |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 745.0 | 62.5 | SP | WEATHERED SANDSTONE , poorly graded sand, fine grained, light brown, very dense. White around 70'. | * | | * 50 = 0.25" (set) |
| 728.0 | 79.5 | | End of boring. Boring sealed upon completion. | * | | * 50 = 0" (set) |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER) AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.

17665.20.WIL

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | B-4A | |
|--|--------------|-------------------------|---|---------------|---------------------|--|
| | | | | LOCATION: | See attached sketch | |
| | | | | DATE: | 7/6/21 | SCALE: 1" = 8' |
| Elev. 805.9 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 804.9 | 1.0 | ML OL ML | <u>Slightly Organic SILT</u> dark brown. (Topsoil) <u>FILL</u> , silt, brown, wet, medium to stiff. | 13 8 16 | | Benchmark: Top nut of the fire hydrant southwest of boring B-4A, understood elevation 809.9 feet. PP = 2.25 tsf, MC = 17.3% PP = 1.0 tsf PP = 1.5 tsf |
| 798.4 | 7.5 | | | | | |
| 796.9 | 9.0 | SM ML | <u>FILL</u> , silty sand with gravel, fine to medium grained, light brown, moist, medium dense. <u>FILL</u> , silty sand, trace gravel, brown, wet, stiff. | 15 | | PP = 1.0 tsf, MC = 14.9% |
| 793.4 | 12.5 | | | | | PP = 1.75 tsf |
| 791.9 | 14.0 | SM ML | <u>FILL</u> , silty sand, trace gravel, fine to medium grained, light brown, moist, medium dense. <u>SILT</u> brown, wet, medium. (Loess) | 12 7 6 | | PP = 2.0 tsf PP = 2.0 tsf, MC = 20.4% |
| 783.4 | 22.5 | ML | <u>SILT with SAND</u> light brown, wet, stiff. (Loess) | 16 | | PP = 1.5 tsf, MC = 15.7% |
| 778.4 | 27.5 | ML | <u>SANDY SILT</u> trace gravel, brown, wet, rather stiff. (Colluvium) | 10 | | PP = 1.5 tsf, MC = 20.5% |
| 768.4 | 37.5 | SM | <u>SILTY SAND</u> trace gravel, light brown, moist, medium dense to very dense. (Colluvium) | 11 28 | | PP = 2.0 tsf |
| 759.4 | 46.5 | SM | <u>WEATHERED SANDSTONE</u> , silty sand, fine grained, brown, very dense. | 52 * | | Hard drilling below 46.5'. * 50 = 0" (set) * 50 = 0" (set) |
| | | | | * | | * 50 = 0" (set) |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: B-4A (cont.) | | |
|--|-------|-------------------|--|----------------------------------|----|--|
| | | | | LOCATION: See attached sketch | | |
| | | | | DATE: 7/6/21 SCALE: 1" = 8' | | |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 738.4 | 67.5 | SP | Greenish brown below 62.5'. WEATHERED SANDSTONE , poorly graded sand, fine grained, yellowish brown, very dense. | * | * | * 50 = 0" (set) * 50 = 0" (set) |
| 727.8 | 78.1 | | Light brown below 76.5'. End of boring. Boring sealed upon completion. | * | * | * 50 = 0" (set) * 50 = 0" (set) |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

17665.20.WIL

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | | S-1 | |
|--|--------------|-------------------------|---|----------------------------------|----|--|--|
| | | | | LOCATION: See attached sketch | | DATE: 2/23/21 | |
| Elev. 806.1 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes | |
| 805.4 | 0.7 | CL OL SM | <u>Slightly Organic LEAN CLAY</u> black. (Topsoil / Fill) <u>SILTY SAND</u> trace gravel, fine to medium grained, light brown, moist, medium dense. (Fill) | 14 20 | | Benchmark: Finished floor of the existing building at the southeast door, understood elevation 806.5 feet. | |
| 798.6 | 7.5 | ML | <u>SILT</u> brown, wet, soft to rather soft. (Fill) | 4 3 | | PP = 0.75 tsf PP = 0.75 tsf, MC = 24.0% | |
| 794.6 | 11.5 | ML | <u>SANDY SILT</u> trace gravel, brown, wet, rather soft to medium. (Colluvium) | 7 4 | | PP = 0.5 tsf PP = 0.5 tsf, MC = 24.6% | |
| 788.6 | 17.5 | ML | <u>SANDY SILT</u> brown to gray, wet, rather stiff. (Loess) | 11 10 11 | | PP = 2.25 tsf PP = 0.5 tsf, MC = 20.2% | |
| 771.1 | 35.0 | | | | | | |
| 770.1 | 36.0 | ML | <u>SANDY SILT</u> trace gravel, gray, wet, stiff. (Colluvium) End of boring. Boring sealed upon completion. | 13 | | | |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | S-2 | |
|--|-------|-------------------|--|-----------|---------------------|---------------------------|
| | | | | LOCATION: | See attached sketch | |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | DATE: | 2/23/21 | SCALE: 1" = 7' |
| 805.8 | 0.0 | | | | | |
| 805.5 | 0.3 | | 3" ASPHALT | | | |
| 804.7 | 1.1 | ML | 10" AGGREGATE BASE SANDY SILT trace gravel, brown, wet, rather soft to medium. (Fill) No gravel around 5'. Gray below 6.5'. Pockets of topsoil around 7.5'. | | 8 | PP = 1.5 tsf |
| 794.3 | 11.5 | | Trace roots around 10'. | | 4 | PP = 1.25 tsf, MC = 18.5% |
| | | CL ML | SILTY CLAY brown, wet, medium to stiff. (Loess) | | 5 | PP = 0.5 tsf, MC = 22.9 |
| | | ML | SILT brown, wet, medium to rather stiff. (Loess) | | 4 | PP = 0.5 tsf |
| 788.3 | 17.5 | | | | 13 | PP = 2.0 tsf, MC = 23.0% |
| | | ML | | | 7 | PP = 1.5 tsf |
| 778.3 | 27.5 | ML | SANDY SILT trace gravel, brown, wet, stiff. (Colluvium) | | 8 | PP = 1.0 tsf, MC = 14.8% |
| 775.8 | 30.0 | | SILTY SAND trace gravel, fine to medium grained, brown, moist, medium dense. (Colluvium) | | 10 | PP = 1.5 tsf |
| 773.3 | 32.5 | SM | POORLY GRADED SAND with GRAVEL fine to medium grained, light brown, moist, medium dense. (Residuum) | | 16 | PP = 1.5 tsf, MC = 13.3% |
| 769.8 | 36.0 | SP | End of boring. Boring sealed upon completion. | | 14 | |

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | S-3 | |
|--|-------|-------------------|--|-----------|---------------------|----------------------------|
| | | | | LOCATION: | See attached sketch | |
| | | DATE: 2/23/21 | | SCALE: | 1" = 7' | |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 806.3 | 0.0 | | | | | |
| 806.0 | 0.3 | | 4" ASPHALT | | | |
| 804.8 | 1.5 | ML | 14" AGGREGATE BASE SANDY SILT trace gravel, pockets of silty clay, brown, wet, medium to rather stiff. (Fill) No silty clay pockets below 4'. Trace roots below 6.5'. Gray below 6.5'. Trace wood around 7.5'. Pockets of topsoil around 10'. | | 10 | PP = 1.0 tsf |
| | | | | | 7 | MC = 18.8% |
| | | | | | 8 | PP = 1.5 tsf |
| | | | | | 7 | PP = 2.0 tsf |
| 794.8 | 11.5 | ML | SILT brown, wet, rather soft to rather stiff. (Loess) | | 5 | PP = 0.75 tsf, MC = 14.3\$ |
| | | | | | 6 | MC = 10.0% |
| | | | | | 4 | MC = 11.3% |
| | | | | | 5 | PP = 1.0 tsf, MC = 13.2% |
| | | | | | 11 | MC = 16.0% |
| | | | | | 10 | PP = 1.25 tsf |
| | | | | | 8 | PP = 1.0 tsf, MC = 20.5% |
| 763.8 | 42.5 | ML | SANDY SILT trace gravel, brown, very wet, medium. (Colluvium) | | 7 | PP = 1.0 tsf, MC = 16.3% |
| 758.8 | 47.5 | SM | SILTY SAND trace gravel, greenish brown, moist, medium dense. (Colluvium) | | 22 | Hard drilling below 47.5'. |
| 755.3 | 51.0 | | End of boring. Boring sealed upon completion. | | | |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | | S-4 | |
|--|-------|-------------------------|---|--|----|---------------|--|
| | | | | LOCATION: See attached sketch | | DATE: 2/23/21 | |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests | Notes |
| 790.1 | 0.0 | | | | | | |
| 789.6 | 0.5 | ML OL ML | <u>Slightly Organic SILT</u> dark brown. (Topsoil) <u>SILT</u> brown, wet. (Loess) | * 11 11 9 8 5 | | | * Frost encountered to 14". MC = 19.2% N-values for Boring B-4 are estimated from DCP values. MC = 8.4% |
| 784.1 | 6.0 | ML | <u>SANDY SILT</u> brown, wet. (LOESS) | 7 6 7 7 9 9 9 9 8 7 | | | MC = 10.7% |
| 775.1 | 15.0 | | End of hand auger probe. Probe sealed upon completion. | | | | |
| LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.) | | | | | | | |
| 17665.20.WIL | | | | | | | |

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: | S-5 | |
|--|-------|-------------------|---|-----------|---------------------|---|
| | | | | LOCATION: | See attached sketch | |
| | | | | DATE: | 2/23/21 | SCALE: 1" = 7' |
| Elev. | Depth | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 806.1 | 0.0 | | | | | |
| 805.8 | 0.3 | | 4" ASPHALT | | | |
| 804.8 | 1.3 | SM | 12" AGGREGATE BASE | | | |
| 801.1 | 5.0 | ML | SILTY SAND trace gravel, medium to coarse grained, light brown, moist, medium dense. (Fill) | 17 | | |
| 797.1 | 9.0 | ML | SILT brown, wet, medium to rather stiff. (Fill) | 8 | | PP = 2.0 tsf, MC = 17.0% Poor sample return. |
| 788.6 | 17.5 | ML | SANDY SILT trace gravel, brown, wet, rather soft to medium. (Loess) | 10 | | MC = 16.6% |
| 770.1 | 36.0 | | SANDY SILT brown, wet, medium to rather stiff. (Loess) | 4 | | MC = 19.0% |
| | | | | 7 | | PP = 0.5 tsf |
| | | | | 6 | | MC = 11.0% |
| | | | End of boring. Boring sealed upon completion. | 10 | | PP = 1.25 tsf, MC = 17.0% |
| | | | | 7 | | |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: S-6 |
|--|--------------|-------------------------|---|----------------------------------|
| | | | | LOCATION: See attached sketch |
| | | DATE: 2/23/21 | | SCALE: 1" = 7' |
| Elev. 793.6 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF |
| 793.1 | 0.5 | ML | <u>Slightly Organic SILT</u> dark brown. (Topsoil) | * |
| 792.1 | 1.5 | OL | | 3 |
| 791.1 | 2.5 | ML | <u>SILT</u> brown, wet. | 9 |
| | | CL | (Loess) | 10 |
| | | ML | <u>SILTY CLAY</u> brown, wet. | 9 |
| | | ML | (Loess) | 8 |
| 786.1 | 7.5 | ML | <u>SILT</u> light brown, wet. (Loess) | 8 |
| | | | <u>SANDY SILT</u> light brown, wet. (Loess) | 6 |
| | | | | 9 |
| | | | | 12 |
| | | | | 15 |
| | | | | 15 |
| 778.6 | 15.0 | | End of hand auger probe. Probe sealed upon completion. | 13 |
| | | | | 15 |
| N-values for Boring B-6 are estimated from DCP values. | | | | |
| LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.) | | | | |
| 17665.20.WIL | | | | |
| S-6 page 1 of 1 | | | | |

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: S-7 |
|--|--------------|-------------------------|--|----------------------------------|
| | | | | LOCATION: See attached sketch |
| | | DATE: 2/23/21 | | SCALE: 1" = 7' |
| Elev. 810.6 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF WL |
| 810.3 | 0.3 | | 4" ASPHALT | |
| 809.1 | 1.5 | CL | 14" AGGREGATE BASE | |
| 806.6 | 4.0 | ML | SILTY CLAY pockets of topsoil, brown, wet, rather stiff. | 12 |
| | | CL | (Fill) | 10 |
| 804.1 | 6.5 | ML | LEAN CLAY brown, wet, rather stiff. (Loess) | 7 |
| | | | SILT brown, wet, medium to stiff. (Loess) | 6 |
| | | | Light brownish gray below 11.5'. | 8 |
| | | | Brown below 17.5'. | 10 |
| | | | | 13 |
| 783.1 | 27.5 | ML | SANDY SILT trace gravel, brown, wet, very stiff to hard. (Colluvium) | 10 |
| | | | | 31 |
| 775.1 | 35.5 | | | PP = 0.75 tsf |
| 774.6 | 36.0 | SM | SILTY SAND trace gravel, fine grained, greenish brown, moist, medium dense. (Colluvium) | PP = 2.0 tsf |
| | | | End of boring. Boring sealed upon completion. | 24 |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: 17665.20.WIL Design Phase Geotechnical Evaluation Proposed Retreat Center CTH MM La Crosse, Wisconsin | | | | BORING: S-8 | | |
|--|--------------|-------------------------|---|----------------------------------|----|---------------------------|
| | | | | LOCATION: See attached sketch | | |
| | | | | DATE: 2/23/21 | | SCALE: 1" = 7' |
| Elev. 814.7 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| 814.2 | 0.5 | ML | 6" AGGREGATE BASE SANDY SILT brown, wet. (Fill) | | * | |
| 810.7 | 4.0 | | SILTY CLAY brown, wet, very stiff. (Loess) | | 29 | MC = 13.9% |
| 808.2 | 6.5 | CL ML | SILT brown, wet, medium to rather stiff. (Loess) | | 10 | PP = 2.5 tsf, MC = 20.7% |
| | | | | | 7 | PP = 0.75 tsf |
| | | | | | 9 | PP = 0.75 tsf |
| | | | | | 11 | PP = 1.0 tsf, MC = 14.4% |
| | | | | | 11 | PP = 0.5 tsf |
| | | | | | 11 | PP = 1.25 tsf |
| 792.2 | 22.5 | ML | SILT with SAND trace gravel, brown, wet, rather stiff. (Colluvium) | | 10 | |
| 787.2 | 27.5 | SM | SILTY SAND seams of lean clay, trace gravel, fine grained, greenish brown, moist, medium dense. (Colluvium) | | 21 | PP = 0.75 tsf, MC = 21.8% |
| 778.7 | 36.0 | | End of boring. Boring sealed upon completion. | | 19 | |

LOG 17665.20.WIL (OUR LADY OF GUADALUPE RETREAT CENTER REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: L2007.017 Design Phase Geotechnical Evaluation Proposed Church for Shrine of Our Lady of Guadalupe County Highway MM La Crosse, Wisconsin | | | | BORING: B-3 | | | |
|--|---------------|--------------|-------------------------|---|-----|----------------|----------------|
| | | | | LOCATION: See attached sketch. | | | |
| | | | | DATE: 02/14/07 | | SCALE: 1" = 6' | |
| Approx. Elev: 812 | Elev. 84.9 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| | 84.4 | 0.5 | ML | <u>6" RECYCLED BITUMINOUS</u> , fabric under bituminous. <u>SILT to SANDY SILT</u> , rare gravel, brown to light brown, frozen to about 2 feet then moist to about 11 feet then wet, medium to very stiff. (Fill) | 15 | 9 | |
| | 66.9 | 18.0 | ML | <u>SILT</u> , with wood, light gray to light brown, very wet, soft. (Fill) | 14 | 21 | |
| | 61.9 | 23.0 | ML | <u>SILT</u> , trace clay, brown to light brown, moist to wet, stiff. (Loess) | 6 | 2 | |
| | 56.9 | 28.0 | ML | <u>SANDY SILT</u> , tan, moist, medium to stiff. (Loess) | 14 | 7 | |
| | 44.9 | 40.0 | GM | <u>SILTY SAND with GRAVEL</u> , fine grained sand, dolostone gravel, light brown to yellowish orange, moist, medium dense. (Colluvium) | 12 | 14 | |
| | 43.9 | 41.0 | | End of Boring. Boring dry upon completion. Boring sealed with bentonite grout upon completion. | | | |

(SFE REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY)

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: L2007.017 Design Phase Geotechnical Evaluation Proposed Church for Shrine of Our Lady of Guadalupe County Highway MM La Crosse, Wisconsin | | | | BORING: B-5 | | | |
|--|---------------|--------------|-------------------------|--|----------------------------------|----------------|------------------|
| | | | | LOCATION: See attached sketch. | | | |
| | | | | DATE: 08/20/03 | | SCALE: 1" = 6' | |
| Approx. Elev. 782 | Elev. 55.0 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| | 54.3 | 0.7 | M1 ML | <u>SILT</u> , dark brown, dry. (Topsoil) <u>SILT</u> , brown, moist, very loose to medium dense. (Loess) | 7 6 4 3 6 6 12 | | |
| | 32.5 | 22.5 | SS | <u>WEATHERED SANDSTONE</u> , light brown, moist. | * | | * 56 = 9" (set) |
| | 25.9 | 29.1 | | End of Boring. Water not observed while drilling. Boring then grouted. | ** | | ** 50 = 1" (set) |

(SEE REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

1.08 1.2007-1.GHY 03.02.07

L2007.017

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: L2003.187 Design Phase Geotechnical Evaluation Proposed Shrine for Our Lady of Guadalupe Church County Highway MM LaCrosse, Wisconsin | | | | BORING: A | | |
|--|--------------|-------------------------|--|----------------------------------|----|---|
| | | | | LOCATION: See attached sketch | | |
| | | | | DATE: 01/14/03 SCALE: 1" = 8' | | |
| Elev. 803.7 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| | | ML | <u>SILT</u> , tan to light brown, moist, rather stiff to stiff. (Loess) | | 9 | |
| 790.7 | 13.0 | ML | <u>SILT</u> , with limestone gravel, light brown, moist, hard. (Colluvium) | | 14 | |
| 785.7 | 18.0 | CL | <u>SANDY LEAN CLAY</u> , with silt and limestone gravel, brown to green, moist, hard. (Colluvium) | | 30 | Some grinding on auger at 18 feet. |
| 780.7 | 23.0 | GM | <u>SILTY SAND and GRAVEL</u> , trace green clay, tan to pale yellow, moist, medium dense to very dense. (Residuum) | | 35 | |
| 766.7 | 37.0 | GM | <u>SILTY SAND and GRAVEL</u> , with clay layers, tan to green, moist, loose. (Residuum) | | 43 | * 50=5" (set) |
| 762.2 | 41.5 | | | | 21 | |
| 760.7 | 43.0 | | <u>WEATHERED LIMESTONE</u> , tan to pale yellow. End of boring. Auger refusal at 43 feet, presumably on fresh limestone. Cave in at 31.5 feet after auger withdrawal. Boring backfilled upon completion. | | 8 | Grinding on auger at 41.5 feet. ** 50=0" (set) |
| (SEE REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.) | | | | | | |
| L2003-187.GPJ 02/01/04 | | | | | | |
| L2003.187 | | | | | | |

LOG OF BORING

CHOSEN VALLEY TESTING

| PROJECT: L2003.187 Design Phase Geotechnical Evaluation Proposed Shrine for Our Lady of Guadalupe Church County Highway MM LaCrosse, Wisconsin | | | | BORING: D | | | | | |
|--|--------------|-------------------------|--|----------------------------------|--|----------------|--|--|--|
| | | | | LOCATION: See attached sketch | | | | | |
| | | | | DATE: 01/14/03 | | SCALE: 1" = 8' | | | |
| Elev. 806.8 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | | | BPF | WL | | |
| | | ML | SILT , tan to light brown, moist, medium to rather stiff. (Loess) | | | 12 | 6 | | |
| 771.8 | 35.0 | ML | SILT , with limestone gravel, light brown, moist, very stiff. (Colluvium) | | | 23 | Some grinding on auger at 35 feet. | | |
| 768.8 | 38.0 | GM | SILTY SAND and GRAVEL , with clay layers, green to pale yellow, moist, dense. (Residuum) | | | 30 | | | |
| 760.8 | 46.0 | | WEATHERED LIMESTONE , tan to pale yellow. | | | 44 | Grinding on auger at 46 feet. * 50=1/4" (set) | | |
| 758.8 | 48.0 | | End of boring. Auger refusal at 48 feet, presumably on fresh limestone. Boring backfilled upon completion. | | | * | | | |

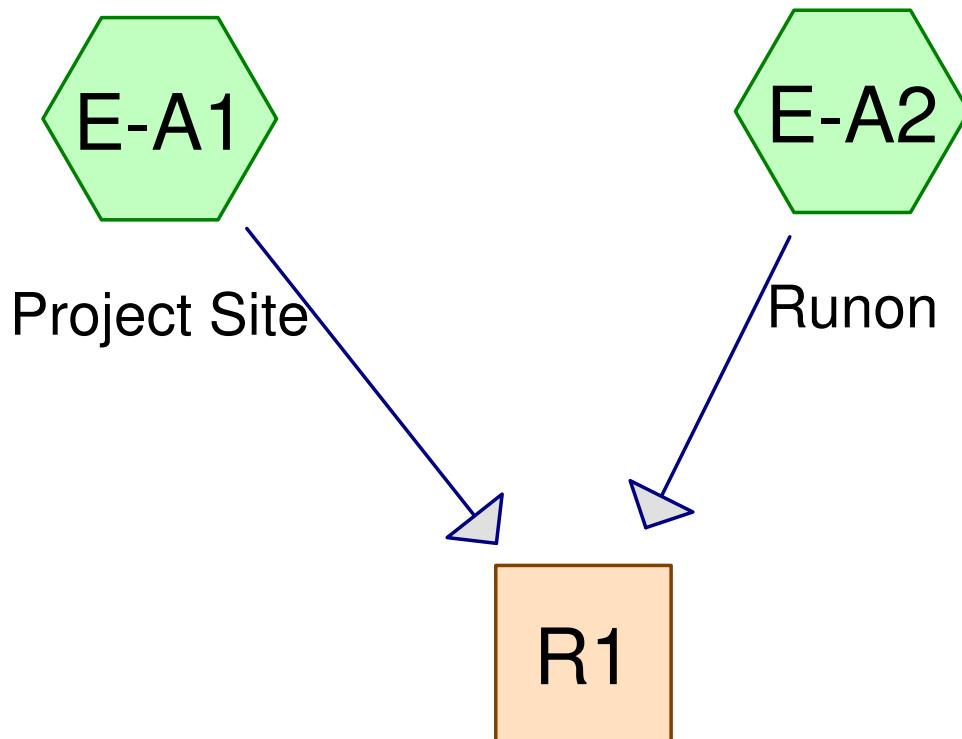
LOG OF BORING

CHOSEN VALLEY TESTING

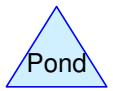
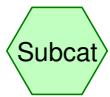
| PROJECT: L2003.187 Design Phase Geotechnical Evaluation Proposed Shrine for Our Lady of Guadalupe Church County Highway MM LaCrosse, Wisconsin | | | | BORING: E | | |
|--|--------------|-------------------------|--|----------------------------------|--|------------------------------------|
| | | | | LOCATION: See attached sketch | | |
| | | | | DATE: 01/14/03 SCALE: 1" = 8' | | |
| Elev. 800.1 | Depth 0.0 | ASTM D2487 Symbol | Description of Materials (ASTM D2488) | BPF | WL | Tests or Notes |
| | | CL | <u>LEAN CLAY</u> , brown to light brown, wet, rather stiff to stiff. (Loess) | | 13 10 11 16 15 15 24 15 | |
| 794.1 | 6.0 | ML | <u>SILT</u> , tan to light brown, moist, rather stiff to very stiff. (Loess) | | 11 16 15 15 24 15 | |
| 766.1 | 34.0 | ML | <u>SILT</u> , with limestone gravel, light brown, moist, hard. (Colluvium) | | 32 | Some grinding on auger at 34 feet. |
| 762.1 | 38.0 | GM | <u>SILTY SAND and GRAVEL</u> , with green clay, tan to pale yellow, moist, dense. (Residuum/Colluvium) | | 41 | |
| 757.1 | 43.0 | CL | <u>SANDY LEAN CLAY</u> , with limestone gravel, pale green to pale yellow, wet, medium dense to dense. (Residuum/Colluvium) | | 26 13 | |
| 749.1 | 51.0 | SP | <u>POORLY GRADED SAND</u> , fine grained, tan to white, moist, medium dense. (Residuum) | | * | * 50=1" (set) |
| 745.6 | 54.5 | | <u>WEATHERED SANDSTONE</u> , tan to pale yellow. End of boring. Auger refusal at 55 feet, presumably on fresh sandstone. Cave in at 47 feet after auger withdrawal. Boring backfilled upon completion. | | | |
| L2003.187 | 04/02/0104 | | | | | |

(SEE REPORT AND STANDARD PLATES FOR EVALUATION AND DESCRIPTIVE TERMINOLOGY.)

4 Peak Runoff Rate Control Calculations



Existing Conditions



Routing Diagram for Retreat Center - Copy3
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Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

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Page 2

Area Listing (selected nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|----|---|
| 1.019 | 58 | Woods/grass comb., Good, HSG B (E-A1, E-A2) |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

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Page 3

Soil Listing (selected nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|-----------------|---------------|-------------------------|
| 0.000 | HSG A | |
| 1.019 | HSG B | E-A1, E-A2 |
| 0.000 | HSG C | |
| 0.000 | HSG D | |
| 0.000 | Other | |

Retreat Center - Copy3

Existing Conditions

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Page 4

Ground Covers (selected nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|------------------|------------------|------------------|------------------|------------------|------------------|-------------------------|-------------------------|
| 0.000 | 1.019 | 0.000 | 0.000 | 0.000 | 1.019 | Woods/grass comb., Good | E-A1, E-A2 |

Retreat Center - Copy3

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Existing Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
Printed 9/16/2024
Page 5

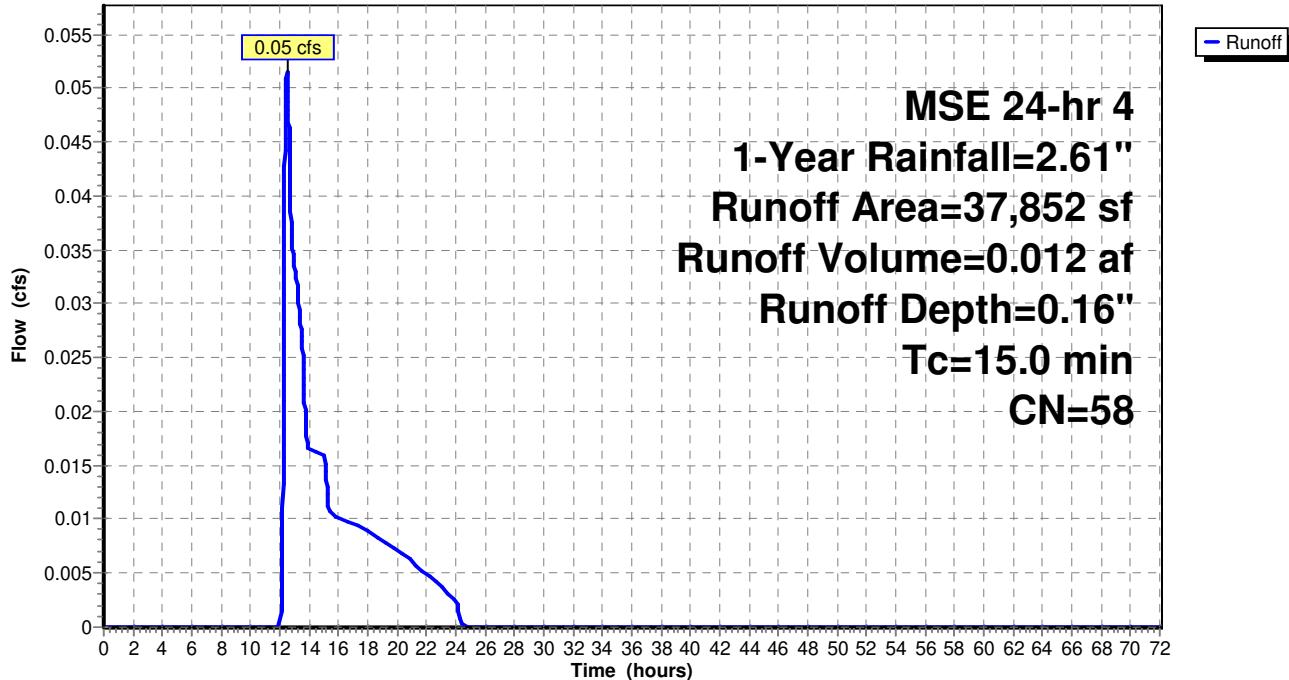
Summary for Subcatchment E-A1: Project Site

Runoff = 0.05 cfs @ 12.48 hrs, Volume= 0.012 af, Depth= 0.16"
Routed to Reach R1 : Existing Conditions

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 1-Year Rainfall=2.61"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 37,852 | 58 | Woods/grass comb., Good, HSG B |
| 37,852 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|-------------|
| 15.0 | Direct Entry, | | | | |

Subcatchment E-A1: Project Site**Hydrograph**

Retreat Center - Copy3

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Existing Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
 Printed 9/16/2024
 Page 6

Hydrograph for Subcatchment E-A1: Project Site

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 2.61 | 0.16 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 2.61 | 0.16 | 0.00 |
| 2.00 | 0.03 | 0.00 | 0.00 | 53.00 | 2.61 | 0.16 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 2.61 | 0.16 | 0.00 |
| 4.00 | 0.08 | 0.00 | 0.00 | 55.00 | 2.61 | 0.16 | 0.00 |
| 5.00 | 0.12 | 0.00 | 0.00 | 56.00 | 2.61 | 0.16 | 0.00 |
| 6.00 | 0.16 | 0.00 | 0.00 | 57.00 | 2.61 | 0.16 | 0.00 |
| 7.00 | 0.21 | 0.00 | 0.00 | 58.00 | 2.61 | 0.16 | 0.00 |
| 8.00 | 0.26 | 0.00 | 0.00 | 59.00 | 2.61 | 0.16 | 0.00 |
| 9.00 | 0.32 | 0.00 | 0.00 | 60.00 | 2.61 | 0.16 | 0.00 |
| 10.00 | 0.41 | 0.00 | 0.00 | 61.00 | 2.61 | 0.16 | 0.00 |
| 11.00 | 0.56 | 0.00 | 0.00 | 62.00 | 2.61 | 0.16 | 0.00 |
| 12.00 | 1.22 | 0.00 | 0.00 | 63.00 | 2.61 | 0.16 | 0.00 |
| 13.00 | 2.05 | 0.05 | 0.03 | 64.00 | 2.61 | 0.16 | 0.00 |
| 14.00 | 2.20 | 0.07 | 0.02 | 65.00 | 2.61 | 0.16 | 0.00 |
| 15.00 | 2.29 | 0.09 | 0.02 | 66.00 | 2.61 | 0.16 | 0.00 |
| 16.00 | 2.35 | 0.10 | 0.01 | 67.00 | 2.61 | 0.16 | 0.00 |
| 17.00 | 2.40 | 0.11 | 0.01 | 68.00 | 2.61 | 0.16 | 0.00 |
| 18.00 | 2.45 | 0.12 | 0.01 | 69.00 | 2.61 | 0.16 | 0.00 |
| 19.00 | 2.49 | 0.13 | 0.01 | 70.00 | 2.61 | 0.16 | 0.00 |
| 20.00 | 2.53 | 0.14 | 0.01 | 71.00 | 2.61 | 0.16 | 0.00 |
| 21.00 | 2.55 | 0.15 | 0.01 | 72.00 | 2.61 | 0.16 | 0.00 |
| 22.00 | 2.58 | 0.15 | 0.00 | | | | |
| 23.00 | 2.60 | 0.16 | 0.00 | | | | |
| 24.00 | 2.61 | 0.16 | 0.00 | | | | |
| 25.00 | 2.61 | 0.16 | 0.00 | | | | |
| 26.00 | 2.61 | 0.16 | 0.00 | | | | |
| 27.00 | 2.61 | 0.16 | 0.00 | | | | |
| 28.00 | 2.61 | 0.16 | 0.00 | | | | |
| 29.00 | 2.61 | 0.16 | 0.00 | | | | |
| 30.00 | 2.61 | 0.16 | 0.00 | | | | |
| 31.00 | 2.61 | 0.16 | 0.00 | | | | |
| 32.00 | 2.61 | 0.16 | 0.00 | | | | |
| 33.00 | 2.61 | 0.16 | 0.00 | | | | |
| 34.00 | 2.61 | 0.16 | 0.00 | | | | |
| 35.00 | 2.61 | 0.16 | 0.00 | | | | |
| 36.00 | 2.61 | 0.16 | 0.00 | | | | |
| 37.00 | 2.61 | 0.16 | 0.00 | | | | |
| 38.00 | 2.61 | 0.16 | 0.00 | | | | |
| 39.00 | 2.61 | 0.16 | 0.00 | | | | |
| 40.00 | 2.61 | 0.16 | 0.00 | | | | |
| 41.00 | 2.61 | 0.16 | 0.00 | | | | |
| 42.00 | 2.61 | 0.16 | 0.00 | | | | |
| 43.00 | 2.61 | 0.16 | 0.00 | | | | |
| 44.00 | 2.61 | 0.16 | 0.00 | | | | |
| 45.00 | 2.61 | 0.16 | 0.00 | | | | |
| 46.00 | 2.61 | 0.16 | 0.00 | | | | |
| 47.00 | 2.61 | 0.16 | 0.00 | | | | |
| 48.00 | 2.61 | 0.16 | 0.00 | | | | |
| 49.00 | 2.61 | 0.16 | 0.00 | | | | |
| 50.00 | 2.61 | 0.16 | 0.00 | | | | |

Retreat Center - Copy3

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Existing Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
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Summary for Subcatchment E-A2: Runon

Runoff = 0.01 cfs @ 12.48 hrs, Volume= 0.002 af, Depth= 0.16"
Routed to Reach R1 : Existing Conditions

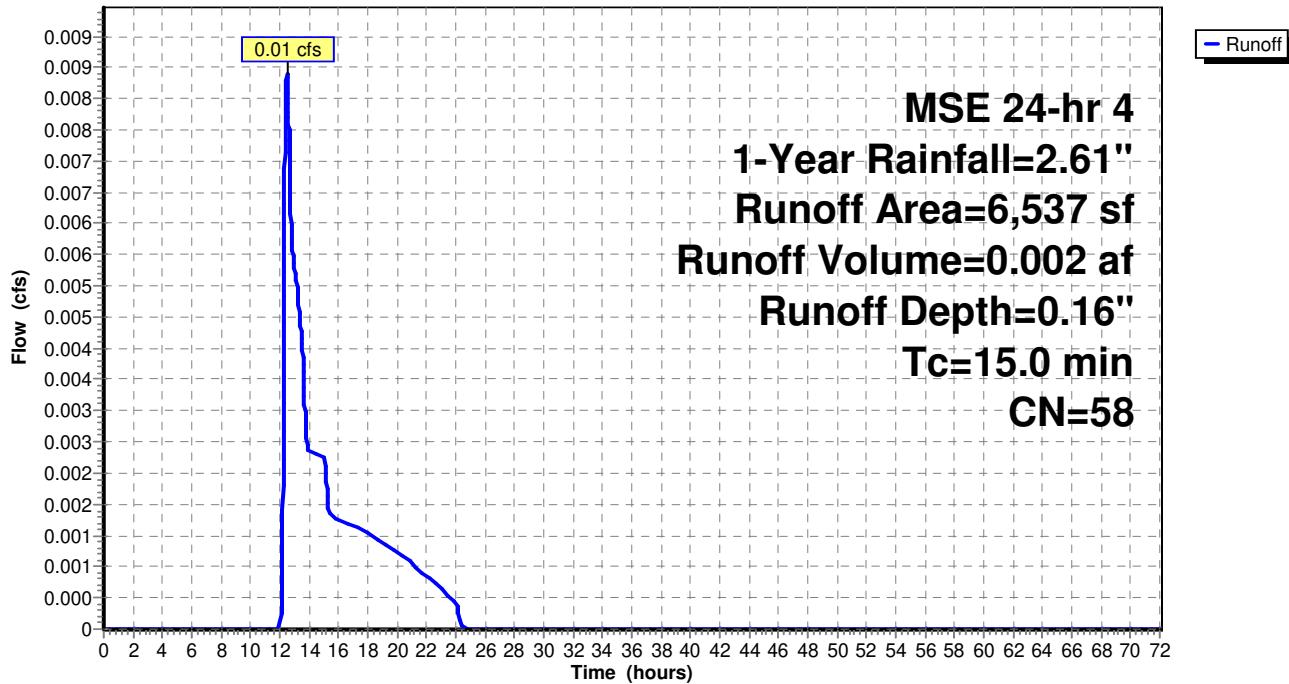
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 1-Year Rainfall=2.61"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 6,537 | 58 | Woods/grass comb., Good, HSG B |
| 6,537 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|---------------|
| 15.0 | | | | | Direct Entry, |

Subcatchment E-A2: Runon

Hydrograph



Retreat Center - Copy3

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Existing Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
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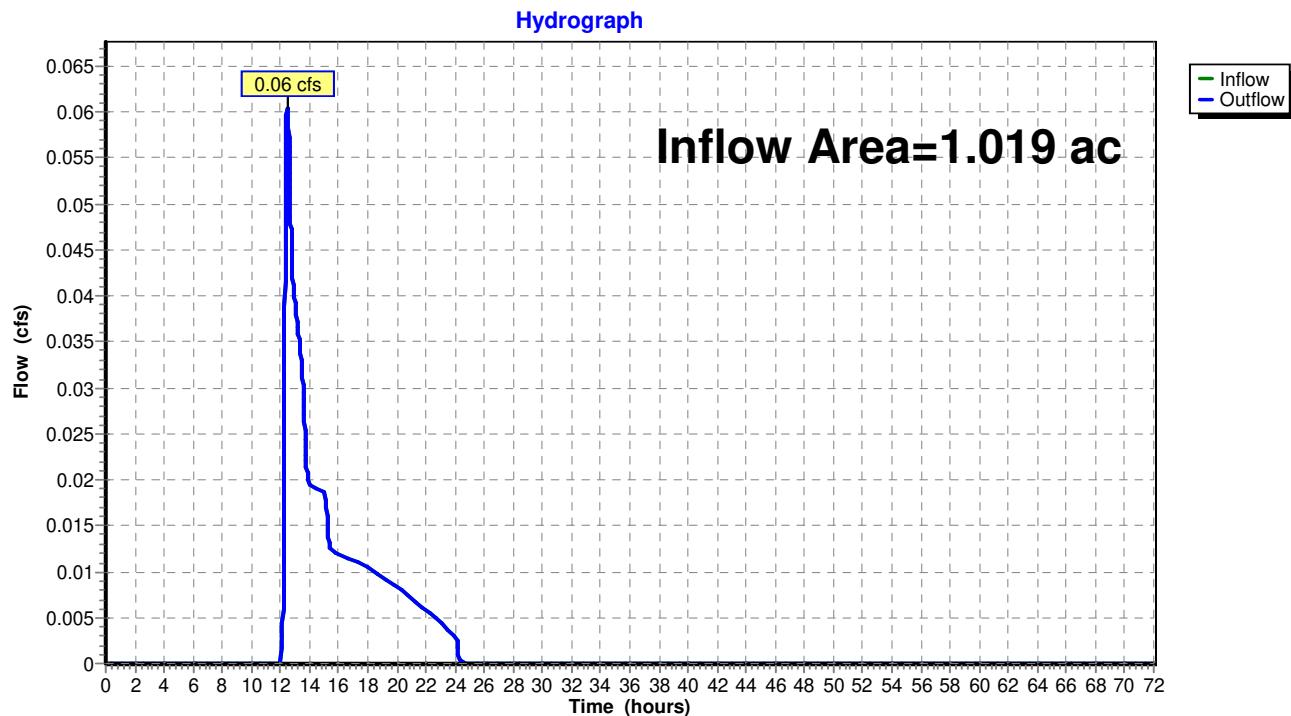
Hydrograph for Subcatchment E-A2: Runon

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 2.61 | 0.16 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 2.61 | 0.16 | 0.00 |
| 2.00 | 0.03 | 0.00 | 0.00 | 53.00 | 2.61 | 0.16 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 2.61 | 0.16 | 0.00 |
| 4.00 | 0.08 | 0.00 | 0.00 | 55.00 | 2.61 | 0.16 | 0.00 |
| 5.00 | 0.12 | 0.00 | 0.00 | 56.00 | 2.61 | 0.16 | 0.00 |
| 6.00 | 0.16 | 0.00 | 0.00 | 57.00 | 2.61 | 0.16 | 0.00 |
| 7.00 | 0.21 | 0.00 | 0.00 | 58.00 | 2.61 | 0.16 | 0.00 |
| 8.00 | 0.26 | 0.00 | 0.00 | 59.00 | 2.61 | 0.16 | 0.00 |
| 9.00 | 0.32 | 0.00 | 0.00 | 60.00 | 2.61 | 0.16 | 0.00 |
| 10.00 | 0.41 | 0.00 | 0.00 | 61.00 | 2.61 | 0.16 | 0.00 |
| 11.00 | 0.56 | 0.00 | 0.00 | 62.00 | 2.61 | 0.16 | 0.00 |
| 12.00 | 1.22 | 0.00 | 0.00 | 63.00 | 2.61 | 0.16 | 0.00 |
| 13.00 | 2.05 | 0.05 | 0.01 | 64.00 | 2.61 | 0.16 | 0.00 |
| 14.00 | 2.20 | 0.07 | 0.00 | 65.00 | 2.61 | 0.16 | 0.00 |
| 15.00 | 2.29 | 0.09 | 0.00 | 66.00 | 2.61 | 0.16 | 0.00 |
| 16.00 | 2.35 | 0.10 | 0.00 | 67.00 | 2.61 | 0.16 | 0.00 |
| 17.00 | 2.40 | 0.11 | 0.00 | 68.00 | 2.61 | 0.16 | 0.00 |
| 18.00 | 2.45 | 0.12 | 0.00 | 69.00 | 2.61 | 0.16 | 0.00 |
| 19.00 | 2.49 | 0.13 | 0.00 | 70.00 | 2.61 | 0.16 | 0.00 |
| 20.00 | 2.53 | 0.14 | 0.00 | 71.00 | 2.61 | 0.16 | 0.00 |
| 21.00 | 2.55 | 0.15 | 0.00 | 72.00 | 2.61 | 0.16 | 0.00 |
| 22.00 | 2.58 | 0.15 | 0.00 | | | | |
| 23.00 | 2.60 | 0.16 | 0.00 | | | | |
| 24.00 | 2.61 | 0.16 | 0.00 | | | | |
| 25.00 | 2.61 | 0.16 | 0.00 | | | | |
| 26.00 | 2.61 | 0.16 | 0.00 | | | | |
| 27.00 | 2.61 | 0.16 | 0.00 | | | | |
| 28.00 | 2.61 | 0.16 | 0.00 | | | | |
| 29.00 | 2.61 | 0.16 | 0.00 | | | | |
| 30.00 | 2.61 | 0.16 | 0.00 | | | | |
| 31.00 | 2.61 | 0.16 | 0.00 | | | | |
| 32.00 | 2.61 | 0.16 | 0.00 | | | | |
| 33.00 | 2.61 | 0.16 | 0.00 | | | | |
| 34.00 | 2.61 | 0.16 | 0.00 | | | | |
| 35.00 | 2.61 | 0.16 | 0.00 | | | | |
| 36.00 | 2.61 | 0.16 | 0.00 | | | | |
| 37.00 | 2.61 | 0.16 | 0.00 | | | | |
| 38.00 | 2.61 | 0.16 | 0.00 | | | | |
| 39.00 | 2.61 | 0.16 | 0.00 | | | | |
| 40.00 | 2.61 | 0.16 | 0.00 | | | | |
| 41.00 | 2.61 | 0.16 | 0.00 | | | | |
| 42.00 | 2.61 | 0.16 | 0.00 | | | | |
| 43.00 | 2.61 | 0.16 | 0.00 | | | | |
| 44.00 | 2.61 | 0.16 | 0.00 | | | | |
| 45.00 | 2.61 | 0.16 | 0.00 | | | | |
| 46.00 | 2.61 | 0.16 | 0.00 | | | | |
| 47.00 | 2.61 | 0.16 | 0.00 | | | | |
| 48.00 | 2.61 | 0.16 | 0.00 | | | | |
| 49.00 | 2.61 | 0.16 | 0.00 | | | | |
| 50.00 | 2.61 | 0.16 | 0.00 | | | | |

Summary for Reach R1: Existing Conditions

Inflow Area = 1.019 ac, 0.00% Impervious, Inflow Depth = 0.16" for 1-Year event
Inflow = 0.06 cfs @ 12.48 hrs, Volume= 0.014 af
Outflow = 0.06 cfs @ 12.48 hrs, Volume= 0.014 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R1: Existing Conditions

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Existing Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
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Hydrograph for Reach R1: Existing Conditions

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.00 | 0.00 | 0.00 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.00 | 0.00 | 0.00 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.00 | 0.00 | 0.00 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.00 | 0.00 | 0.00 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.00 | 0.00 | 0.00 |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.00 | 0.00 | 0.00 |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.00 | 0.00 | 0.00 |
| 8.00 | 0.00 | 0.00 | 0.00 | 59.00 | 0.00 | 0.00 | 0.00 |
| 9.00 | 0.00 | 0.00 | 0.00 | 60.00 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.00 | 0.00 | 0.00 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.00 | 0.00 | 0.00 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 0.00 | 0.00 | 0.00 | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.04 | 0.04 | 0.04 | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.02 | 0.02 | 0.02 | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.02 | 0.02 | 0.02 | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.01 | 0.01 | 0.01 | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.01 | 0.01 | 0.01 | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.01 | 0.01 | 0.01 | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.01 | 0.01 | 0.01 | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.01 | 0.01 | 0.01 | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.01 | 0.01 | 0.01 | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.01 | 0.01 | | | | | |
| 23.00 | 0.00 | 0.00 | | | | | |
| 24.00 | 0.00 | 0.00 | | | | | |
| 25.00 | 0.00 | 0.00 | | | | | |
| 26.00 | 0.00 | 0.00 | | | | | |
| 27.00 | 0.00 | 0.00 | | | | | |
| 28.00 | 0.00 | 0.00 | | | | | |
| 29.00 | 0.00 | 0.00 | | | | | |
| 30.00 | 0.00 | 0.00 | | | | | |
| 31.00 | 0.00 | 0.00 | | | | | |
| 32.00 | 0.00 | 0.00 | | | | | |
| 33.00 | 0.00 | 0.00 | | | | | |
| 34.00 | 0.00 | 0.00 | | | | | |
| 35.00 | 0.00 | 0.00 | | | | | |
| 36.00 | 0.00 | 0.00 | | | | | |
| 37.00 | 0.00 | 0.00 | | | | | |
| 38.00 | 0.00 | 0.00 | | | | | |
| 39.00 | 0.00 | 0.00 | | | | | |
| 40.00 | 0.00 | 0.00 | | | | | |
| 41.00 | 0.00 | 0.00 | | | | | |
| 42.00 | 0.00 | 0.00 | | | | | |
| 43.00 | 0.00 | 0.00 | | | | | |
| 44.00 | 0.00 | 0.00 | | | | | |
| 45.00 | 0.00 | 0.00 | | | | | |
| 46.00 | 0.00 | 0.00 | | | | | |
| 47.00 | 0.00 | 0.00 | | | | | |
| 48.00 | 0.00 | 0.00 | | | | | |
| 49.00 | 0.00 | 0.00 | | | | | |
| 50.00 | 0.00 | 0.00 | | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions
MSE 24-hr 4 2-Year Rainfall=3.00"
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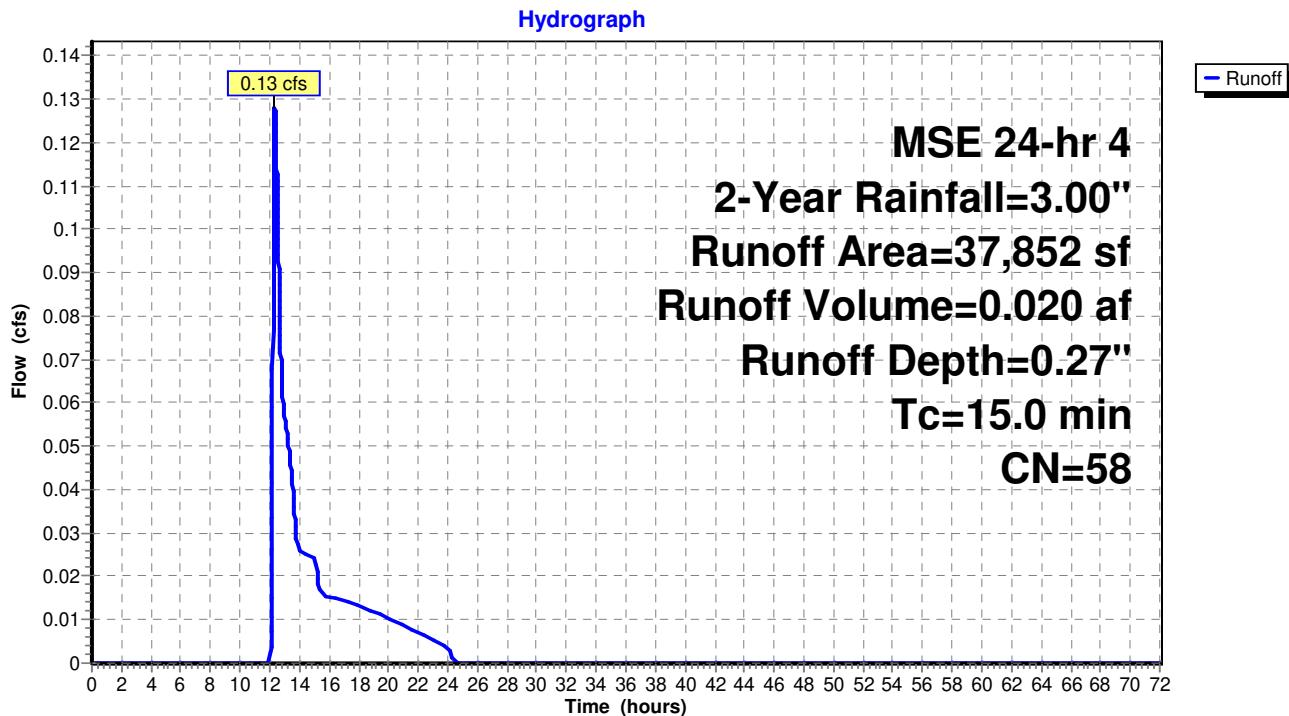
Summary for Subcatchment E-A1: Project Site

Runoff = 0.13 cfs @ 12.34 hrs, Volume= 0.020 af, Depth= 0.27"
Routed to Reach R1 : Existing Conditions

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 2-Year Rainfall=3.00"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 37,852 | 58 | Woods/grass comb., Good, HSG B |
| 37,852 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|-------------|
| 15.0 | Direct Entry, | | | | |

Subcatchment E-A1: Project Site

Retreat Center - Copy3

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Existing Conditions
MSE 24-hr 4 2-Year Rainfall=3.00"
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Hydrograph for Subcatchment E-A1: Project Site

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 3.00 | 0.27 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 3.00 | 0.27 | 0.00 |
| 2.00 | 0.04 | 0.00 | 0.00 | 53.00 | 3.00 | 0.27 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 3.00 | 0.27 | 0.00 |
| 4.00 | 0.10 | 0.00 | 0.00 | 55.00 | 3.00 | 0.27 | 0.00 |
| 5.00 | 0.14 | 0.00 | 0.00 | 56.00 | 3.00 | 0.27 | 0.00 |
| 6.00 | 0.18 | 0.00 | 0.00 | 57.00 | 3.00 | 0.27 | 0.00 |
| 7.00 | 0.24 | 0.00 | 0.00 | 58.00 | 3.00 | 0.27 | 0.00 |
| 8.00 | 0.30 | 0.00 | 0.00 | 59.00 | 3.00 | 0.27 | 0.00 |
| 9.00 | 0.36 | 0.00 | 0.00 | 60.00 | 3.00 | 0.27 | 0.00 |
| 10.00 | 0.48 | 0.00 | 0.00 | 61.00 | 3.00 | 0.27 | 0.00 |
| 11.00 | 0.65 | 0.00 | 0.00 | 62.00 | 3.00 | 0.27 | 0.00 |
| 12.00 | 1.41 | 0.00 | 0.00 | 63.00 | 3.00 | 0.27 | 0.00 |
| 13.00 | 2.35 | 0.10 | 0.06 | 64.00 | 3.00 | 0.27 | 0.00 |
| 14.00 | 2.52 | 0.14 | 0.03 | 65.00 | 3.00 | 0.27 | 0.00 |
| 15.00 | 2.64 | 0.17 | 0.02 | 66.00 | 3.00 | 0.27 | 0.00 |
| 16.00 | 2.70 | 0.19 | 0.02 | 67.00 | 3.00 | 0.27 | 0.00 |
| 17.00 | 2.76 | 0.20 | 0.01 | 68.00 | 3.00 | 0.27 | 0.00 |
| 18.00 | 2.82 | 0.22 | 0.01 | 69.00 | 3.00 | 0.27 | 0.00 |
| 19.00 | 2.86 | 0.23 | 0.01 | 70.00 | 3.00 | 0.27 | 0.00 |
| 20.00 | 2.90 | 0.24 | 0.01 | 71.00 | 3.00 | 0.27 | 0.00 |
| 21.00 | 2.94 | 0.25 | 0.01 | 72.00 | 3.00 | 0.27 | 0.00 |
| 22.00 | 2.96 | 0.26 | 0.01 | | | | |
| 23.00 | 2.99 | 0.27 | 0.01 | | | | |
| 24.00 | 3.00 | 0.27 | 0.00 | | | | |
| 25.00 | 3.00 | 0.27 | 0.00 | | | | |
| 26.00 | 3.00 | 0.27 | 0.00 | | | | |
| 27.00 | 3.00 | 0.27 | 0.00 | | | | |
| 28.00 | 3.00 | 0.27 | 0.00 | | | | |
| 29.00 | 3.00 | 0.27 | 0.00 | | | | |
| 30.00 | 3.00 | 0.27 | 0.00 | | | | |
| 31.00 | 3.00 | 0.27 | 0.00 | | | | |
| 32.00 | 3.00 | 0.27 | 0.00 | | | | |
| 33.00 | 3.00 | 0.27 | 0.00 | | | | |
| 34.00 | 3.00 | 0.27 | 0.00 | | | | |
| 35.00 | 3.00 | 0.27 | 0.00 | | | | |
| 36.00 | 3.00 | 0.27 | 0.00 | | | | |
| 37.00 | 3.00 | 0.27 | 0.00 | | | | |
| 38.00 | 3.00 | 0.27 | 0.00 | | | | |
| 39.00 | 3.00 | 0.27 | 0.00 | | | | |
| 40.00 | 3.00 | 0.27 | 0.00 | | | | |
| 41.00 | 3.00 | 0.27 | 0.00 | | | | |
| 42.00 | 3.00 | 0.27 | 0.00 | | | | |
| 43.00 | 3.00 | 0.27 | 0.00 | | | | |
| 44.00 | 3.00 | 0.27 | 0.00 | | | | |
| 45.00 | 3.00 | 0.27 | 0.00 | | | | |
| 46.00 | 3.00 | 0.27 | 0.00 | | | | |
| 47.00 | 3.00 | 0.27 | 0.00 | | | | |
| 48.00 | 3.00 | 0.27 | 0.00 | | | | |
| 49.00 | 3.00 | 0.27 | 0.00 | | | | |
| 50.00 | 3.00 | 0.27 | 0.00 | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions
MSE 24-hr 4 2-Year Rainfall=3.00"
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Summary for Subcatchment E-A2: Runon

Runoff = 0.02 cfs @ 12.34 hrs, Volume= 0.003 af, Depth= 0.27"
Routed to Reach R1 : Existing Conditions

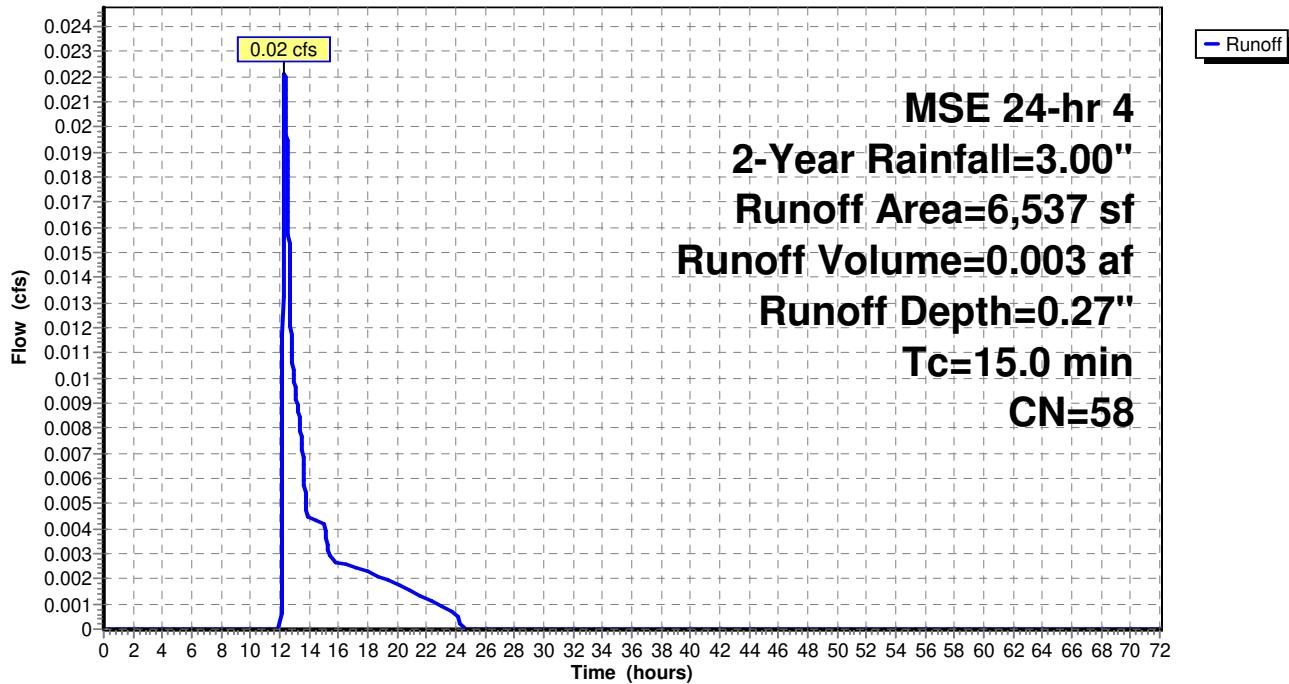
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 2-Year Rainfall=3.00"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 6,537 | 58 | Woods/grass comb., Good, HSG B |
| 6,537 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|-------------|
| 15.0 | Direct Entry, | | | | |

Subcatchment E-A2: Runon

Hydrograph



Retreat Center - Copy3

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Existing Conditions
MSE 24-hr 4 2-Year Rainfall=3.00"
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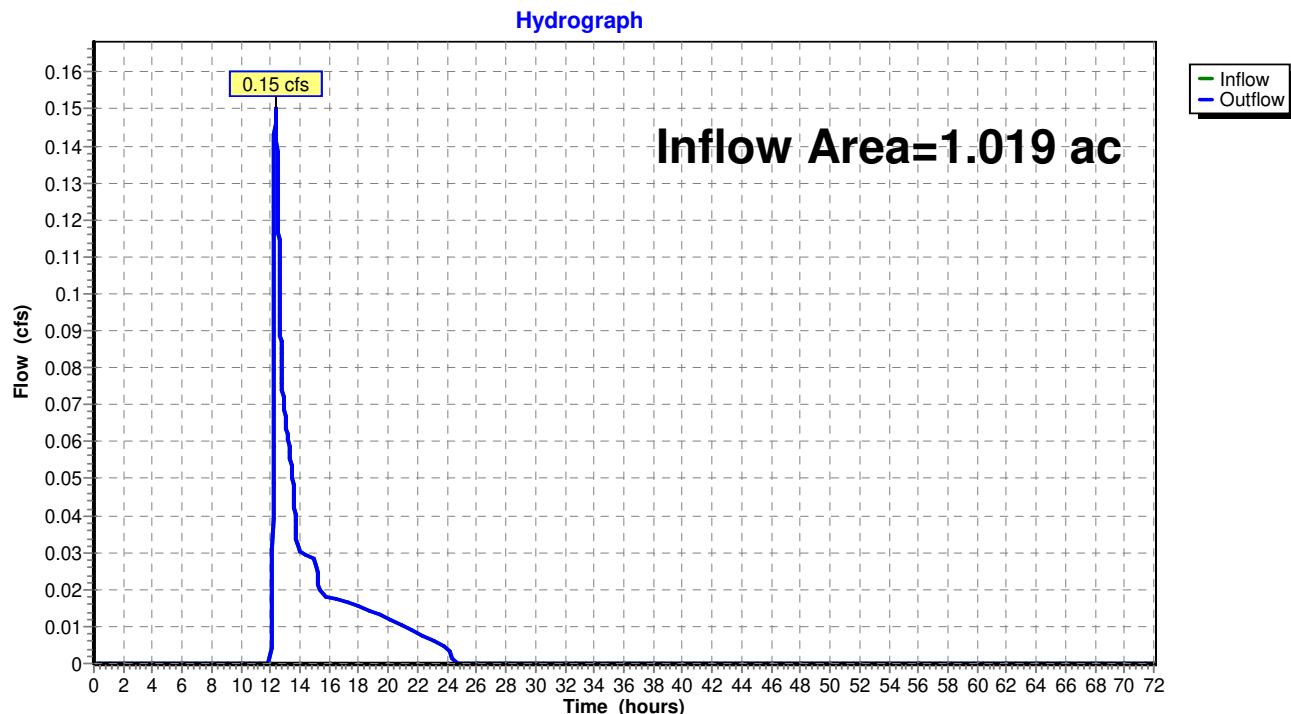
Hydrograph for Subcatchment E-A2: Runon

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 3.00 | 0.27 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 3.00 | 0.27 | 0.00 |
| 2.00 | 0.04 | 0.00 | 0.00 | 53.00 | 3.00 | 0.27 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 3.00 | 0.27 | 0.00 |
| 4.00 | 0.10 | 0.00 | 0.00 | 55.00 | 3.00 | 0.27 | 0.00 |
| 5.00 | 0.14 | 0.00 | 0.00 | 56.00 | 3.00 | 0.27 | 0.00 |
| 6.00 | 0.18 | 0.00 | 0.00 | 57.00 | 3.00 | 0.27 | 0.00 |
| 7.00 | 0.24 | 0.00 | 0.00 | 58.00 | 3.00 | 0.27 | 0.00 |
| 8.00 | 0.30 | 0.00 | 0.00 | 59.00 | 3.00 | 0.27 | 0.00 |
| 9.00 | 0.36 | 0.00 | 0.00 | 60.00 | 3.00 | 0.27 | 0.00 |
| 10.00 | 0.48 | 0.00 | 0.00 | 61.00 | 3.00 | 0.27 | 0.00 |
| 11.00 | 0.65 | 0.00 | 0.00 | 62.00 | 3.00 | 0.27 | 0.00 |
| 12.00 | 1.41 | 0.00 | 0.00 | 63.00 | 3.00 | 0.27 | 0.00 |
| 13.00 | 2.35 | 0.10 | 0.01 | 64.00 | 3.00 | 0.27 | 0.00 |
| 14.00 | 2.52 | 0.14 | 0.00 | 65.00 | 3.00 | 0.27 | 0.00 |
| 15.00 | 2.64 | 0.17 | 0.00 | 66.00 | 3.00 | 0.27 | 0.00 |
| 16.00 | 2.70 | 0.19 | 0.00 | 67.00 | 3.00 | 0.27 | 0.00 |
| 17.00 | 2.76 | 0.20 | 0.00 | 68.00 | 3.00 | 0.27 | 0.00 |
| 18.00 | 2.82 | 0.22 | 0.00 | 69.00 | 3.00 | 0.27 | 0.00 |
| 19.00 | 2.86 | 0.23 | 0.00 | 70.00 | 3.00 | 0.27 | 0.00 |
| 20.00 | 2.90 | 0.24 | 0.00 | 71.00 | 3.00 | 0.27 | 0.00 |
| 21.00 | 2.94 | 0.25 | 0.00 | 72.00 | 3.00 | 0.27 | 0.00 |
| 22.00 | 2.96 | 0.26 | 0.00 | | | | |
| 23.00 | 2.99 | 0.27 | 0.00 | | | | |
| 24.00 | 3.00 | 0.27 | 0.00 | | | | |
| 25.00 | 3.00 | 0.27 | 0.00 | | | | |
| 26.00 | 3.00 | 0.27 | 0.00 | | | | |
| 27.00 | 3.00 | 0.27 | 0.00 | | | | |
| 28.00 | 3.00 | 0.27 | 0.00 | | | | |
| 29.00 | 3.00 | 0.27 | 0.00 | | | | |
| 30.00 | 3.00 | 0.27 | 0.00 | | | | |
| 31.00 | 3.00 | 0.27 | 0.00 | | | | |
| 32.00 | 3.00 | 0.27 | 0.00 | | | | |
| 33.00 | 3.00 | 0.27 | 0.00 | | | | |
| 34.00 | 3.00 | 0.27 | 0.00 | | | | |
| 35.00 | 3.00 | 0.27 | 0.00 | | | | |
| 36.00 | 3.00 | 0.27 | 0.00 | | | | |
| 37.00 | 3.00 | 0.27 | 0.00 | | | | |
| 38.00 | 3.00 | 0.27 | 0.00 | | | | |
| 39.00 | 3.00 | 0.27 | 0.00 | | | | |
| 40.00 | 3.00 | 0.27 | 0.00 | | | | |
| 41.00 | 3.00 | 0.27 | 0.00 | | | | |
| 42.00 | 3.00 | 0.27 | 0.00 | | | | |
| 43.00 | 3.00 | 0.27 | 0.00 | | | | |
| 44.00 | 3.00 | 0.27 | 0.00 | | | | |
| 45.00 | 3.00 | 0.27 | 0.00 | | | | |
| 46.00 | 3.00 | 0.27 | 0.00 | | | | |
| 47.00 | 3.00 | 0.27 | 0.00 | | | | |
| 48.00 | 3.00 | 0.27 | 0.00 | | | | |
| 49.00 | 3.00 | 0.27 | 0.00 | | | | |
| 50.00 | 3.00 | 0.27 | 0.00 | | | | |

Summary for Reach R1: Existing Conditions

Inflow Area = 1.019 ac, 0.00% Impervious, Inflow Depth = 0.27" for 2-Year event
Inflow = 0.15 cfs @ 12.34 hrs, Volume= 0.023 af
Outflow = 0.15 cfs @ 12.34 hrs, Volume= 0.023 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R1: Existing Conditions

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions
MSE 24-hr 4 2-Year Rainfall=3.00"
Printed 9/16/2024
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Hydrograph for Reach R1: Existing Conditions

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.00 | 0.00 | 0.00 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.00 | 0.00 | 0.00 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.00 | 0.00 | 0.00 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.00 | 0.00 | 0.00 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.00 | 0.00 | 0.00 |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.00 | 0.00 | 0.00 |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.00 | 0.00 | 0.00 |
| 8.00 | 0.00 | 0.00 | 0.00 | 59.00 | 0.00 | 0.00 | 0.00 |
| 9.00 | 0.00 | 0.00 | 0.00 | 60.00 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.00 | 0.00 | 0.00 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.00 | 0.00 | 0.00 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 0.00 | 0.00 | | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.07 | 0.07 | | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.03 | 0.03 | | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.03 | 0.03 | | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.02 | 0.02 | | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.02 | 0.02 | | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.02 | 0.02 | | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.01 | 0.01 | | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.01 | 0.01 | | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.01 | 0.01 | | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.01 | 0.01 | | | | | |
| 23.00 | 0.01 | 0.01 | | | | | |
| 24.00 | 0.00 | 0.00 | | | | | |
| 25.00 | 0.00 | 0.00 | | | | | |
| 26.00 | 0.00 | 0.00 | | | | | |
| 27.00 | 0.00 | 0.00 | | | | | |
| 28.00 | 0.00 | 0.00 | | | | | |
| 29.00 | 0.00 | 0.00 | | | | | |
| 30.00 | 0.00 | 0.00 | | | | | |
| 31.00 | 0.00 | 0.00 | | | | | |
| 32.00 | 0.00 | 0.00 | | | | | |
| 33.00 | 0.00 | 0.00 | | | | | |
| 34.00 | 0.00 | 0.00 | | | | | |
| 35.00 | 0.00 | 0.00 | | | | | |
| 36.00 | 0.00 | 0.00 | | | | | |
| 37.00 | 0.00 | 0.00 | | | | | |
| 38.00 | 0.00 | 0.00 | | | | | |
| 39.00 | 0.00 | 0.00 | | | | | |
| 40.00 | 0.00 | 0.00 | | | | | |
| 41.00 | 0.00 | 0.00 | | | | | |
| 42.00 | 0.00 | 0.00 | | | | | |
| 43.00 | 0.00 | 0.00 | | | | | |
| 44.00 | 0.00 | 0.00 | | | | | |
| 45.00 | 0.00 | 0.00 | | | | | |
| 46.00 | 0.00 | 0.00 | | | | | |
| 47.00 | 0.00 | 0.00 | | | | | |
| 48.00 | 0.00 | 0.00 | | | | | |
| 49.00 | 0.00 | 0.00 | | | | | |
| 50.00 | 0.00 | 0.00 | | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

MSE 24-hr 4 10-Year Rainfall=4.44"

Printed 9/16/2024

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Summary for Subcatchment E-A1: Project Site

Runoff = 0.72 cfs @ 12.26 hrs, Volume= 0.063 af, Depth= 0.87"
Routed to Reach R1 : Existing Conditions

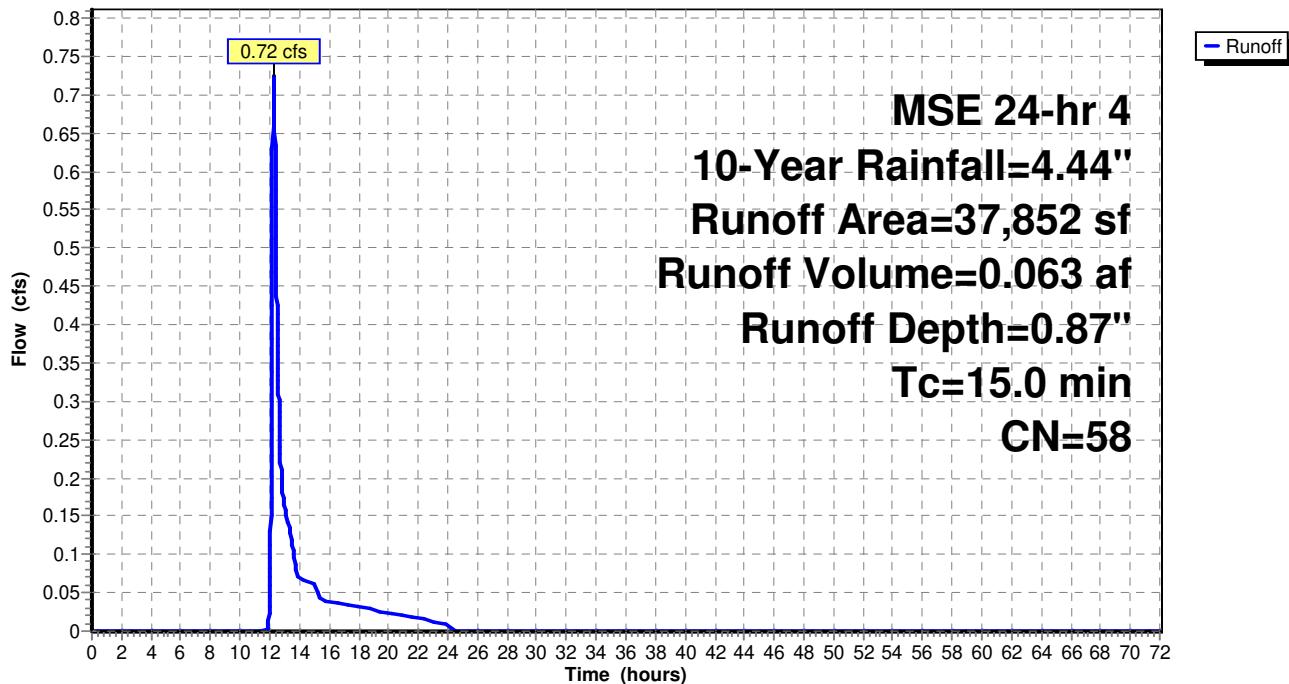
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 10-Year Rainfall=4.44"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 37,852 | 58 | Woods/grass comb., Good, HSG B |
| 37,852 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|-------------|
| 15.0 | Direct Entry, | | | | |

Subcatchment E-A1: Project Site

Hydrograph



Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

MSE 24-hr 4 10-Year Rainfall=4.44"

Printed 9/16/2024

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Hydrograph for Subcatchment E-A1: Project Site

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 4.44 | 0.87 | 0.00 |
| 1.00 | 0.02 | 0.00 | 0.00 | 52.00 | 4.44 | 0.87 | 0.00 |
| 2.00 | 0.05 | 0.00 | 0.00 | 53.00 | 4.44 | 0.87 | 0.00 |
| 3.00 | 0.09 | 0.00 | 0.00 | 54.00 | 4.44 | 0.87 | 0.00 |
| 4.00 | 0.14 | 0.00 | 0.00 | 55.00 | 4.44 | 0.87 | 0.00 |
| 5.00 | 0.20 | 0.00 | 0.00 | 56.00 | 4.44 | 0.87 | 0.00 |
| 6.00 | 0.27 | 0.00 | 0.00 | 57.00 | 4.44 | 0.87 | 0.00 |
| 7.00 | 0.35 | 0.00 | 0.00 | 58.00 | 4.44 | 0.87 | 0.00 |
| 8.00 | 0.44 | 0.00 | 0.00 | 59.00 | 4.44 | 0.87 | 0.00 |
| 9.00 | 0.54 | 0.00 | 0.00 | 60.00 | 4.44 | 0.87 | 0.00 |
| 10.00 | 0.70 | 0.00 | 0.00 | 61.00 | 4.44 | 0.87 | 0.00 |
| 11.00 | 0.96 | 0.00 | 0.00 | 62.00 | 4.44 | 0.87 | 0.00 |
| 12.00 | 2.08 | 0.05 | 0.05 | 63.00 | 4.44 | 0.87 | 0.00 |
| 13.00 | 3.48 | 0.45 | 0.16 | 64.00 | 4.44 | 0.87 | 0.00 |
| 14.00 | 3.74 | 0.55 | 0.07 | 65.00 | 4.44 | 0.87 | 0.00 |
| 15.00 | 3.90 | 0.62 | 0.06 | 66.00 | 4.44 | 0.87 | 0.00 |
| 16.00 | 4.00 | 0.66 | 0.04 | 67.00 | 4.44 | 0.87 | 0.00 |
| 17.00 | 4.09 | 0.71 | 0.03 | 68.00 | 4.44 | 0.87 | 0.00 |
| 18.00 | 4.17 | 0.74 | 0.03 | 69.00 | 4.44 | 0.87 | 0.00 |
| 19.00 | 4.24 | 0.77 | 0.03 | 70.00 | 4.44 | 0.87 | 0.00 |
| 20.00 | 4.30 | 0.80 | 0.02 | 71.00 | 4.44 | 0.87 | 0.00 |
| 21.00 | 4.35 | 0.83 | 0.02 | 72.00 | 4.44 | 0.87 | 0.00 |
| 22.00 | 4.39 | 0.85 | 0.02 | | | | |
| 23.00 | 4.42 | 0.86 | 0.01 | | | | |
| 24.00 | 4.44 | 0.87 | 0.01 | | | | |
| 25.00 | 4.44 | 0.87 | 0.00 | | | | |
| 26.00 | 4.44 | 0.87 | 0.00 | | | | |
| 27.00 | 4.44 | 0.87 | 0.00 | | | | |
| 28.00 | 4.44 | 0.87 | 0.00 | | | | |
| 29.00 | 4.44 | 0.87 | 0.00 | | | | |
| 30.00 | 4.44 | 0.87 | 0.00 | | | | |
| 31.00 | 4.44 | 0.87 | 0.00 | | | | |
| 32.00 | 4.44 | 0.87 | 0.00 | | | | |
| 33.00 | 4.44 | 0.87 | 0.00 | | | | |
| 34.00 | 4.44 | 0.87 | 0.00 | | | | |
| 35.00 | 4.44 | 0.87 | 0.00 | | | | |
| 36.00 | 4.44 | 0.87 | 0.00 | | | | |
| 37.00 | 4.44 | 0.87 | 0.00 | | | | |
| 38.00 | 4.44 | 0.87 | 0.00 | | | | |
| 39.00 | 4.44 | 0.87 | 0.00 | | | | |
| 40.00 | 4.44 | 0.87 | 0.00 | | | | |
| 41.00 | 4.44 | 0.87 | 0.00 | | | | |
| 42.00 | 4.44 | 0.87 | 0.00 | | | | |
| 43.00 | 4.44 | 0.87 | 0.00 | | | | |
| 44.00 | 4.44 | 0.87 | 0.00 | | | | |
| 45.00 | 4.44 | 0.87 | 0.00 | | | | |
| 46.00 | 4.44 | 0.87 | 0.00 | | | | |
| 47.00 | 4.44 | 0.87 | 0.00 | | | | |
| 48.00 | 4.44 | 0.87 | 0.00 | | | | |
| 49.00 | 4.44 | 0.87 | 0.00 | | | | |
| 50.00 | 4.44 | 0.87 | 0.00 | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

MSE 24-hr 4 10-Year Rainfall=4.44"

Printed 9/16/2024

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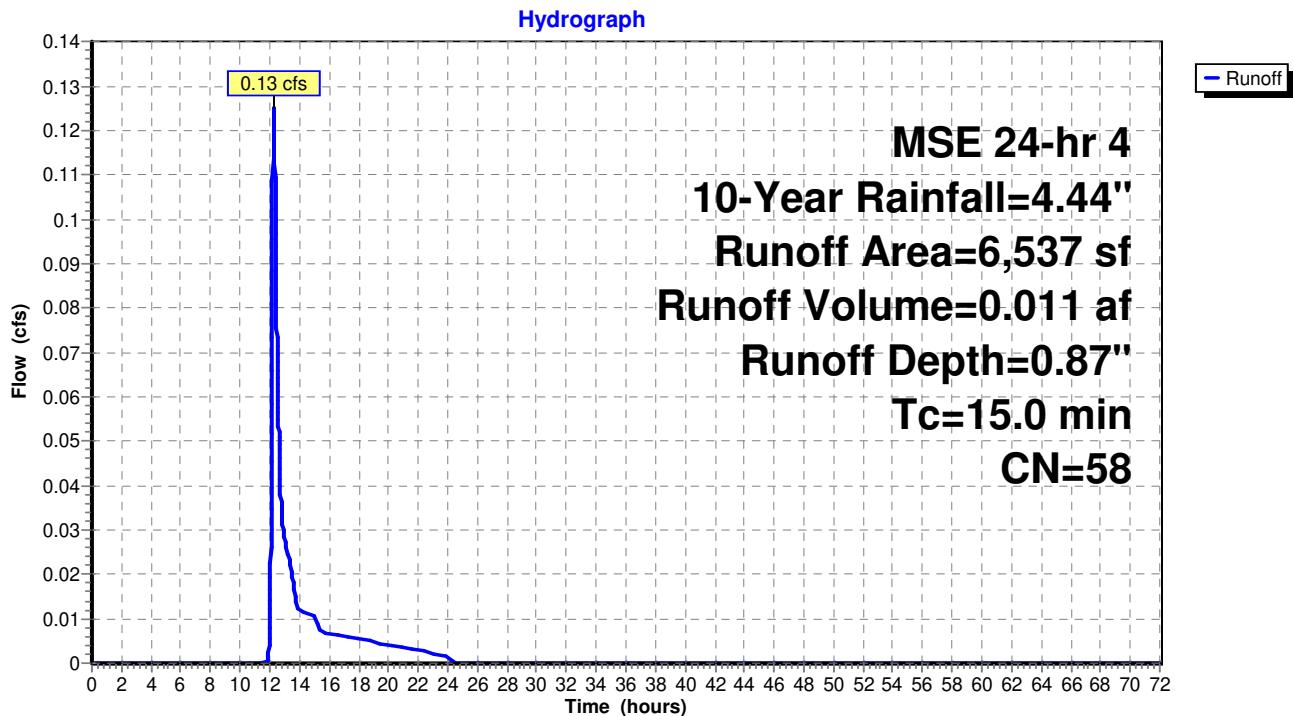
Summary for Subcatchment E-A2: Runon

Runoff = 0.13 cfs @ 12.26 hrs, Volume= 0.011 af, Depth= 0.87"
Routed to Reach R1 : Existing Conditions

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 10-Year Rainfall=4.44"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 6,537 | 58 | Woods/grass comb., Good, HSG B |
| 6,537 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|---------------|
| 15.0 | | | | | Direct Entry, |

Subcatchment E-A2: Runon

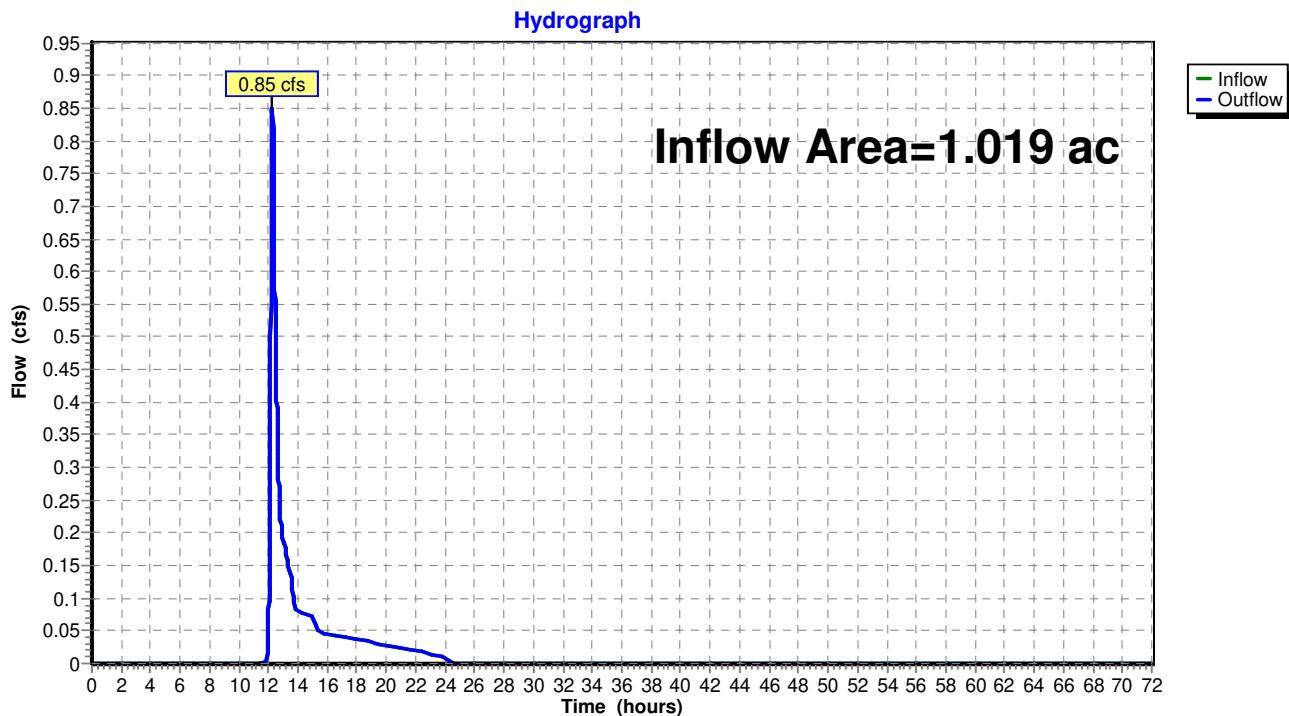
Hydrograph for Subcatchment E-A2: Runon

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 4.44 | 0.87 | 0.00 |
| 1.00 | 0.02 | 0.00 | 0.00 | 52.00 | 4.44 | 0.87 | 0.00 |
| 2.00 | 0.05 | 0.00 | 0.00 | 53.00 | 4.44 | 0.87 | 0.00 |
| 3.00 | 0.09 | 0.00 | 0.00 | 54.00 | 4.44 | 0.87 | 0.00 |
| 4.00 | 0.14 | 0.00 | 0.00 | 55.00 | 4.44 | 0.87 | 0.00 |
| 5.00 | 0.20 | 0.00 | 0.00 | 56.00 | 4.44 | 0.87 | 0.00 |
| 6.00 | 0.27 | 0.00 | 0.00 | 57.00 | 4.44 | 0.87 | 0.00 |
| 7.00 | 0.35 | 0.00 | 0.00 | 58.00 | 4.44 | 0.87 | 0.00 |
| 8.00 | 0.44 | 0.00 | 0.00 | 59.00 | 4.44 | 0.87 | 0.00 |
| 9.00 | 0.54 | 0.00 | 0.00 | 60.00 | 4.44 | 0.87 | 0.00 |
| 10.00 | 0.70 | 0.00 | 0.00 | 61.00 | 4.44 | 0.87 | 0.00 |
| 11.00 | 0.96 | 0.00 | 0.00 | 62.00 | 4.44 | 0.87 | 0.00 |
| 12.00 | 2.08 | 0.05 | 0.01 | 63.00 | 4.44 | 0.87 | 0.00 |
| 13.00 | 3.48 | 0.45 | 0.03 | 64.00 | 4.44 | 0.87 | 0.00 |
| 14.00 | 3.74 | 0.55 | 0.01 | 65.00 | 4.44 | 0.87 | 0.00 |
| 15.00 | 3.90 | 0.62 | 0.01 | 66.00 | 4.44 | 0.87 | 0.00 |
| 16.00 | 4.00 | 0.66 | 0.01 | 67.00 | 4.44 | 0.87 | 0.00 |
| 17.00 | 4.09 | 0.71 | 0.01 | 68.00 | 4.44 | 0.87 | 0.00 |
| 18.00 | 4.17 | 0.74 | 0.01 | 69.00 | 4.44 | 0.87 | 0.00 |
| 19.00 | 4.24 | 0.77 | 0.00 | 70.00 | 4.44 | 0.87 | 0.00 |
| 20.00 | 4.30 | 0.80 | 0.00 | 71.00 | 4.44 | 0.87 | 0.00 |
| 21.00 | 4.35 | 0.83 | 0.00 | 72.00 | 4.44 | 0.87 | 0.00 |
| 22.00 | 4.39 | 0.85 | 0.00 | | | | |
| 23.00 | 4.42 | 0.86 | 0.00 | | | | |
| 24.00 | 4.44 | 0.87 | 0.00 | | | | |
| 25.00 | 4.44 | 0.87 | 0.00 | | | | |
| 26.00 | 4.44 | 0.87 | 0.00 | | | | |
| 27.00 | 4.44 | 0.87 | 0.00 | | | | |
| 28.00 | 4.44 | 0.87 | 0.00 | | | | |
| 29.00 | 4.44 | 0.87 | 0.00 | | | | |
| 30.00 | 4.44 | 0.87 | 0.00 | | | | |
| 31.00 | 4.44 | 0.87 | 0.00 | | | | |
| 32.00 | 4.44 | 0.87 | 0.00 | | | | |
| 33.00 | 4.44 | 0.87 | 0.00 | | | | |
| 34.00 | 4.44 | 0.87 | 0.00 | | | | |
| 35.00 | 4.44 | 0.87 | 0.00 | | | | |
| 36.00 | 4.44 | 0.87 | 0.00 | | | | |
| 37.00 | 4.44 | 0.87 | 0.00 | | | | |
| 38.00 | 4.44 | 0.87 | 0.00 | | | | |
| 39.00 | 4.44 | 0.87 | 0.00 | | | | |
| 40.00 | 4.44 | 0.87 | 0.00 | | | | |
| 41.00 | 4.44 | 0.87 | 0.00 | | | | |
| 42.00 | 4.44 | 0.87 | 0.00 | | | | |
| 43.00 | 4.44 | 0.87 | 0.00 | | | | |
| 44.00 | 4.44 | 0.87 | 0.00 | | | | |
| 45.00 | 4.44 | 0.87 | 0.00 | | | | |
| 46.00 | 4.44 | 0.87 | 0.00 | | | | |
| 47.00 | 4.44 | 0.87 | 0.00 | | | | |
| 48.00 | 4.44 | 0.87 | 0.00 | | | | |
| 49.00 | 4.44 | 0.87 | 0.00 | | | | |
| 50.00 | 4.44 | 0.87 | 0.00 | | | | |

Summary for Reach R1: Existing Conditions

Inflow Area = 1.019 ac, 0.00% Impervious, Inflow Depth = 0.87" for 10-Year event
Inflow = 0.85 cfs @ 12.26 hrs, Volume= 0.074 af
Outflow = 0.85 cfs @ 12.26 hrs, Volume= 0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R1: Existing Conditions

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions
MSE 24-hr 4 10-Year Rainfall=4.44"
Printed 9/16/2024
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Hydrograph for Reach R1: Existing Conditions

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.00 | 0.00 | 0.00 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.00 | 0.00 | 0.00 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.00 | 0.00 | 0.00 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.00 | 0.00 | 0.00 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.00 | 0.00 | 0.00 |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.00 | 0.00 | 0.00 |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.00 | 0.00 | 0.00 |
| 8.00 | 0.00 | 0.00 | 0.00 | 59.00 | 0.00 | 0.00 | 0.00 |
| 9.00 | 0.00 | 0.00 | 0.00 | 60.00 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.00 | 0.00 | 0.00 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.00 | 0.00 | 0.00 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 0.06 | 0.06 | | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.19 | 0.19 | | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.08 | 0.08 | | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.07 | 0.07 | | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.04 | 0.04 | | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.04 | 0.04 | | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.04 | 0.04 | | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.03 | 0.03 | | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.03 | 0.03 | | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.02 | 0.02 | | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.02 | 0.02 | | | | | |
| 23.00 | 0.01 | 0.01 | | | | | |
| 24.00 | 0.01 | 0.01 | | | | | |
| 25.00 | 0.00 | 0.00 | | | | | |
| 26.00 | 0.00 | 0.00 | | | | | |
| 27.00 | 0.00 | 0.00 | | | | | |
| 28.00 | 0.00 | 0.00 | | | | | |
| 29.00 | 0.00 | 0.00 | | | | | |
| 30.00 | 0.00 | 0.00 | | | | | |
| 31.00 | 0.00 | 0.00 | | | | | |
| 32.00 | 0.00 | 0.00 | | | | | |
| 33.00 | 0.00 | 0.00 | | | | | |
| 34.00 | 0.00 | 0.00 | | | | | |
| 35.00 | 0.00 | 0.00 | | | | | |
| 36.00 | 0.00 | 0.00 | | | | | |
| 37.00 | 0.00 | 0.00 | | | | | |
| 38.00 | 0.00 | 0.00 | | | | | |
| 39.00 | 0.00 | 0.00 | | | | | |
| 40.00 | 0.00 | 0.00 | | | | | |
| 41.00 | 0.00 | 0.00 | | | | | |
| 42.00 | 0.00 | 0.00 | | | | | |
| 43.00 | 0.00 | 0.00 | | | | | |
| 44.00 | 0.00 | 0.00 | | | | | |
| 45.00 | 0.00 | 0.00 | | | | | |
| 46.00 | 0.00 | 0.00 | | | | | |
| 47.00 | 0.00 | 0.00 | | | | | |
| 48.00 | 0.00 | 0.00 | | | | | |
| 49.00 | 0.00 | 0.00 | | | | | |
| 50.00 | 0.00 | 0.00 | | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

MSE 24-hr 4 100-Year Rainfall=7.60"

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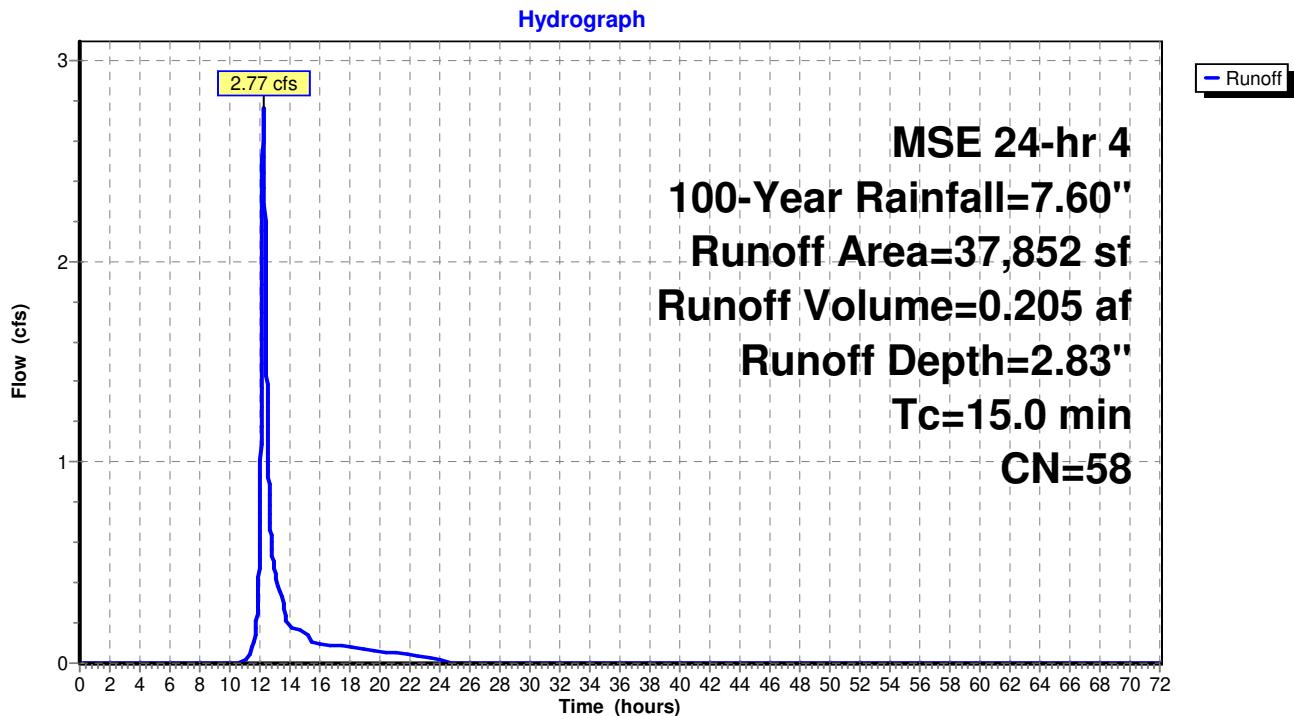
Summary for Subcatchment E-A1: Project Site

Runoff = 2.77 cfs @ 12.24 hrs, Volume= 0.205 af, Depth= 2.83"
Routed to Reach R1 : Existing Conditions

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 100-Year Rainfall=7.60"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 37,852 | 58 | Woods/grass comb., Good, HSG B |
| 37,852 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|---------------|
| 15.0 | | | | | Direct Entry, |

Subcatchment E-A1: Project Site

Retreat Center - Copy3

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Existing Conditions

MSE 24-hr 4 100-Year Rainfall=7.60"

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Hydrograph for Subcatchment E-A1: Project Site

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 7.60 | 2.83 | 0.00 |
| 1.00 | 0.04 | 0.00 | 0.00 | 52.00 | 7.60 | 2.83 | 0.00 |
| 2.00 | 0.09 | 0.00 | 0.00 | 53.00 | 7.60 | 2.83 | 0.00 |
| 3.00 | 0.16 | 0.00 | 0.00 | 54.00 | 7.60 | 2.83 | 0.00 |
| 4.00 | 0.25 | 0.00 | 0.00 | 55.00 | 7.60 | 2.83 | 0.00 |
| 5.00 | 0.35 | 0.00 | 0.00 | 56.00 | 7.60 | 2.83 | 0.00 |
| 6.00 | 0.47 | 0.00 | 0.00 | 57.00 | 7.60 | 2.83 | 0.00 |
| 7.00 | 0.60 | 0.00 | 0.00 | 58.00 | 7.60 | 2.83 | 0.00 |
| 8.00 | 0.75 | 0.00 | 0.00 | 59.00 | 7.60 | 2.83 | 0.00 |
| 9.00 | 0.92 | 0.00 | 0.00 | 60.00 | 7.60 | 2.83 | 0.00 |
| 10.00 | 1.20 | 0.00 | 0.00 | 61.00 | 7.60 | 2.83 | 0.00 |
| 11.00 | 1.64 | 0.01 | 0.01 | 62.00 | 7.60 | 2.83 | 0.00 |
| 12.00 | 3.56 | 0.48 | 0.66 | 63.00 | 7.60 | 2.83 | 0.00 |
| 13.00 | 5.96 | 1.73 | 0.45 | 64.00 | 7.60 | 2.83 | 0.00 |
| 14.00 | 6.40 | 2.01 | 0.18 | 65.00 | 7.60 | 2.83 | 0.00 |
| 15.00 | 6.68 | 2.19 | 0.16 | 66.00 | 7.60 | 2.83 | 0.00 |
| 16.00 | 6.85 | 2.31 | 0.10 | 67.00 | 7.60 | 2.83 | 0.00 |
| 17.00 | 7.00 | 2.41 | 0.09 | 68.00 | 7.60 | 2.83 | 0.00 |
| 18.00 | 7.13 | 2.50 | 0.08 | 69.00 | 7.60 | 2.83 | 0.00 |
| 19.00 | 7.25 | 2.58 | 0.07 | 70.00 | 7.60 | 2.83 | 0.00 |
| 20.00 | 7.35 | 2.65 | 0.06 | 71.00 | 7.60 | 2.83 | 0.00 |
| 21.00 | 7.44 | 2.71 | 0.05 | 72.00 | 7.60 | 2.83 | 0.00 |
| 22.00 | 7.51 | 2.76 | 0.04 | | | | |
| 23.00 | 7.56 | 2.80 | 0.03 | | | | |
| 24.00 | 7.60 | 2.83 | 0.02 | | | | |
| 25.00 | 7.60 | 2.83 | 0.00 | | | | |
| 26.00 | 7.60 | 2.83 | 0.00 | | | | |
| 27.00 | 7.60 | 2.83 | 0.00 | | | | |
| 28.00 | 7.60 | 2.83 | 0.00 | | | | |
| 29.00 | 7.60 | 2.83 | 0.00 | | | | |
| 30.00 | 7.60 | 2.83 | 0.00 | | | | |
| 31.00 | 7.60 | 2.83 | 0.00 | | | | |
| 32.00 | 7.60 | 2.83 | 0.00 | | | | |
| 33.00 | 7.60 | 2.83 | 0.00 | | | | |
| 34.00 | 7.60 | 2.83 | 0.00 | | | | |
| 35.00 | 7.60 | 2.83 | 0.00 | | | | |
| 36.00 | 7.60 | 2.83 | 0.00 | | | | |
| 37.00 | 7.60 | 2.83 | 0.00 | | | | |
| 38.00 | 7.60 | 2.83 | 0.00 | | | | |
| 39.00 | 7.60 | 2.83 | 0.00 | | | | |
| 40.00 | 7.60 | 2.83 | 0.00 | | | | |
| 41.00 | 7.60 | 2.83 | 0.00 | | | | |
| 42.00 | 7.60 | 2.83 | 0.00 | | | | |
| 43.00 | 7.60 | 2.83 | 0.00 | | | | |
| 44.00 | 7.60 | 2.83 | 0.00 | | | | |
| 45.00 | 7.60 | 2.83 | 0.00 | | | | |
| 46.00 | 7.60 | 2.83 | 0.00 | | | | |
| 47.00 | 7.60 | 2.83 | 0.00 | | | | |
| 48.00 | 7.60 | 2.83 | 0.00 | | | | |
| 49.00 | 7.60 | 2.83 | 0.00 | | | | |
| 50.00 | 7.60 | 2.83 | 0.00 | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Existing Conditions

MSE 24-hr 4 100-Year Rainfall=7.60"

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Summary for Subcatchment E-A2: Runon

Runoff = 0.48 cfs @ 12.24 hrs, Volume= 0.035 af, Depth= 2.83"
Routed to Reach R1 : Existing Conditions

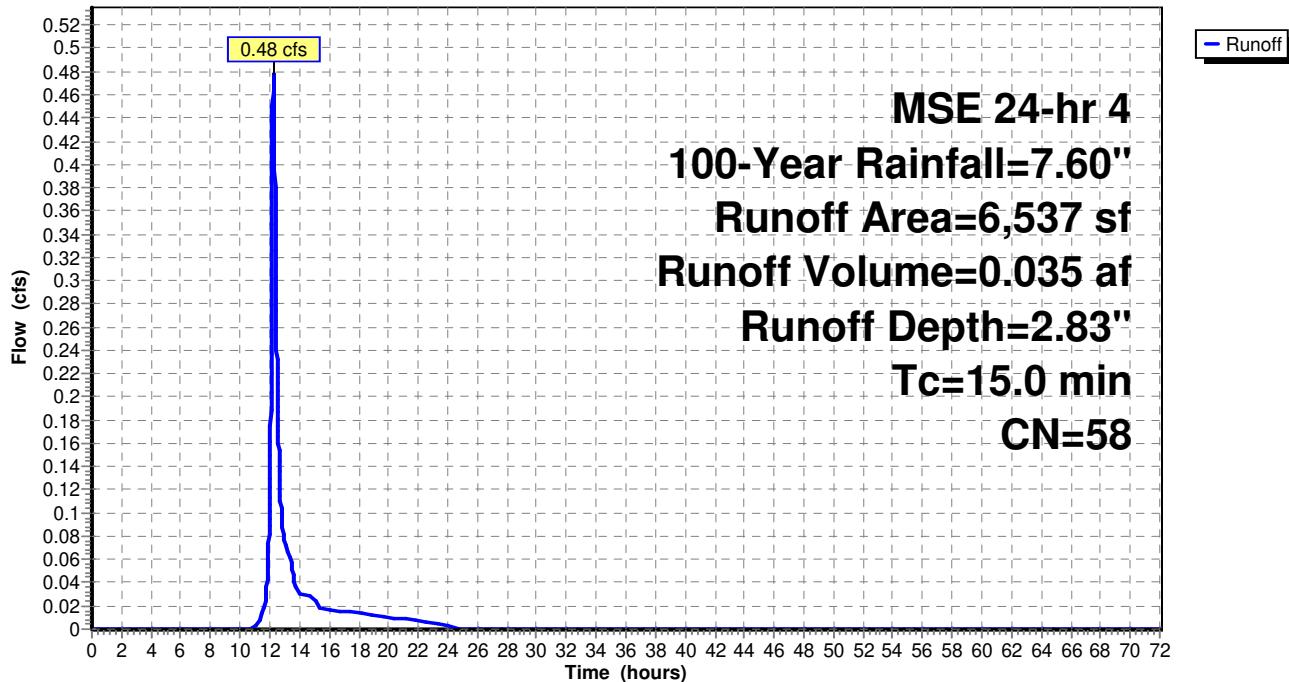
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 100-Year Rainfall=7.60"

| Area (sf) | CN | Description |
|-----------|----|--------------------------------|
| 6,537 | 58 | Woods/grass comb., Good, HSG B |
| 6,537 | | 100.00% Pervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|------|------------------|------------------|----------------------|-------------------|---------------|
| 15.0 | | | | | Direct Entry, |

Subcatchment E-A2: Runon

Hydrograph



Retreat Center - Copy3

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Existing Conditions

MSE 24-hr 4 100-Year Rainfall=7.60"

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Hydrograph for Subcatchment E-A2: Runon

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 7.60 | 2.83 | 0.00 |
| 1.00 | 0.04 | 0.00 | 0.00 | 52.00 | 7.60 | 2.83 | 0.00 |
| 2.00 | 0.09 | 0.00 | 0.00 | 53.00 | 7.60 | 2.83 | 0.00 |
| 3.00 | 0.16 | 0.00 | 0.00 | 54.00 | 7.60 | 2.83 | 0.00 |
| 4.00 | 0.25 | 0.00 | 0.00 | 55.00 | 7.60 | 2.83 | 0.00 |
| 5.00 | 0.35 | 0.00 | 0.00 | 56.00 | 7.60 | 2.83 | 0.00 |
| 6.00 | 0.47 | 0.00 | 0.00 | 57.00 | 7.60 | 2.83 | 0.00 |
| 7.00 | 0.60 | 0.00 | 0.00 | 58.00 | 7.60 | 2.83 | 0.00 |
| 8.00 | 0.75 | 0.00 | 0.00 | 59.00 | 7.60 | 2.83 | 0.00 |
| 9.00 | 0.92 | 0.00 | 0.00 | 60.00 | 7.60 | 2.83 | 0.00 |
| 10.00 | 1.20 | 0.00 | 0.00 | 61.00 | 7.60 | 2.83 | 0.00 |
| 11.00 | 1.64 | 0.01 | 0.00 | 62.00 | 7.60 | 2.83 | 0.00 |
| 12.00 | 3.56 | 0.48 | 0.11 | 63.00 | 7.60 | 2.83 | 0.00 |
| 13.00 | 5.96 | 1.73 | 0.08 | 64.00 | 7.60 | 2.83 | 0.00 |
| 14.00 | 6.40 | 2.01 | 0.03 | 65.00 | 7.60 | 2.83 | 0.00 |
| 15.00 | 6.68 | 2.19 | 0.03 | 66.00 | 7.60 | 2.83 | 0.00 |
| 16.00 | 6.85 | 2.31 | 0.02 | 67.00 | 7.60 | 2.83 | 0.00 |
| 17.00 | 7.00 | 2.41 | 0.02 | 68.00 | 7.60 | 2.83 | 0.00 |
| 18.00 | 7.13 | 2.50 | 0.01 | 69.00 | 7.60 | 2.83 | 0.00 |
| 19.00 | 7.25 | 2.58 | 0.01 | 70.00 | 7.60 | 2.83 | 0.00 |
| 20.00 | 7.35 | 2.65 | 0.01 | 71.00 | 7.60 | 2.83 | 0.00 |
| 21.00 | 7.44 | 2.71 | 0.01 | 72.00 | 7.60 | 2.83 | 0.00 |
| 22.00 | 7.51 | 2.76 | 0.01 | | | | |
| 23.00 | 7.56 | 2.80 | 0.01 | | | | |
| 24.00 | 7.60 | 2.83 | 0.00 | | | | |
| 25.00 | 7.60 | 2.83 | 0.00 | | | | |
| 26.00 | 7.60 | 2.83 | 0.00 | | | | |
| 27.00 | 7.60 | 2.83 | 0.00 | | | | |
| 28.00 | 7.60 | 2.83 | 0.00 | | | | |
| 29.00 | 7.60 | 2.83 | 0.00 | | | | |
| 30.00 | 7.60 | 2.83 | 0.00 | | | | |
| 31.00 | 7.60 | 2.83 | 0.00 | | | | |
| 32.00 | 7.60 | 2.83 | 0.00 | | | | |
| 33.00 | 7.60 | 2.83 | 0.00 | | | | |
| 34.00 | 7.60 | 2.83 | 0.00 | | | | |
| 35.00 | 7.60 | 2.83 | 0.00 | | | | |
| 36.00 | 7.60 | 2.83 | 0.00 | | | | |
| 37.00 | 7.60 | 2.83 | 0.00 | | | | |
| 38.00 | 7.60 | 2.83 | 0.00 | | | | |
| 39.00 | 7.60 | 2.83 | 0.00 | | | | |
| 40.00 | 7.60 | 2.83 | 0.00 | | | | |
| 41.00 | 7.60 | 2.83 | 0.00 | | | | |
| 42.00 | 7.60 | 2.83 | 0.00 | | | | |
| 43.00 | 7.60 | 2.83 | 0.00 | | | | |
| 44.00 | 7.60 | 2.83 | 0.00 | | | | |
| 45.00 | 7.60 | 2.83 | 0.00 | | | | |
| 46.00 | 7.60 | 2.83 | 0.00 | | | | |
| 47.00 | 7.60 | 2.83 | 0.00 | | | | |
| 48.00 | 7.60 | 2.83 | 0.00 | | | | |
| 49.00 | 7.60 | 2.83 | 0.00 | | | | |
| 50.00 | 7.60 | 2.83 | 0.00 | | | | |

Summary for Reach R1: Existing Conditions

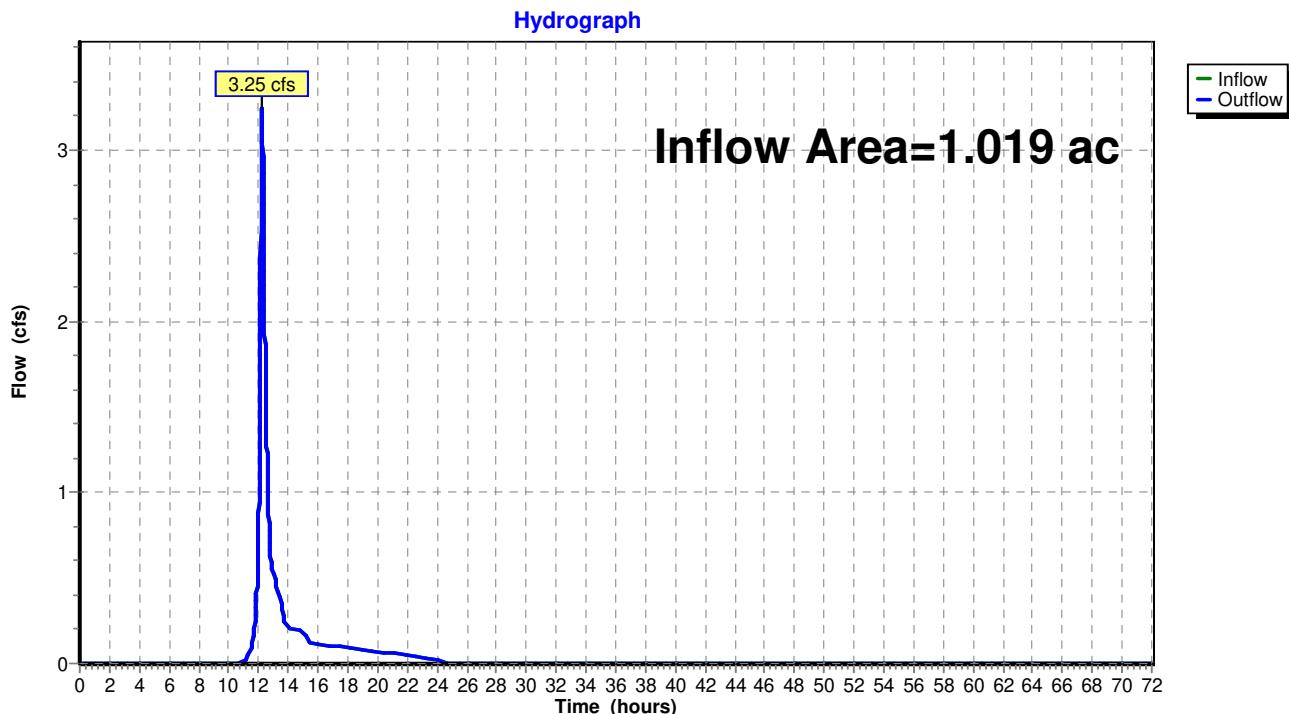
Inflow Area = 1.019 ac, 0.00% Impervious, Inflow Depth = 2.83" for 100-Year event

Inflow = 3.25 cfs @ 12.24 hrs, Volume= 0.240 af

Outflow = 3.25 cfs @ 12.24 hrs, Volume= 0.240 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R1: Existing Conditions



Retreat Center - Copy3

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Existing Conditions

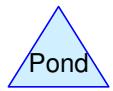
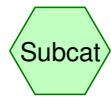
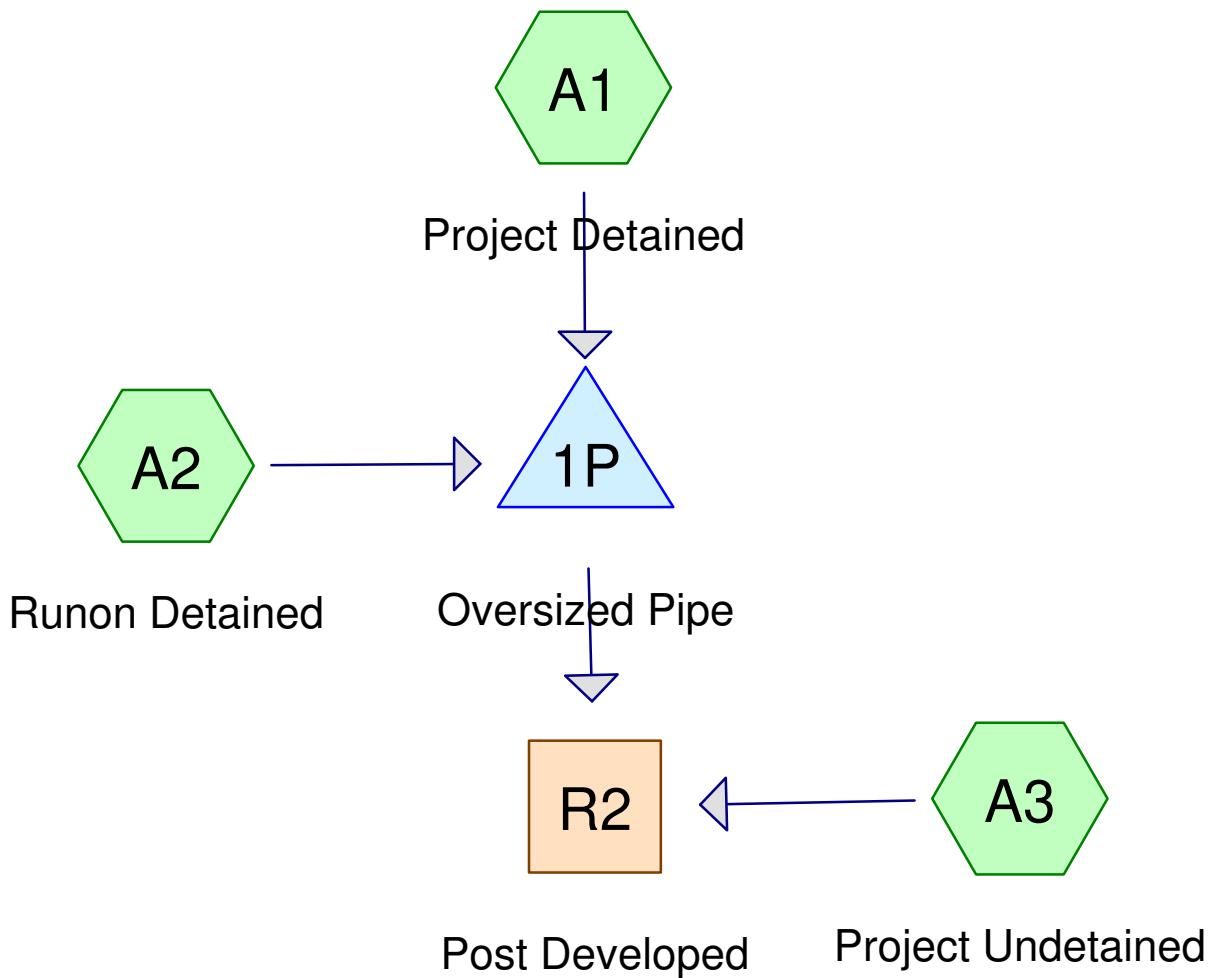
MSE 24-hr 4 100-Year Rainfall=7.60"

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Hydrograph for Reach R1: Existing Conditions

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.00 | 0.00 | 0.00 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.00 | 0.00 | 0.00 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.00 | 0.00 | 0.00 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.00 | 0.00 | 0.00 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.00 | 0.00 | 0.00 |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.00 | 0.00 | 0.00 |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.00 | 0.00 | 0.00 |
| 8.00 | 0.00 | 0.00 | 0.00 | 59.00 | 0.00 | 0.00 | 0.00 |
| 9.00 | 0.00 | 0.00 | 0.00 | 60.00 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.00 | 0.00 | 0.00 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.01 | 0.01 | 0.00 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 0.77 | 0.77 | 0.00 | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.53 | 0.53 | 0.00 | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.21 | 0.21 | 0.00 | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.19 | 0.19 | 0.00 | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.11 | 0.11 | 0.00 | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.10 | 0.10 | 0.00 | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.09 | 0.09 | 0.00 | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.08 | 0.08 | 0.00 | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.07 | 0.07 | 0.00 | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.06 | 0.06 | 0.00 | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.05 | 0.05 | 0.00 | | | | |
| 23.00 | 0.04 | 0.04 | 0.00 | | | | |
| 24.00 | 0.02 | 0.02 | 0.00 | | | | |
| 25.00 | 0.00 | 0.00 | 0.00 | | | | |
| 26.00 | 0.00 | 0.00 | 0.00 | | | | |
| 27.00 | 0.00 | 0.00 | 0.00 | | | | |
| 28.00 | 0.00 | 0.00 | 0.00 | | | | |
| 29.00 | 0.00 | 0.00 | 0.00 | | | | |
| 30.00 | 0.00 | 0.00 | 0.00 | | | | |
| 31.00 | 0.00 | 0.00 | 0.00 | | | | |
| 32.00 | 0.00 | 0.00 | 0.00 | | | | |
| 33.00 | 0.00 | 0.00 | 0.00 | | | | |
| 34.00 | 0.00 | 0.00 | 0.00 | | | | |
| 35.00 | 0.00 | 0.00 | 0.00 | | | | |
| 36.00 | 0.00 | 0.00 | 0.00 | | | | |
| 37.00 | 0.00 | 0.00 | 0.00 | | | | |
| 38.00 | 0.00 | 0.00 | 0.00 | | | | |
| 39.00 | 0.00 | 0.00 | 0.00 | | | | |
| 40.00 | 0.00 | 0.00 | 0.00 | | | | |
| 41.00 | 0.00 | 0.00 | 0.00 | | | | |
| 42.00 | 0.00 | 0.00 | 0.00 | | | | |
| 43.00 | 0.00 | 0.00 | 0.00 | | | | |
| 44.00 | 0.00 | 0.00 | 0.00 | | | | |
| 45.00 | 0.00 | 0.00 | 0.00 | | | | |
| 46.00 | 0.00 | 0.00 | 0.00 | | | | |
| 47.00 | 0.00 | 0.00 | 0.00 | | | | |
| 48.00 | 0.00 | 0.00 | 0.00 | | | | |
| 49.00 | 0.00 | 0.00 | 0.00 | | | | |
| 50.00 | 0.00 | 0.00 | 0.00 | | | | |



Routing Diagram for Retreat Center - Copy3
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Area Listing (selected nodes)

| Area (acres) | CN | Description (subcatchment-numbers) |
|-----------------|----|--|
| 0.366 | 61 | >75% Grass cover, Good, HSG B (A1, A2, A3) |
| 0.315 | 98 | Paved parking, HSG B (A1) |
| 0.321 | 98 | Roof (A1, A2) |
| 0.017 | 98 | Unconnected pavement, HSG B (A3) |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Proposed Conditions

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Soil Listing (selected nodes)

| Area (acres) | Soil Group | Subcatchment Numbers |
|-----------------|---------------|-------------------------|
| 0.000 | HSG A | |
| 0.698 | HSG B | A1, A2, A3 |
| 0.000 | HSG C | |
| 0.000 | HSG D | |
| 0.321 | Other | A1, A2 |

Retreat Center - Copy3

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Ground Covers (selected nodes)

| HSG-A (acres) | HSG-B (acres) | HSG-C (acres) | HSG-D (acres) | Other (acres) | Total (acres) | Ground Cover | Subcatchment Numbers |
|------------------|------------------|------------------|------------------|------------------|------------------|------------------------|-------------------------|
| 0.000 | 0.366 | 0.000 | 0.000 | 0.000 | 0.366 | >75% Grass cover, Good | A1, A2, A3 |
| 0.000 | 0.315 | 0.000 | 0.000 | 0.000 | 0.315 | Paved parking | A1 |
| 0.000 | 0.000 | 0.000 | 0.000 | 0.321 | 0.321 | Roof | A1, A2 |
| 0.000 | 0.017 | 0.000 | 0.000 | 0.000 | 0.017 | Unconnected pavement | A3 |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Proposed Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
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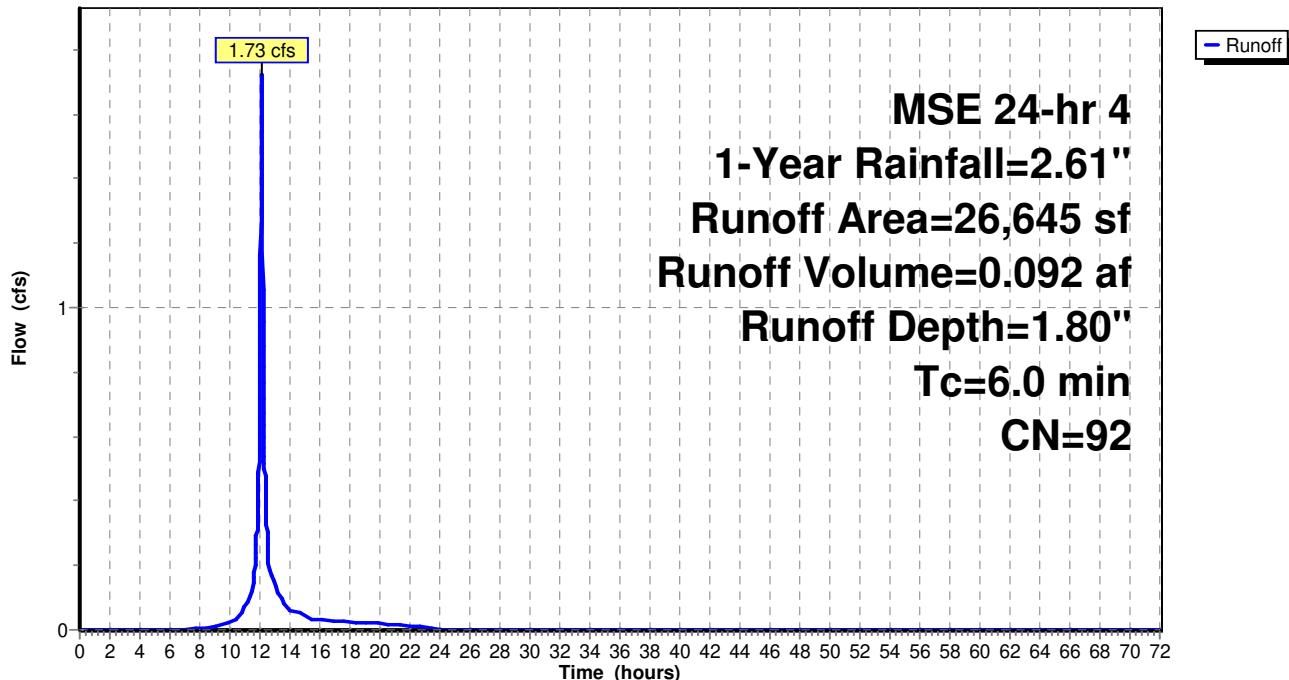
Summary for Subcatchment A1: Project Detained

Runoff = 1.73 cfs @ 12.13 hrs, Volume= 0.092 af, Depth= 1.80"
Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 1-Year Rainfall=2.61"

| Area (sf) | CN | Description |
|-----------|-------|-------------------------------|
| 13,722 | 98 | Paved parking, HSG B |
| * | 8,443 | Roof |
| 4,480 | 61 | >75% Grass cover, Good, HSG B |
| 26,645 | 92 | Weighted Average |
| 4,480 | | 16.81% Pervious Area |
| 22,165 | | 83.19% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A1: Project Detained**Hydrograph**

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Proposed Conditions
MSE 24-hr 4 1-Year Rainfall=2.61"
 Printed 9/16/2024
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Hydrograph for Subcatchment A1: Project Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 2.61 | 1.80 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 2.61 | 1.80 | 0.00 |
| 2.00 | 0.03 | 0.00 | 0.00 | 53.00 | 2.61 | 1.80 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 2.61 | 1.80 | 0.00 |
| 4.00 | 0.08 | 0.00 | 0.00 | 55.00 | 2.61 | 1.80 | 0.00 |
| 5.00 | 0.12 | 0.00 | 0.00 | 56.00 | 2.61 | 1.80 | 0.00 |
| 6.00 | 0.16 | 0.00 | 0.00 | 57.00 | 2.61 | 1.80 | 0.00 |
| 7.00 | 0.21 | 0.00 | 0.00 | 58.00 | 2.61 | 1.80 | 0.00 |
| 8.00 | 0.26 | 0.01 | 0.01 | 59.00 | 2.61 | 1.80 | 0.00 |
| 9.00 | 0.32 | 0.02 | 0.01 | 60.00 | 2.61 | 1.80 | 0.00 |
| 10.00 | 0.41 | 0.05 | 0.02 | 61.00 | 2.61 | 1.80 | 0.00 |
| 11.00 | 0.56 | 0.12 | 0.07 | 62.00 | 2.61 | 1.80 | 0.00 |
| 12.00 | 1.22 | 0.57 | 0.82 | 63.00 | 2.61 | 1.80 | 0.00 |
| 13.00 | 2.05 | 1.28 | 0.14 | 64.00 | 2.61 | 1.80 | 0.00 |
| 14.00 | 2.20 | 1.41 | 0.06 | 65.00 | 2.61 | 1.80 | 0.00 |
| 15.00 | 2.29 | 1.50 | 0.05 | 66.00 | 2.61 | 1.80 | 0.00 |
| 16.00 | 2.35 | 1.56 | 0.03 | 67.00 | 2.61 | 1.80 | 0.00 |
| 17.00 | 2.40 | 1.60 | 0.03 | 68.00 | 2.61 | 1.80 | 0.00 |
| 18.00 | 2.45 | 1.65 | 0.03 | 69.00 | 2.61 | 1.80 | 0.00 |
| 19.00 | 2.49 | 1.68 | 0.02 | 70.00 | 2.61 | 1.80 | 0.00 |
| 20.00 | 2.53 | 1.72 | 0.02 | 71.00 | 2.61 | 1.80 | 0.00 |
| 21.00 | 2.55 | 1.74 | 0.02 | 72.00 | 2.61 | 1.80 | 0.00 |
| 22.00 | 2.58 | 1.77 | 0.01 | | | | |
| 23.00 | 2.60 | 1.78 | 0.01 | | | | |
| 24.00 | 2.61 | 1.80 | 0.01 | | | | |
| 25.00 | 2.61 | 1.80 | 0.00 | | | | |
| 26.00 | 2.61 | 1.80 | 0.00 | | | | |
| 27.00 | 2.61 | 1.80 | 0.00 | | | | |
| 28.00 | 2.61 | 1.80 | 0.00 | | | | |
| 29.00 | 2.61 | 1.80 | 0.00 | | | | |
| 30.00 | 2.61 | 1.80 | 0.00 | | | | |
| 31.00 | 2.61 | 1.80 | 0.00 | | | | |
| 32.00 | 2.61 | 1.80 | 0.00 | | | | |
| 33.00 | 2.61 | 1.80 | 0.00 | | | | |
| 34.00 | 2.61 | 1.80 | 0.00 | | | | |
| 35.00 | 2.61 | 1.80 | 0.00 | | | | |
| 36.00 | 2.61 | 1.80 | 0.00 | | | | |
| 37.00 | 2.61 | 1.80 | 0.00 | | | | |
| 38.00 | 2.61 | 1.80 | 0.00 | | | | |
| 39.00 | 2.61 | 1.80 | 0.00 | | | | |
| 40.00 | 2.61 | 1.80 | 0.00 | | | | |
| 41.00 | 2.61 | 1.80 | 0.00 | | | | |
| 42.00 | 2.61 | 1.80 | 0.00 | | | | |
| 43.00 | 2.61 | 1.80 | 0.00 | | | | |
| 44.00 | 2.61 | 1.80 | 0.00 | | | | |
| 45.00 | 2.61 | 1.80 | 0.00 | | | | |
| 46.00 | 2.61 | 1.80 | 0.00 | | | | |
| 47.00 | 2.61 | 1.80 | 0.00 | | | | |
| 48.00 | 2.61 | 1.80 | 0.00 | | | | |
| 49.00 | 2.61 | 1.80 | 0.00 | | | | |
| 50.00 | 2.61 | 1.80 | 0.00 | | | | |

Retreat Center - Copy3

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MSE 24-hr 4 1-Year Rainfall=2.61"
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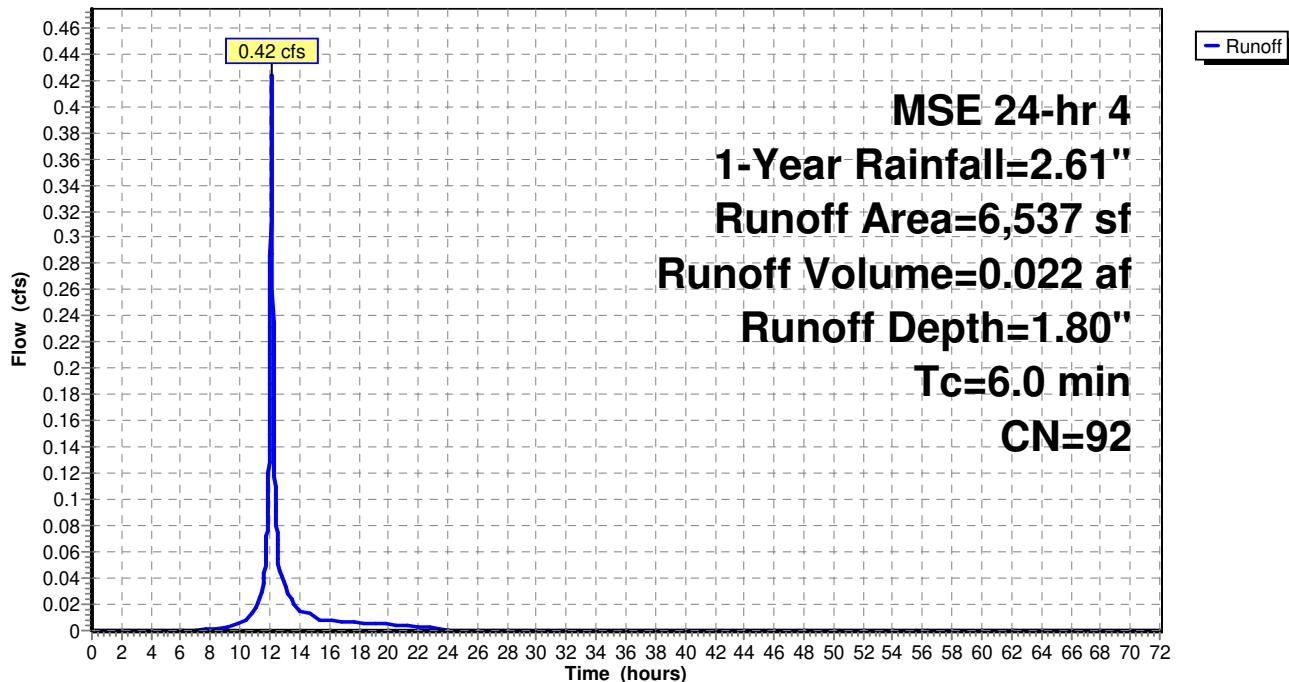
Summary for Subcatchment A2: Runon Detained

Runoff = 0.42 cfs @ 12.13 hrs, Volume= 0.022 af, Depth= 1.80"
 Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
 MSE 24-hr 4 1-Year Rainfall=2.61"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| * 5,529 | 98 | Roof |
| 1,008 | 61 | >75% Grass cover, Good, HSG B |
| 6,537 | 92 | Weighted Average |
| 1,008 | | 15.42% Pervious Area |
| 5,529 | | 84.58% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A2: Runon Detained**Hydrograph**

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Hydrograph for Subcatchment A2: Runon Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 2.61 | 1.80 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 2.61 | 1.80 | 0.00 |
| 2.00 | 0.03 | 0.00 | 0.00 | 53.00 | 2.61 | 1.80 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 2.61 | 1.80 | 0.00 |
| 4.00 | 0.08 | 0.00 | 0.00 | 55.00 | 2.61 | 1.80 | 0.00 |
| 5.00 | 0.12 | 0.00 | 0.00 | 56.00 | 2.61 | 1.80 | 0.00 |
| 6.00 | 0.16 | 0.00 | 0.00 | 57.00 | 2.61 | 1.80 | 0.00 |
| 7.00 | 0.21 | 0.00 | 0.00 | 58.00 | 2.61 | 1.80 | 0.00 |
| 8.00 | 0.26 | 0.01 | 0.00 | 59.00 | 2.61 | 1.80 | 0.00 |
| 9.00 | 0.32 | 0.02 | 0.00 | 60.00 | 2.61 | 1.80 | 0.00 |
| 10.00 | 0.41 | 0.05 | 0.01 | 61.00 | 2.61 | 1.80 | 0.00 |
| 11.00 | 0.56 | 0.12 | 0.02 | 62.00 | 2.61 | 1.80 | 0.00 |
| 12.00 | 1.22 | 0.57 | 0.20 | 63.00 | 2.61 | 1.80 | 0.00 |
| 13.00 | 2.05 | 1.28 | 0.04 | 64.00 | 2.61 | 1.80 | 0.00 |
| 14.00 | 2.20 | 1.41 | 0.01 | 65.00 | 2.61 | 1.80 | 0.00 |
| 15.00 | 2.29 | 1.50 | 0.01 | 66.00 | 2.61 | 1.80 | 0.00 |
| 16.00 | 2.35 | 1.56 | 0.01 | 67.00 | 2.61 | 1.80 | 0.00 |
| 17.00 | 2.40 | 1.60 | 0.01 | 68.00 | 2.61 | 1.80 | 0.00 |
| 18.00 | 2.45 | 1.65 | 0.01 | 69.00 | 2.61 | 1.80 | 0.00 |
| 19.00 | 2.49 | 1.68 | 0.01 | 70.00 | 2.61 | 1.80 | 0.00 |
| 20.00 | 2.53 | 1.72 | 0.00 | 71.00 | 2.61 | 1.80 | 0.00 |
| 21.00 | 2.55 | 1.74 | 0.00 | 72.00 | 2.61 | 1.80 | 0.00 |
| 22.00 | 2.58 | 1.77 | 0.00 | | | | |
| 23.00 | 2.60 | 1.78 | 0.00 | | | | |
| 24.00 | 2.61 | 1.80 | 0.00 | | | | |
| 25.00 | 2.61 | 1.80 | 0.00 | | | | |
| 26.00 | 2.61 | 1.80 | 0.00 | | | | |
| 27.00 | 2.61 | 1.80 | 0.00 | | | | |
| 28.00 | 2.61 | 1.80 | 0.00 | | | | |
| 29.00 | 2.61 | 1.80 | 0.00 | | | | |
| 30.00 | 2.61 | 1.80 | 0.00 | | | | |
| 31.00 | 2.61 | 1.80 | 0.00 | | | | |
| 32.00 | 2.61 | 1.80 | 0.00 | | | | |
| 33.00 | 2.61 | 1.80 | 0.00 | | | | |
| 34.00 | 2.61 | 1.80 | 0.00 | | | | |
| 35.00 | 2.61 | 1.80 | 0.00 | | | | |
| 36.00 | 2.61 | 1.80 | 0.00 | | | | |
| 37.00 | 2.61 | 1.80 | 0.00 | | | | |
| 38.00 | 2.61 | 1.80 | 0.00 | | | | |
| 39.00 | 2.61 | 1.80 | 0.00 | | | | |
| 40.00 | 2.61 | 1.80 | 0.00 | | | | |
| 41.00 | 2.61 | 1.80 | 0.00 | | | | |
| 42.00 | 2.61 | 1.80 | 0.00 | | | | |
| 43.00 | 2.61 | 1.80 | 0.00 | | | | |
| 44.00 | 2.61 | 1.80 | 0.00 | | | | |
| 45.00 | 2.61 | 1.80 | 0.00 | | | | |
| 46.00 | 2.61 | 1.80 | 0.00 | | | | |
| 47.00 | 2.61 | 1.80 | 0.00 | | | | |
| 48.00 | 2.61 | 1.80 | 0.00 | | | | |
| 49.00 | 2.61 | 1.80 | 0.00 | | | | |
| 50.00 | 2.61 | 1.80 | 0.00 | | | | |

Retreat Center - Copy3

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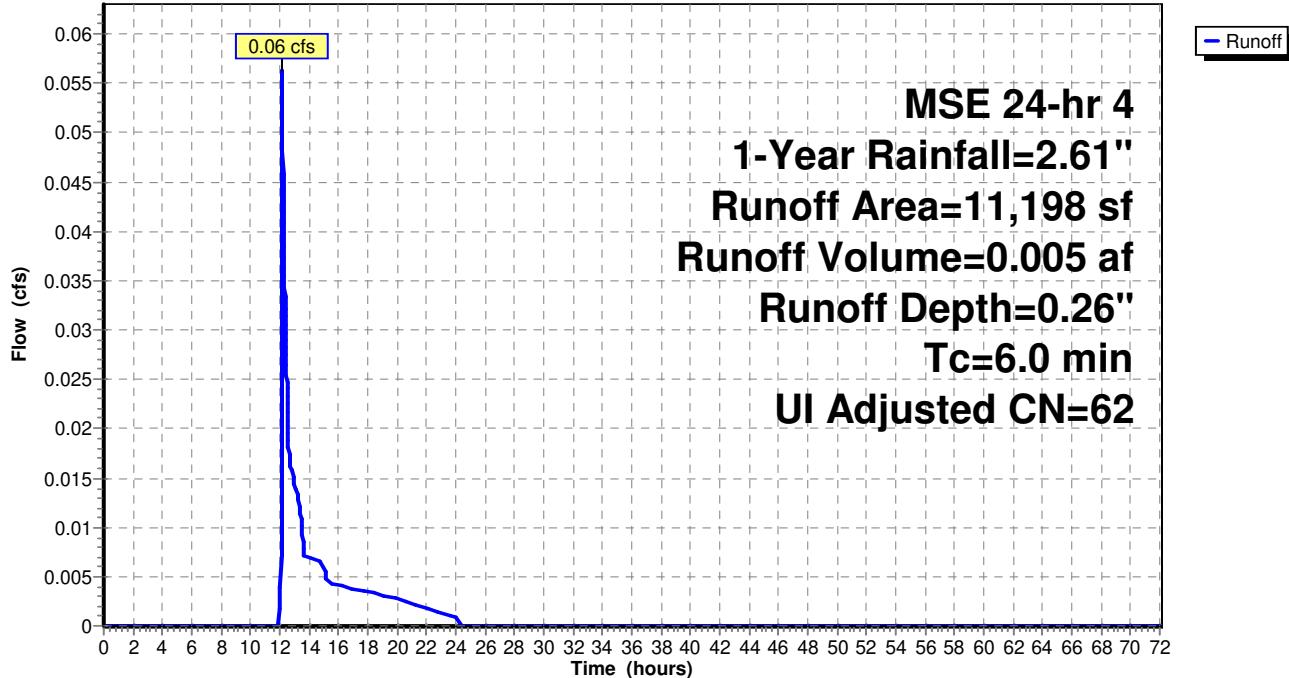
Summary for Subcatchment A3: Project Undetained

Runoff = 0.06 cfs @ 12.16 hrs, Volume= 0.005 af, Depth= 0.26"
Routed to Reach R2 : Post Developed

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 1-Year Rainfall=2.61"

| Area (sf) | CN | Adj | Description |
|-----------|----|-----|-------------------------------|
| 739 | 98 | | Unconnected pavement, HSG B |
| 10,459 | 61 | | >75% Grass cover, Good, HSG B |
| 11,198 | 63 | 62 | Weighted Average, UI Adjusted |
| 10,459 | | | 93.40% Pervious Area |
| 739 | | | 6.60% Impervious Area |
| 739 | | | 100.00% Unconnected |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A3: Project Undetained**Hydrograph**

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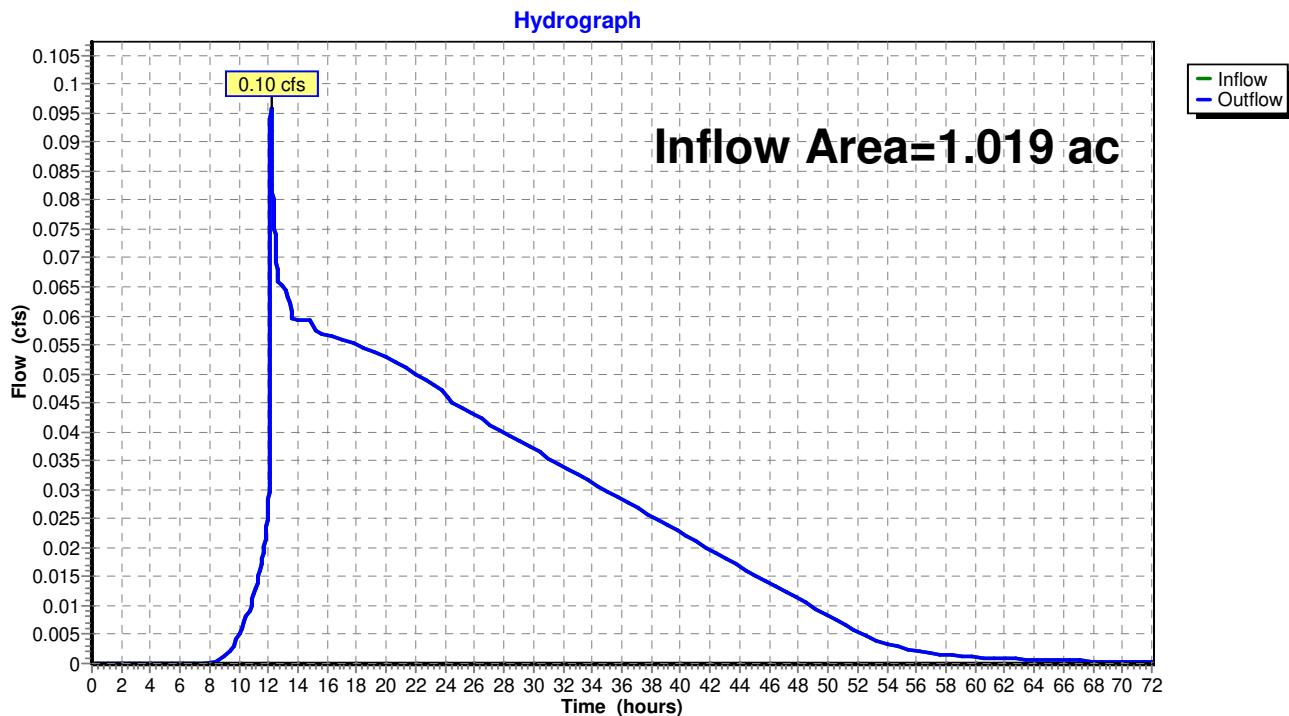
Hydrograph for Subcatchment A3: Project Undetained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 2.61 | 0.26 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 2.61 | 0.26 | 0.00 |
| 2.00 | 0.03 | 0.00 | 0.00 | 53.00 | 2.61 | 0.26 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 2.61 | 0.26 | 0.00 |
| 4.00 | 0.08 | 0.00 | 0.00 | 55.00 | 2.61 | 0.26 | 0.00 |
| 5.00 | 0.12 | 0.00 | 0.00 | 56.00 | 2.61 | 0.26 | 0.00 |
| 6.00 | 0.16 | 0.00 | 0.00 | 57.00 | 2.61 | 0.26 | 0.00 |
| 7.00 | 0.21 | 0.00 | 0.00 | 58.00 | 2.61 | 0.26 | 0.00 |
| 8.00 | 0.26 | 0.00 | 0.00 | 59.00 | 2.61 | 0.26 | 0.00 |
| 9.00 | 0.32 | 0.00 | 0.00 | 60.00 | 2.61 | 0.26 | 0.00 |
| 10.00 | 0.41 | 0.00 | 0.00 | 61.00 | 2.61 | 0.26 | 0.00 |
| 11.00 | 0.56 | 0.00 | 0.00 | 62.00 | 2.61 | 0.26 | 0.00 |
| 12.00 | 1.22 | 0.00 | 0.00 | 63.00 | 2.61 | 0.26 | 0.00 |
| 13.00 | 2.05 | 0.10 | 0.01 | 64.00 | 2.61 | 0.26 | 0.00 |
| 14.00 | 2.20 | 0.13 | 0.01 | 65.00 | 2.61 | 0.26 | 0.00 |
| 15.00 | 2.29 | 0.16 | 0.01 | 66.00 | 2.61 | 0.26 | 0.00 |
| 16.00 | 2.35 | 0.17 | 0.00 | 67.00 | 2.61 | 0.26 | 0.00 |
| 17.00 | 2.40 | 0.19 | 0.00 | 68.00 | 2.61 | 0.26 | 0.00 |
| 18.00 | 2.45 | 0.20 | 0.00 | 69.00 | 2.61 | 0.26 | 0.00 |
| 19.00 | 2.49 | 0.22 | 0.00 | 70.00 | 2.61 | 0.26 | 0.00 |
| 20.00 | 2.53 | 0.23 | 0.00 | 71.00 | 2.61 | 0.26 | 0.00 |
| 21.00 | 2.55 | 0.24 | 0.00 | 72.00 | 2.61 | 0.26 | 0.00 |
| 22.00 | 2.58 | 0.24 | 0.00 | | | | |
| 23.00 | 2.60 | 0.25 | 0.00 | | | | |
| 24.00 | 2.61 | 0.26 | 0.00 | | | | |
| 25.00 | 2.61 | 0.26 | 0.00 | | | | |
| 26.00 | 2.61 | 0.26 | 0.00 | | | | |
| 27.00 | 2.61 | 0.26 | 0.00 | | | | |
| 28.00 | 2.61 | 0.26 | 0.00 | | | | |
| 29.00 | 2.61 | 0.26 | 0.00 | | | | |
| 30.00 | 2.61 | 0.26 | 0.00 | | | | |
| 31.00 | 2.61 | 0.26 | 0.00 | | | | |
| 32.00 | 2.61 | 0.26 | 0.00 | | | | |
| 33.00 | 2.61 | 0.26 | 0.00 | | | | |
| 34.00 | 2.61 | 0.26 | 0.00 | | | | |
| 35.00 | 2.61 | 0.26 | 0.00 | | | | |
| 36.00 | 2.61 | 0.26 | 0.00 | | | | |
| 37.00 | 2.61 | 0.26 | 0.00 | | | | |
| 38.00 | 2.61 | 0.26 | 0.00 | | | | |
| 39.00 | 2.61 | 0.26 | 0.00 | | | | |
| 40.00 | 2.61 | 0.26 | 0.00 | | | | |
| 41.00 | 2.61 | 0.26 | 0.00 | | | | |
| 42.00 | 2.61 | 0.26 | 0.00 | | | | |
| 43.00 | 2.61 | 0.26 | 0.00 | | | | |
| 44.00 | 2.61 | 0.26 | 0.00 | | | | |
| 45.00 | 2.61 | 0.26 | 0.00 | | | | |
| 46.00 | 2.61 | 0.26 | 0.00 | | | | |
| 47.00 | 2.61 | 0.26 | 0.00 | | | | |
| 48.00 | 2.61 | 0.26 | 0.00 | | | | |
| 49.00 | 2.61 | 0.26 | 0.00 | | | | |
| 50.00 | 2.61 | 0.26 | 0.00 | | | | |

Summary for Reach R2: Post Developed

Inflow Area = 1.019 ac, 64.07% Impervious, Inflow Depth > 1.40" for 1-Year event
Inflow = 0.10 cfs @ 12.16 hrs, Volume= 0.119 af
Outflow = 0.10 cfs @ 12.16 hrs, Volume= 0.119 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R2: Post Developed

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Hydrograph for Reach R2: Post Developed

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.01 | 0.01 | 0.01 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.01 | 0.01 | 0.01 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.00 | 0.00 | 0.00 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.00 | 0.00 | 0.00 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.00 | 0.00 | 0.00 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.00 | 0.00 | 0.00 |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.00 | 0.00 | 0.00 |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.00 | 0.00 | 0.00 |
| 8.00 | 0.00 | 0.00 | 0.00 | 59.00 | 0.00 | 0.00 | 0.00 |
| 9.00 | 0.00 | 0.00 | 0.00 | 60.00 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.01 | 0.01 | 0.01 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.01 | 0.01 | 0.01 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 0.03 | 0.03 | 0.03 | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.06 | 0.06 | 0.06 | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.06 | 0.06 | 0.06 | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.06 | 0.06 | 0.06 | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.06 | 0.06 | 0.06 | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.06 | 0.06 | 0.06 | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.06 | 0.06 | 0.06 | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.05 | 0.05 | 0.05 | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.05 | 0.05 | 0.05 | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.05 | 0.05 | 0.05 | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.05 | 0.05 | | | | | |
| 23.00 | 0.05 | 0.05 | | | | | |
| 24.00 | 0.05 | 0.05 | | | | | |
| 25.00 | 0.04 | 0.04 | | | | | |
| 26.00 | 0.04 | 0.04 | | | | | |
| 27.00 | 0.04 | 0.04 | | | | | |
| 28.00 | 0.04 | 0.04 | | | | | |
| 29.00 | 0.04 | 0.04 | | | | | |
| 30.00 | 0.04 | 0.04 | | | | | |
| 31.00 | 0.04 | 0.04 | | | | | |
| 32.00 | 0.03 | 0.03 | | | | | |
| 33.00 | 0.03 | 0.03 | | | | | |
| 34.00 | 0.03 | 0.03 | | | | | |
| 35.00 | 0.03 | 0.03 | | | | | |
| 36.00 | 0.03 | 0.03 | | | | | |
| 37.00 | 0.03 | 0.03 | | | | | |
| 38.00 | 0.03 | 0.03 | | | | | |
| 39.00 | 0.02 | 0.02 | | | | | |
| 40.00 | 0.02 | 0.02 | | | | | |
| 41.00 | 0.02 | 0.02 | | | | | |
| 42.00 | 0.02 | 0.02 | | | | | |
| 43.00 | 0.02 | 0.02 | | | | | |
| 44.00 | 0.02 | 0.02 | | | | | |
| 45.00 | 0.02 | 0.02 | | | | | |
| 46.00 | 0.01 | 0.01 | | | | | |
| 47.00 | 0.01 | 0.01 | | | | | |
| 48.00 | 0.01 | 0.01 | | | | | |
| 49.00 | 0.01 | 0.01 | | | | | |
| 50.00 | 0.01 | 0.01 | | | | | |

Summary for Pond 1P: Oversized Pipe

Inflow Area = 0.762 ac, 83.46% Impervious, Inflow Depth = 1.80" for 1-Year event
Inflow = 2.15 cfs @ 12.13 hrs, Volume= 0.114 af
Outflow = 0.05 cfs @ 15.09 hrs, Volume= 0.113 af, Atten= 98%, Lag= 177.3 min
Primary = 0.05 cfs @ 15.09 hrs, Volume= 0.113 af

Routed to Reach R2 : Post Developed

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Starting Elev= 784.00' Surf.Area= 0.041 ac Storage= 0.111 af
Peak Elev= 786.01' @ 15.09 hrs Surf.Area= 0.036 ac Storage= 0.192 af (0.080 af above start)

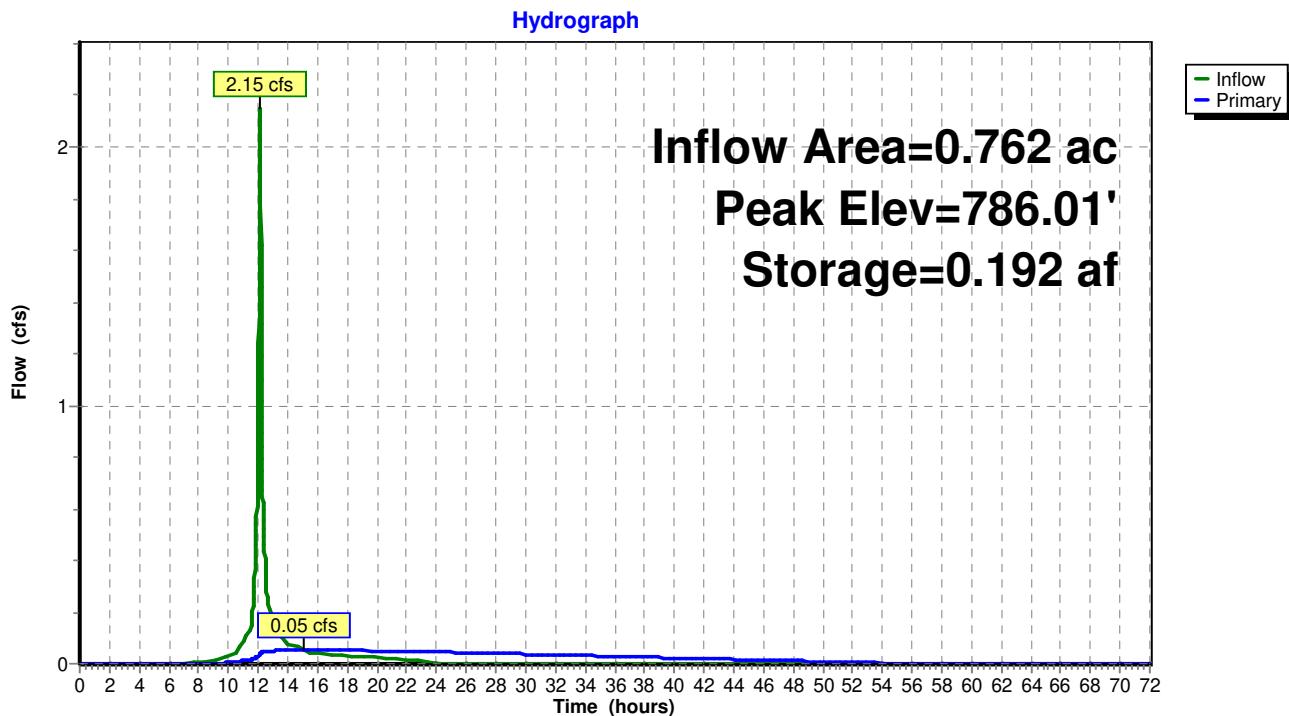
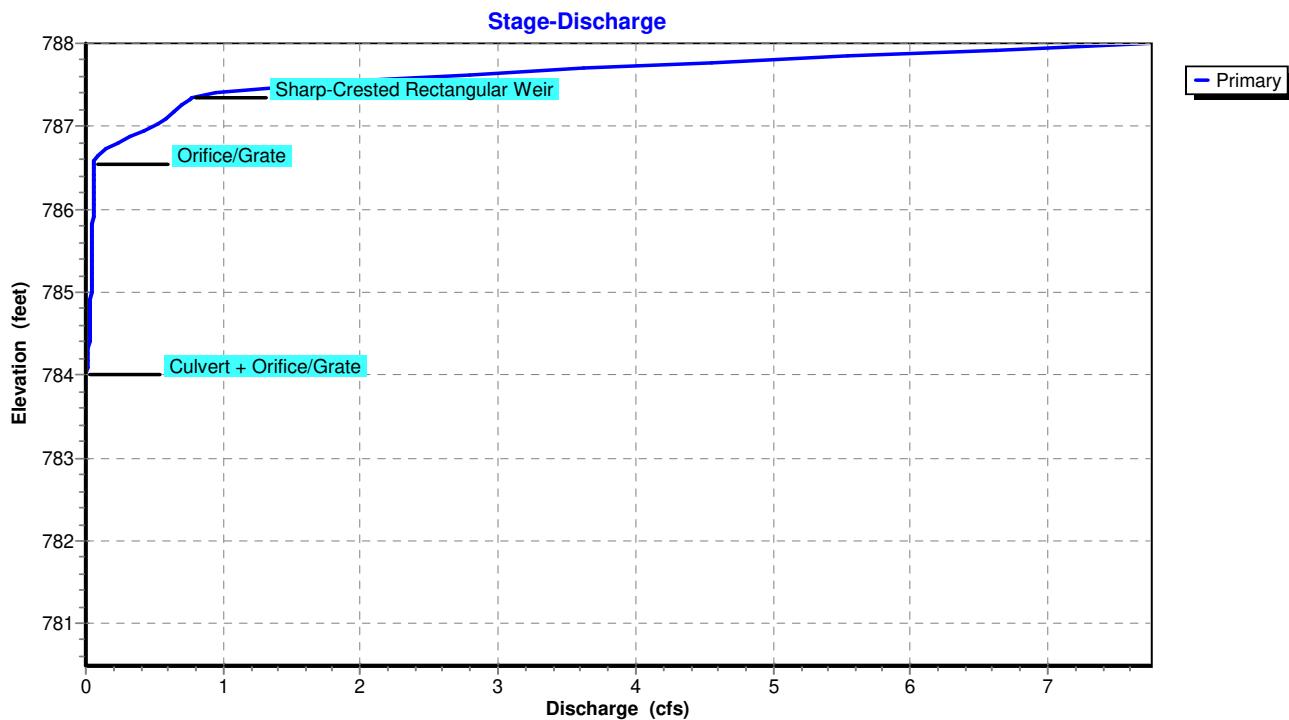
Plug-Flow detention time= 2,987.6 min calculated for 0.002 af (2% of inflow)
Center-of-Mass det. time= 831.1 min (1,626.8 - 795.8)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 780.50' | 0.243 af | 90.0" Round Pipe Storage L= 240.0' |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 784.00' | 18.0" Round Culvert L= 19.0' RCP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 784.00' / 783.75' S= 0.0132 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 1.77 sf |
| #2 | Device 1 | 784.00' | 1.2" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #3 | Device 1 | 786.55' | 6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 787.35' | 4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s) |

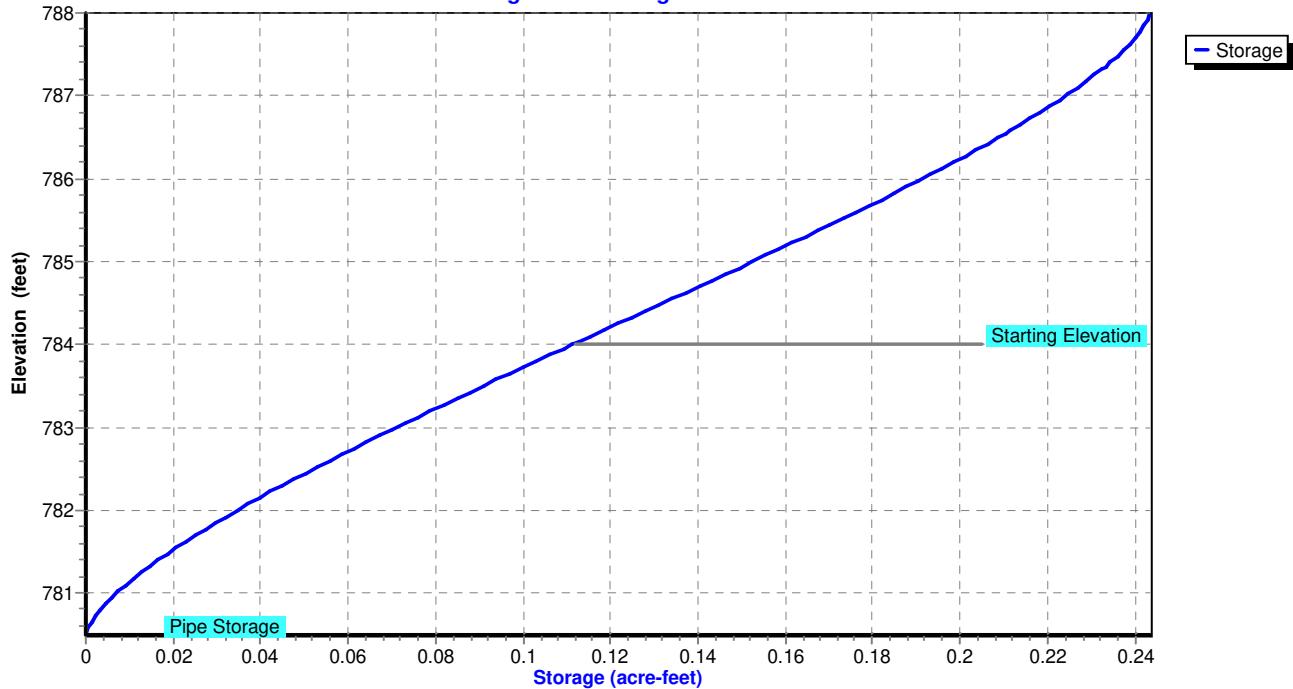
Primary OutFlow Max=0.05 cfs @ 15.09 hrs HW=786.01' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.05 cfs of 8.42 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 0.05 cfs @ 6.74 fps)
- 3=Orifice/Grate (Controls 0.00 cfs)
- 4=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: Oversized Pipe**Pond 1P: Oversized Pipe**

Pond 1P: Oversized Pipe

Stage-Area-Storage



Hydrograph for Pond 1P: Oversized Pipe

| Time (hours) | Inflow (cfs) | Storage (acre-feet) | Elevation (feet) | Primary (cfs) |
|-----------------|-----------------|------------------------|---------------------|------------------|
| 0.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 2.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 4.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 6.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 8.00 | 0.01 | 0.112 | 784.01 | 0.00 |
| 10.00 | 0.03 | 0.114 | 784.07 | 0.01 |
| 12.00 | 1.02 | 0.137 | 784.61 | 0.03 |
| 14.00 | 0.07 | 0.190 | 785.97 | 0.05 |
| 16.00 | 0.04 | 0.191 | 785.98 | 0.05 |
| 18.00 | 0.03 | 0.188 | 785.91 | 0.05 |
| 20.00 | 0.02 | 0.184 | 785.80 | 0.05 |
| 22.00 | 0.02 | 0.179 | 785.67 | 0.05 |
| 24.00 | 0.01 | 0.173 | 785.52 | 0.05 |
| 26.00 | 0.00 | 0.166 | 785.34 | 0.04 |
| 28.00 | 0.00 | 0.159 | 785.16 | 0.04 |
| 30.00 | 0.00 | 0.153 | 785.01 | 0.04 |
| 32.00 | 0.00 | 0.147 | 784.86 | 0.03 |
| 34.00 | 0.00 | 0.141 | 784.73 | 0.03 |
| 36.00 | 0.00 | 0.137 | 784.61 | 0.03 |
| 38.00 | 0.00 | 0.132 | 784.50 | 0.03 |
| 40.00 | 0.00 | 0.128 | 784.41 | 0.02 |
| 42.00 | 0.00 | 0.125 | 784.32 | 0.02 |
| 44.00 | 0.00 | 0.122 | 784.25 | 0.02 |
| 46.00 | 0.00 | 0.119 | 784.19 | 0.01 |
| 48.00 | 0.00 | 0.117 | 784.14 | 0.01 |
| 50.00 | 0.00 | 0.115 | 784.10 | 0.01 |
| 52.00 | 0.00 | 0.114 | 784.07 | 0.01 |
| 54.00 | 0.00 | 0.114 | 784.05 | 0.00 |
| 56.00 | 0.00 | 0.113 | 784.04 | 0.00 |
| 58.00 | 0.00 | 0.113 | 784.04 | 0.00 |
| 60.00 | 0.00 | 0.113 | 784.03 | 0.00 |
| 62.00 | 0.00 | 0.112 | 784.03 | 0.00 |
| 64.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 66.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 68.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 70.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 72.00 | 0.00 | 0.112 | 784.02 | 0.00 |

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Stage-Discharge for Pond 1P: Oversized Pipe

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 780.50 | 0.00 | 783.05 | 0.00 | 785.60 | 0.05 |
| 780.55 | 0.00 | 783.10 | 0.00 | 785.65 | 0.05 |
| 780.60 | 0.00 | 783.15 | 0.00 | 785.70 | 0.05 |
| 780.65 | 0.00 | 783.20 | 0.00 | 785.75 | 0.05 |
| 780.70 | 0.00 | 783.25 | 0.00 | 785.80 | 0.05 |
| 780.75 | 0.00 | 783.30 | 0.00 | 785.85 | 0.05 |
| 780.80 | 0.00 | 783.35 | 0.00 | 785.90 | 0.05 |
| 780.85 | 0.00 | 783.40 | 0.00 | 785.95 | 0.05 |
| 780.90 | 0.00 | 783.45 | 0.00 | 786.00 | 0.05 |
| 780.95 | 0.00 | 783.50 | 0.00 | 786.05 | 0.05 |
| 781.00 | 0.00 | 783.55 | 0.00 | 786.10 | 0.05 |
| 781.05 | 0.00 | 783.60 | 0.00 | 786.15 | 0.05 |
| 781.10 | 0.00 | 783.65 | 0.00 | 786.20 | 0.06 |
| 781.15 | 0.00 | 783.70 | 0.00 | 786.25 | 0.06 |
| 781.20 | 0.00 | 783.75 | 0.00 | 786.30 | 0.06 |
| 781.25 | 0.00 | 783.80 | 0.00 | 786.35 | 0.06 |
| 781.30 | 0.00 | 783.85 | 0.00 | 786.40 | 0.06 |
| 781.35 | 0.00 | 783.90 | 0.00 | 786.45 | 0.06 |
| 781.40 | 0.00 | 783.95 | 0.00 | 786.50 | 0.06 |
| 781.45 | 0.00 | 784.00 | 0.00 | 786.55 | 0.06 |
| 781.50 | 0.00 | 784.05 | 0.00 | 786.60 | 0.07 |
| 781.55 | 0.00 | 784.10 | 0.01 | 786.65 | 0.09 |
| 781.60 | 0.00 | 784.15 | 0.01 | 786.70 | 0.13 |
| 781.65 | 0.00 | 784.20 | 0.01 | 786.75 | 0.17 |
| 781.70 | 0.00 | 784.25 | 0.02 | 786.80 | 0.23 |
| 781.75 | 0.00 | 784.30 | 0.02 | 786.85 | 0.29 |
| 781.80 | 0.00 | 784.35 | 0.02 | 786.90 | 0.36 |
| 781.85 | 0.00 | 784.40 | 0.02 | 786.95 | 0.43 |
| 781.90 | 0.00 | 784.45 | 0.02 | 787.00 | 0.49 |
| 781.95 | 0.00 | 784.50 | 0.03 | 787.05 | 0.54 |
| 782.00 | 0.00 | 784.55 | 0.03 | 787.10 | 0.58 |
| 782.05 | 0.00 | 784.60 | 0.03 | 787.15 | 0.63 |
| 782.10 | 0.00 | 784.65 | 0.03 | 787.20 | 0.67 |
| 782.15 | 0.00 | 784.70 | 0.03 | 787.25 | 0.70 |
| 782.20 | 0.00 | 784.75 | 0.03 | 787.30 | 0.74 |
| 782.25 | 0.00 | 784.80 | 0.03 | 787.35 | 0.77 |
| 782.30 | 0.00 | 784.85 | 0.03 | 787.40 | 0.95 |
| 782.35 | 0.00 | 784.90 | 0.03 | 787.45 | 1.24 |
| 782.40 | 0.00 | 784.95 | 0.04 | 787.50 | 1.62 |
| 782.45 | 0.00 | 785.00 | 0.04 | 787.55 | 2.05 |
| 782.50 | 0.00 | 785.05 | 0.04 | 787.60 | 2.53 |
| 782.55 | 0.00 | 785.10 | 0.04 | 787.65 | 3.06 |
| 782.60 | 0.00 | 785.15 | 0.04 | 787.70 | 3.63 |
| 782.65 | 0.00 | 785.20 | 0.04 | 787.75 | 4.24 |
| 782.70 | 0.00 | 785.25 | 0.04 | 787.80 | 4.88 |
| 782.75 | 0.00 | 785.30 | 0.04 | 787.85 | 5.55 |
| 782.80 | 0.00 | 785.35 | 0.04 | 787.90 | 6.25 |
| 782.85 | 0.00 | 785.40 | 0.04 | 787.95 | 6.99 |
| 782.90 | 0.00 | 785.45 | 0.04 | 788.00 | 7.74 |
| 782.95 | 0.00 | 785.50 | 0.05 | | |
| 783.00 | 0.00 | 785.55 | 0.05 | | |

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Stage-Area-Storage for Pond 1P: Oversized Pipe

| Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) |
|---------------------|------------------------|---------------------|------------------------|---------------------|------------------------|
| 780.50 | 0.000 | 783.05 | 0.073 | 785.60 | 0.176 |
| 780.55 | 0.000 | 783.10 | 0.075 | 785.65 | 0.178 |
| 780.60 | 0.001 | 783.15 | 0.077 | 785.70 | 0.180 |
| 780.65 | 0.001 | 783.20 | 0.079 | 785.75 | 0.182 |
| 780.70 | 0.002 | 783.25 | 0.081 | 785.80 | 0.184 |
| 780.75 | 0.002 | 783.30 | 0.083 | 785.85 | 0.186 |
| 780.80 | 0.003 | 783.35 | 0.085 | 785.90 | 0.188 |
| 780.85 | 0.004 | 783.40 | 0.087 | 785.95 | 0.189 |
| 780.90 | 0.005 | 783.45 | 0.089 | 786.00 | 0.191 |
| 780.95 | 0.006 | 783.50 | 0.091 | 786.05 | 0.193 |
| 781.00 | 0.007 | 783.55 | 0.093 | 786.10 | 0.195 |
| 781.05 | 0.008 | 783.60 | 0.095 | 786.15 | 0.197 |
| 781.10 | 0.009 | 783.65 | 0.097 | 786.20 | 0.198 |
| 781.15 | 0.010 | 783.70 | 0.099 | 786.25 | 0.200 |
| 781.20 | 0.011 | 783.75 | 0.101 | 786.30 | 0.202 |
| 781.25 | 0.013 | 783.80 | 0.103 | 786.35 | 0.204 |
| 781.30 | 0.014 | 783.85 | 0.105 | 786.40 | 0.205 |
| 781.35 | 0.015 | 783.90 | 0.107 | 786.45 | 0.207 |
| 781.40 | 0.017 | 783.95 | 0.109 | 786.50 | 0.209 |
| 781.45 | 0.018 | 784.00 | 0.111 | 786.55 | 0.210 |
| 781.50 | 0.019 | 784.05 | 0.113 | 786.60 | 0.212 |
| 781.55 | 0.021 | 784.10 | 0.116 | 786.65 | 0.214 |
| 781.60 | 0.022 | 784.15 | 0.118 | 786.70 | 0.215 |
| 781.65 | 0.024 | 784.20 | 0.120 | 786.75 | 0.217 |
| 781.70 | 0.025 | 784.25 | 0.122 | 786.80 | 0.218 |
| 781.75 | 0.027 | 784.30 | 0.124 | 786.85 | 0.220 |
| 781.80 | 0.028 | 784.35 | 0.126 | 786.90 | 0.221 |
| 781.85 | 0.030 | 784.40 | 0.128 | 786.95 | 0.223 |
| 781.90 | 0.031 | 784.45 | 0.130 | 787.00 | 0.224 |
| 781.95 | 0.033 | 784.50 | 0.132 | 787.05 | 0.226 |
| 782.00 | 0.035 | 784.55 | 0.134 | 787.10 | 0.227 |
| 782.05 | 0.036 | 784.60 | 0.136 | 787.15 | 0.228 |
| 782.10 | 0.038 | 784.65 | 0.138 | 787.20 | 0.229 |
| 782.15 | 0.040 | 784.70 | 0.140 | 787.25 | 0.231 |
| 782.20 | 0.041 | 784.75 | 0.142 | 787.30 | 0.232 |
| 782.25 | 0.043 | 784.80 | 0.144 | 787.35 | 0.233 |
| 782.30 | 0.045 | 784.85 | 0.146 | 787.40 | 0.234 |
| 782.35 | 0.047 | 784.90 | 0.148 | 787.45 | 0.235 |
| 782.40 | 0.048 | 784.95 | 0.150 | 787.50 | 0.236 |
| 782.45 | 0.050 | 785.00 | 0.152 | 787.55 | 0.237 |
| 782.50 | 0.052 | 785.05 | 0.155 | 787.60 | 0.238 |
| 782.55 | 0.054 | 785.10 | 0.157 | 787.65 | 0.239 |
| 782.60 | 0.056 | 785.15 | 0.159 | 787.70 | 0.240 |
| 782.65 | 0.058 | 785.20 | 0.161 | 787.75 | 0.241 |
| 782.70 | 0.060 | 785.25 | 0.163 | 787.80 | 0.242 |
| 782.75 | 0.061 | 785.30 | 0.165 | 787.85 | 0.242 |
| 782.80 | 0.063 | 785.35 | 0.166 | 787.90 | 0.243 |
| 782.85 | 0.065 | 785.40 | 0.168 | 787.95 | 0.243 |
| 782.90 | 0.067 | 785.45 | 0.170 | 788.00 | 0.243 |
| 782.95 | 0.069 | 785.50 | 0.172 | | |
| 783.00 | 0.071 | 785.55 | 0.174 | | |

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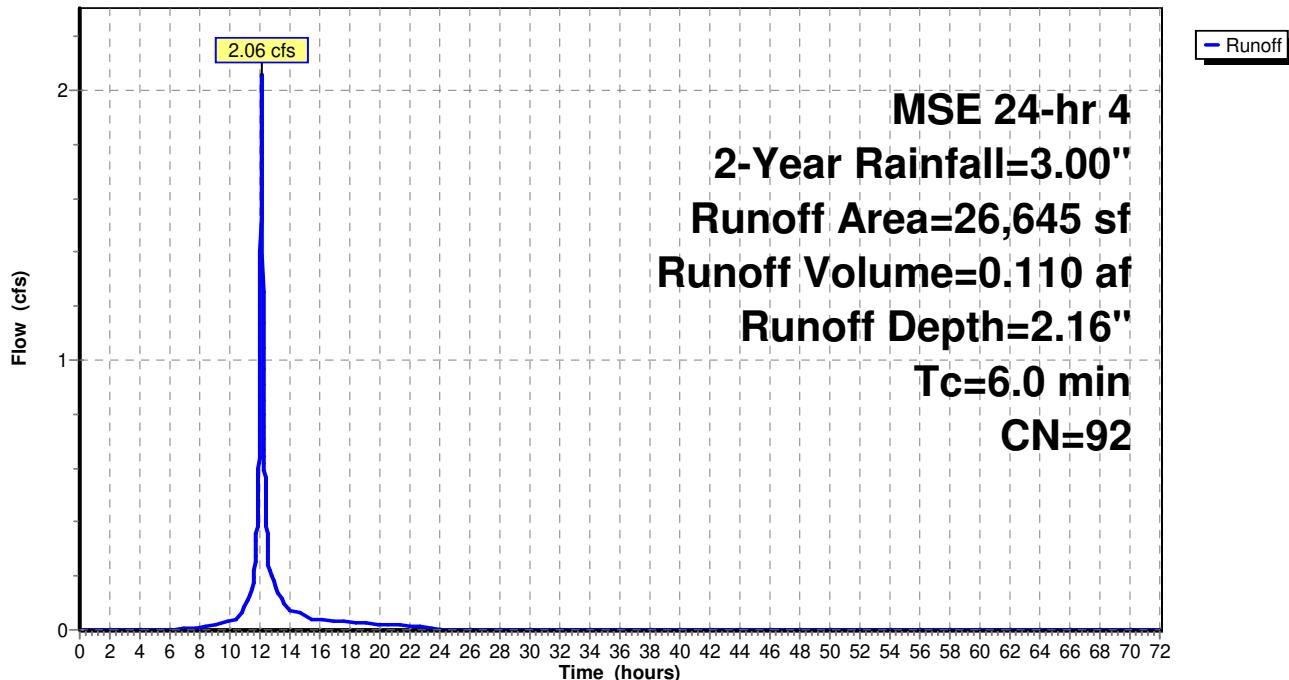
Summary for Subcatchment A1: Project Detained

Runoff = 2.06 cfs @ 12.13 hrs, Volume= 0.110 af, Depth= 2.16"
Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 2-Year Rainfall=3.00"

| Area (sf) | CN | Description |
|-----------|-------|-------------------------------|
| 13,722 | 98 | Paved parking, HSG B |
| * | 8,443 | Roof |
| | 4,480 | >75% Grass cover, Good, HSG B |
| 26,645 | 92 | Weighted Average |
| | 4,480 | 16.81% Pervious Area |
| 22,165 | | 83.19% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|-------------|
| 6.0 | Direct Entry, | | | | |

Subcatchment A1: Project Detained**Hydrograph**

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Hydrograph for Subcatchment A1: Project Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 3.00 | 2.16 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 3.00 | 2.16 | 0.00 |
| 2.00 | 0.04 | 0.00 | 0.00 | 53.00 | 3.00 | 2.16 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 3.00 | 2.16 | 0.00 |
| 4.00 | 0.10 | 0.00 | 0.00 | 55.00 | 3.00 | 2.16 | 0.00 |
| 5.00 | 0.14 | 0.00 | 0.00 | 56.00 | 3.00 | 2.16 | 0.00 |
| 6.00 | 0.18 | 0.00 | 0.00 | 57.00 | 3.00 | 2.16 | 0.00 |
| 7.00 | 0.24 | 0.00 | 0.00 | 58.00 | 3.00 | 2.16 | 0.00 |
| 8.00 | 0.30 | 0.02 | 0.01 | 59.00 | 3.00 | 2.16 | 0.00 |
| 9.00 | 0.36 | 0.03 | 0.01 | 60.00 | 3.00 | 2.16 | 0.00 |
| 10.00 | 0.48 | 0.08 | 0.03 | 61.00 | 3.00 | 2.16 | 0.00 |
| 11.00 | 0.65 | 0.17 | 0.09 | 62.00 | 3.00 | 2.16 | 0.00 |
| 12.00 | 1.41 | 0.72 | 0.99 | 63.00 | 3.00 | 2.16 | 0.00 |
| 13.00 | 2.35 | 1.56 | 0.17 | 64.00 | 3.00 | 2.16 | 0.00 |
| 14.00 | 2.52 | 1.72 | 0.07 | 65.00 | 3.00 | 2.16 | 0.00 |
| 15.00 | 2.64 | 1.82 | 0.06 | 66.00 | 3.00 | 2.16 | 0.00 |
| 16.00 | 2.70 | 1.88 | 0.04 | 67.00 | 3.00 | 2.16 | 0.00 |
| 17.00 | 2.76 | 1.94 | 0.03 | 68.00 | 3.00 | 2.16 | 0.00 |
| 18.00 | 2.82 | 1.99 | 0.03 | 69.00 | 3.00 | 2.16 | 0.00 |
| 19.00 | 2.86 | 2.03 | 0.03 | 70.00 | 3.00 | 2.16 | 0.00 |
| 20.00 | 2.90 | 2.07 | 0.02 | 71.00 | 3.00 | 2.16 | 0.00 |
| 21.00 | 2.94 | 2.10 | 0.02 | 72.00 | 3.00 | 2.16 | 0.00 |
| 22.00 | 2.96 | 2.13 | 0.01 | | | | |
| 23.00 | 2.99 | 2.15 | 0.01 | | | | |
| 24.00 | 3.00 | 2.16 | 0.01 | | | | |
| 25.00 | 3.00 | 2.16 | 0.00 | | | | |
| 26.00 | 3.00 | 2.16 | 0.00 | | | | |
| 27.00 | 3.00 | 2.16 | 0.00 | | | | |
| 28.00 | 3.00 | 2.16 | 0.00 | | | | |
| 29.00 | 3.00 | 2.16 | 0.00 | | | | |
| 30.00 | 3.00 | 2.16 | 0.00 | | | | |
| 31.00 | 3.00 | 2.16 | 0.00 | | | | |
| 32.00 | 3.00 | 2.16 | 0.00 | | | | |
| 33.00 | 3.00 | 2.16 | 0.00 | | | | |
| 34.00 | 3.00 | 2.16 | 0.00 | | | | |
| 35.00 | 3.00 | 2.16 | 0.00 | | | | |
| 36.00 | 3.00 | 2.16 | 0.00 | | | | |
| 37.00 | 3.00 | 2.16 | 0.00 | | | | |
| 38.00 | 3.00 | 2.16 | 0.00 | | | | |
| 39.00 | 3.00 | 2.16 | 0.00 | | | | |
| 40.00 | 3.00 | 2.16 | 0.00 | | | | |
| 41.00 | 3.00 | 2.16 | 0.00 | | | | |
| 42.00 | 3.00 | 2.16 | 0.00 | | | | |
| 43.00 | 3.00 | 2.16 | 0.00 | | | | |
| 44.00 | 3.00 | 2.16 | 0.00 | | | | |
| 45.00 | 3.00 | 2.16 | 0.00 | | | | |
| 46.00 | 3.00 | 2.16 | 0.00 | | | | |
| 47.00 | 3.00 | 2.16 | 0.00 | | | | |
| 48.00 | 3.00 | 2.16 | 0.00 | | | | |
| 49.00 | 3.00 | 2.16 | 0.00 | | | | |
| 50.00 | 3.00 | 2.16 | 0.00 | | | | |

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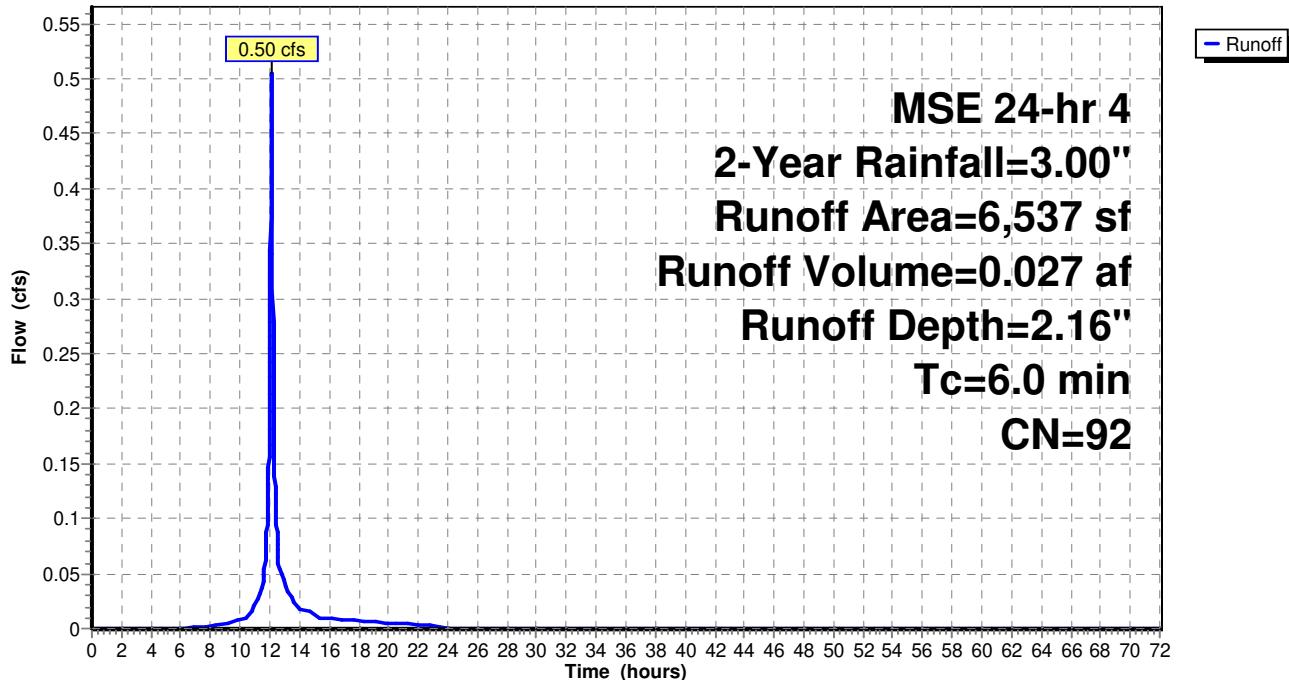
Summary for Subcatchment A2: Runon Detained

Runoff = 0.50 cfs @ 12.13 hrs, Volume= 0.027 af, Depth= 2.16"
Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 2-Year Rainfall=3.00"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| * 5,529 | 98 | Roof |
| 1,008 | 61 | >75% Grass cover, Good, HSG B |
| 6,537 | 92 | Weighted Average |
| 1,008 | | 15.42% Pervious Area |
| 5,529 | | 84.58% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A2: Runon Detained**Hydrograph**

Hydrograph for Subcatchment A2: Runon Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 3.00 | 2.16 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 3.00 | 2.16 | 0.00 |
| 2.00 | 0.04 | 0.00 | 0.00 | 53.00 | 3.00 | 2.16 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 3.00 | 2.16 | 0.00 |
| 4.00 | 0.10 | 0.00 | 0.00 | 55.00 | 3.00 | 2.16 | 0.00 |
| 5.00 | 0.14 | 0.00 | 0.00 | 56.00 | 3.00 | 2.16 | 0.00 |
| 6.00 | 0.18 | 0.00 | 0.00 | 57.00 | 3.00 | 2.16 | 0.00 |
| 7.00 | 0.24 | 0.00 | 0.00 | 58.00 | 3.00 | 2.16 | 0.00 |
| 8.00 | 0.30 | 0.02 | 0.00 | 59.00 | 3.00 | 2.16 | 0.00 |
| 9.00 | 0.36 | 0.03 | 0.00 | 60.00 | 3.00 | 2.16 | 0.00 |
| 10.00 | 0.48 | 0.08 | 0.01 | 61.00 | 3.00 | 2.16 | 0.00 |
| 11.00 | 0.65 | 0.17 | 0.02 | 62.00 | 3.00 | 2.16 | 0.00 |
| 12.00 | 1.41 | 0.72 | 0.24 | 63.00 | 3.00 | 2.16 | 0.00 |
| 13.00 | 2.35 | 1.56 | 0.04 | 64.00 | 3.00 | 2.16 | 0.00 |
| 14.00 | 2.52 | 1.72 | 0.02 | 65.00 | 3.00 | 2.16 | 0.00 |
| 15.00 | 2.64 | 1.82 | 0.01 | 66.00 | 3.00 | 2.16 | 0.00 |
| 16.00 | 2.70 | 1.88 | 0.01 | 67.00 | 3.00 | 2.16 | 0.00 |
| 17.00 | 2.76 | 1.94 | 0.01 | 68.00 | 3.00 | 2.16 | 0.00 |
| 18.00 | 2.82 | 1.99 | 0.01 | 69.00 | 3.00 | 2.16 | 0.00 |
| 19.00 | 2.86 | 2.03 | 0.01 | 70.00 | 3.00 | 2.16 | 0.00 |
| 20.00 | 2.90 | 2.07 | 0.01 | 71.00 | 3.00 | 2.16 | 0.00 |
| 21.00 | 2.94 | 2.10 | 0.00 | 72.00 | 3.00 | 2.16 | 0.00 |
| 22.00 | 2.96 | 2.13 | 0.00 | | | | |
| 23.00 | 2.99 | 2.15 | 0.00 | | | | |
| 24.00 | 3.00 | 2.16 | 0.00 | | | | |
| 25.00 | 3.00 | 2.16 | 0.00 | | | | |
| 26.00 | 3.00 | 2.16 | 0.00 | | | | |
| 27.00 | 3.00 | 2.16 | 0.00 | | | | |
| 28.00 | 3.00 | 2.16 | 0.00 | | | | |
| 29.00 | 3.00 | 2.16 | 0.00 | | | | |
| 30.00 | 3.00 | 2.16 | 0.00 | | | | |
| 31.00 | 3.00 | 2.16 | 0.00 | | | | |
| 32.00 | 3.00 | 2.16 | 0.00 | | | | |
| 33.00 | 3.00 | 2.16 | 0.00 | | | | |
| 34.00 | 3.00 | 2.16 | 0.00 | | | | |
| 35.00 | 3.00 | 2.16 | 0.00 | | | | |
| 36.00 | 3.00 | 2.16 | 0.00 | | | | |
| 37.00 | 3.00 | 2.16 | 0.00 | | | | |
| 38.00 | 3.00 | 2.16 | 0.00 | | | | |
| 39.00 | 3.00 | 2.16 | 0.00 | | | | |
| 40.00 | 3.00 | 2.16 | 0.00 | | | | |
| 41.00 | 3.00 | 2.16 | 0.00 | | | | |
| 42.00 | 3.00 | 2.16 | 0.00 | | | | |
| 43.00 | 3.00 | 2.16 | 0.00 | | | | |
| 44.00 | 3.00 | 2.16 | 0.00 | | | | |
| 45.00 | 3.00 | 2.16 | 0.00 | | | | |
| 46.00 | 3.00 | 2.16 | 0.00 | | | | |
| 47.00 | 3.00 | 2.16 | 0.00 | | | | |
| 48.00 | 3.00 | 2.16 | 0.00 | | | | |
| 49.00 | 3.00 | 2.16 | 0.00 | | | | |
| 50.00 | 3.00 | 2.16 | 0.00 | | | | |

Retreat Center - Copy3

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Proposed Conditions
MSE 24-hr 4 2-Year Rainfall=3.00"
 Printed 9/16/2024
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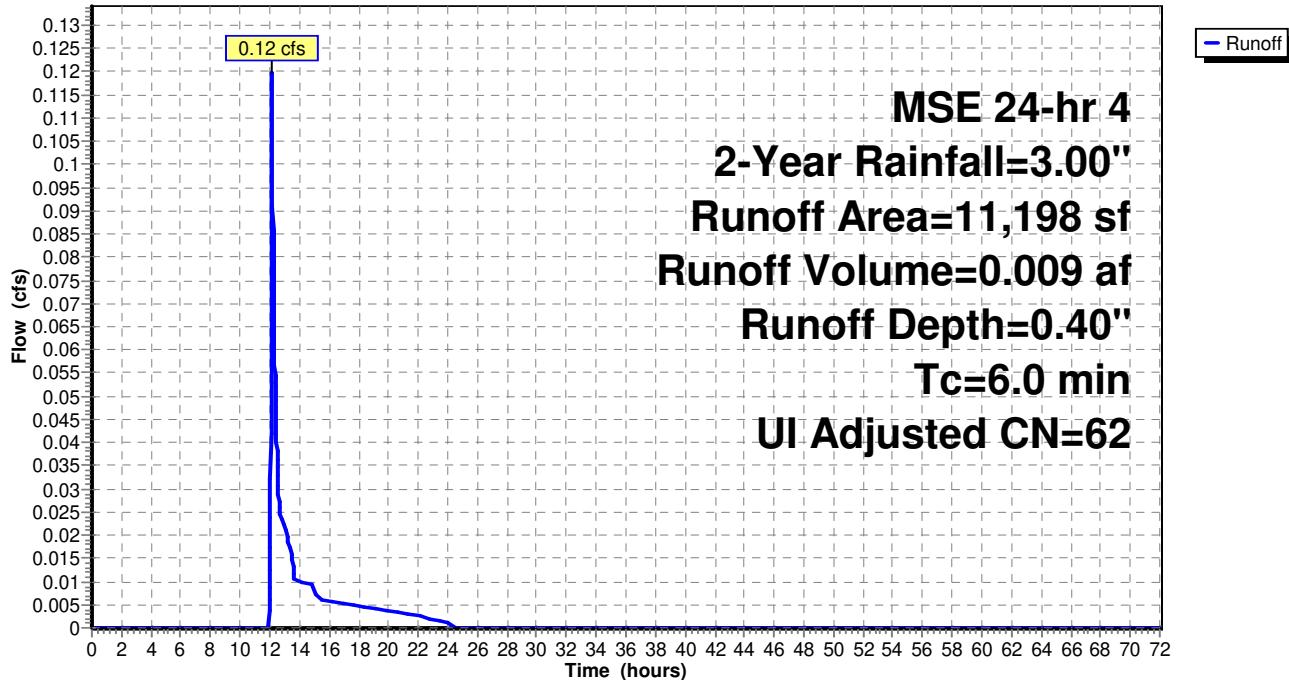
Summary for Subcatchment A3: Project Undetained

Runoff = 0.12 cfs @ 12.15 hrs, Volume= 0.009 af, Depth= 0.40"
 Routed to Reach R2 : Post Developed

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 2-Year Rainfall=3.00"

| Area (sf) | CN | Adj | Description |
|-----------|----|-----|-------------------------------|
| 739 | 98 | | Unconnected pavement, HSG B |
| 10,459 | 61 | | >75% Grass cover, Good, HSG B |
| 11,198 | 63 | 62 | Weighted Average, UI Adjusted |
| 10,459 | | | 93.40% Pervious Area |
| 739 | | | 6.60% Impervious Area |
| 739 | | | 100.00% Unconnected |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A3: Project Undetained**Hydrograph**

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MSE 24-hr 4 2-Year Rainfall=3.00"
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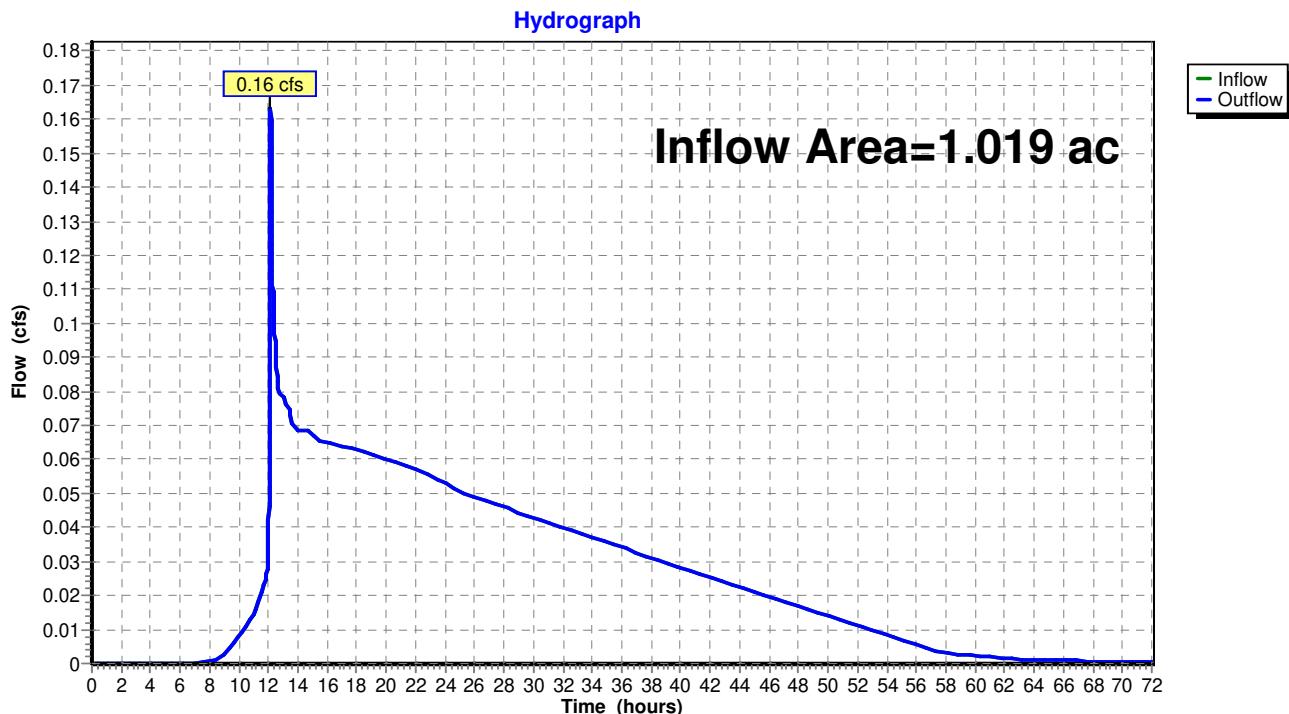
Hydrograph for Subcatchment A3: Project Undetained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 3.00 | 0.40 | 0.00 |
| 1.00 | 0.01 | 0.00 | 0.00 | 52.00 | 3.00 | 0.40 | 0.00 |
| 2.00 | 0.04 | 0.00 | 0.00 | 53.00 | 3.00 | 0.40 | 0.00 |
| 3.00 | 0.06 | 0.00 | 0.00 | 54.00 | 3.00 | 0.40 | 0.00 |
| 4.00 | 0.10 | 0.00 | 0.00 | 55.00 | 3.00 | 0.40 | 0.00 |
| 5.00 | 0.14 | 0.00 | 0.00 | 56.00 | 3.00 | 0.40 | 0.00 |
| 6.00 | 0.18 | 0.00 | 0.00 | 57.00 | 3.00 | 0.40 | 0.00 |
| 7.00 | 0.24 | 0.00 | 0.00 | 58.00 | 3.00 | 0.40 | 0.00 |
| 8.00 | 0.30 | 0.00 | 0.00 | 59.00 | 3.00 | 0.40 | 0.00 |
| 9.00 | 0.36 | 0.00 | 0.00 | 60.00 | 3.00 | 0.40 | 0.00 |
| 10.00 | 0.48 | 0.00 | 0.00 | 61.00 | 3.00 | 0.40 | 0.00 |
| 11.00 | 0.65 | 0.00 | 0.00 | 62.00 | 3.00 | 0.40 | 0.00 |
| 12.00 | 1.41 | 0.01 | 0.00 | 63.00 | 3.00 | 0.40 | 0.00 |
| 13.00 | 2.35 | 0.17 | 0.02 | 64.00 | 3.00 | 0.40 | 0.00 |
| 14.00 | 2.52 | 0.23 | 0.01 | 65.00 | 3.00 | 0.40 | 0.00 |
| 15.00 | 2.64 | 0.26 | 0.01 | 66.00 | 3.00 | 0.40 | 0.00 |
| 16.00 | 2.70 | 0.29 | 0.01 | 67.00 | 3.00 | 0.40 | 0.00 |
| 17.00 | 2.76 | 0.31 | 0.01 | 68.00 | 3.00 | 0.40 | 0.00 |
| 18.00 | 2.82 | 0.33 | 0.00 | 69.00 | 3.00 | 0.40 | 0.00 |
| 19.00 | 2.86 | 0.34 | 0.00 | 70.00 | 3.00 | 0.40 | 0.00 |
| 20.00 | 2.90 | 0.36 | 0.00 | 71.00 | 3.00 | 0.40 | 0.00 |
| 21.00 | 2.94 | 0.37 | 0.00 | 72.00 | 3.00 | 0.40 | 0.00 |
| 22.00 | 2.96 | 0.38 | 0.00 | | | | |
| 23.00 | 2.99 | 0.39 | 0.00 | | | | |
| 24.00 | 3.00 | 0.40 | 0.00 | | | | |
| 25.00 | 3.00 | 0.40 | 0.00 | | | | |
| 26.00 | 3.00 | 0.40 | 0.00 | | | | |
| 27.00 | 3.00 | 0.40 | 0.00 | | | | |
| 28.00 | 3.00 | 0.40 | 0.00 | | | | |
| 29.00 | 3.00 | 0.40 | 0.00 | | | | |
| 30.00 | 3.00 | 0.40 | 0.00 | | | | |
| 31.00 | 3.00 | 0.40 | 0.00 | | | | |
| 32.00 | 3.00 | 0.40 | 0.00 | | | | |
| 33.00 | 3.00 | 0.40 | 0.00 | | | | |
| 34.00 | 3.00 | 0.40 | 0.00 | | | | |
| 35.00 | 3.00 | 0.40 | 0.00 | | | | |
| 36.00 | 3.00 | 0.40 | 0.00 | | | | |
| 37.00 | 3.00 | 0.40 | 0.00 | | | | |
| 38.00 | 3.00 | 0.40 | 0.00 | | | | |
| 39.00 | 3.00 | 0.40 | 0.00 | | | | |
| 40.00 | 3.00 | 0.40 | 0.00 | | | | |
| 41.00 | 3.00 | 0.40 | 0.00 | | | | |
| 42.00 | 3.00 | 0.40 | 0.00 | | | | |
| 43.00 | 3.00 | 0.40 | 0.00 | | | | |
| 44.00 | 3.00 | 0.40 | 0.00 | | | | |
| 45.00 | 3.00 | 0.40 | 0.00 | | | | |
| 46.00 | 3.00 | 0.40 | 0.00 | | | | |
| 47.00 | 3.00 | 0.40 | 0.00 | | | | |
| 48.00 | 3.00 | 0.40 | 0.00 | | | | |
| 49.00 | 3.00 | 0.40 | 0.00 | | | | |
| 50.00 | 3.00 | 0.40 | 0.00 | | | | |

Summary for Reach R2: Post Developed

Inflow Area = 1.019 ac, 64.07% Impervious, Inflow Depth > 1.71" for 2-Year event
Inflow = 0.16 cfs @ 12.15 hrs, Volume= 0.145 af
Outflow = 0.16 cfs @ 12.15 hrs, Volume= 0.145 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R2: Post Developed

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Hydrograph for Reach R2: Post Developed

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.01 | 0.01 | 0.01 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.01 | 0.01 | 0.01 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.01 | 0.01 | 0.01 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.01 | 0.01 | 0.01 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.01 | 0.01 | 0.01 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.01 | 0.01 | 0.01 |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.00 | 0.00 | 0.00 |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.00 | 0.00 | 0.00 |
| 8.00 | 0.00 | 0.00 | 0.00 | 59.00 | 0.00 | 0.00 | 0.00 |
| 9.00 | 0.00 | 0.00 | 0.00 | 60.00 | 0.00 | 0.00 | 0.00 |
| 10.00 | 0.01 | 0.01 | 0.01 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.01 | 0.01 | 0.01 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 0.04 | 0.04 | 0.04 | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.08 | 0.08 | 0.08 | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.07 | 0.07 | 0.07 | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.07 | 0.07 | 0.07 | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.06 | 0.06 | 0.06 | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.06 | 0.06 | 0.06 | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.06 | 0.06 | 0.06 | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.06 | 0.06 | 0.06 | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.06 | 0.06 | 0.06 | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.06 | 0.06 | 0.06 | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.06 | 0.06 | | | | | |
| 23.00 | 0.06 | 0.06 | | | | | |
| 24.00 | 0.05 | 0.05 | | | | | |
| 25.00 | 0.05 | 0.05 | | | | | |
| 26.00 | 0.05 | 0.05 | | | | | |
| 27.00 | 0.05 | 0.05 | | | | | |
| 28.00 | 0.05 | 0.05 | | | | | |
| 29.00 | 0.04 | 0.04 | | | | | |
| 30.00 | 0.04 | 0.04 | | | | | |
| 31.00 | 0.04 | 0.04 | | | | | |
| 32.00 | 0.04 | 0.04 | | | | | |
| 33.00 | 0.04 | 0.04 | | | | | |
| 34.00 | 0.04 | 0.04 | | | | | |
| 35.00 | 0.04 | 0.04 | | | | | |
| 36.00 | 0.03 | 0.03 | | | | | |
| 37.00 | 0.03 | 0.03 | | | | | |
| 38.00 | 0.03 | 0.03 | | | | | |
| 39.00 | 0.03 | 0.03 | | | | | |
| 40.00 | 0.03 | 0.03 | | | | | |
| 41.00 | 0.03 | 0.03 | | | | | |
| 42.00 | 0.03 | 0.03 | | | | | |
| 43.00 | 0.02 | 0.02 | | | | | |
| 44.00 | 0.02 | 0.02 | | | | | |
| 45.00 | 0.02 | 0.02 | | | | | |
| 46.00 | 0.02 | 0.02 | | | | | |
| 47.00 | 0.02 | 0.02 | | | | | |
| 48.00 | 0.02 | 0.02 | | | | | |
| 49.00 | 0.02 | 0.02 | | | | | |
| 50.00 | 0.01 | 0.01 | | | | | |

Retreat Center - Copy3

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MSE 24-hr 4 2-Year Rainfall=3.00"
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Summary for Pond 1P: Oversized Pipe

Inflow Area = 0.762 ac, 83.46% Impervious, Inflow Depth = 2.16" for 2-Year event
Inflow = 2.56 cfs @ 12.13 hrs, Volume= 0.137 af
Outflow = 0.06 cfs @ 15.10 hrs, Volume= 0.136 af, Atten= 98%, Lag= 177.9 min
Primary = 0.06 cfs @ 15.10 hrs, Volume= 0.136 af

Routed to Reach R2 : Post Developed

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Starting Elev= 784.00' Surf.Area= 0.041 ac Storage= 0.111 af
Peak Elev= 786.52' @ 15.10 hrs Surf.Area= 0.033 ac Storage= 0.209 af (0.098 af above start)

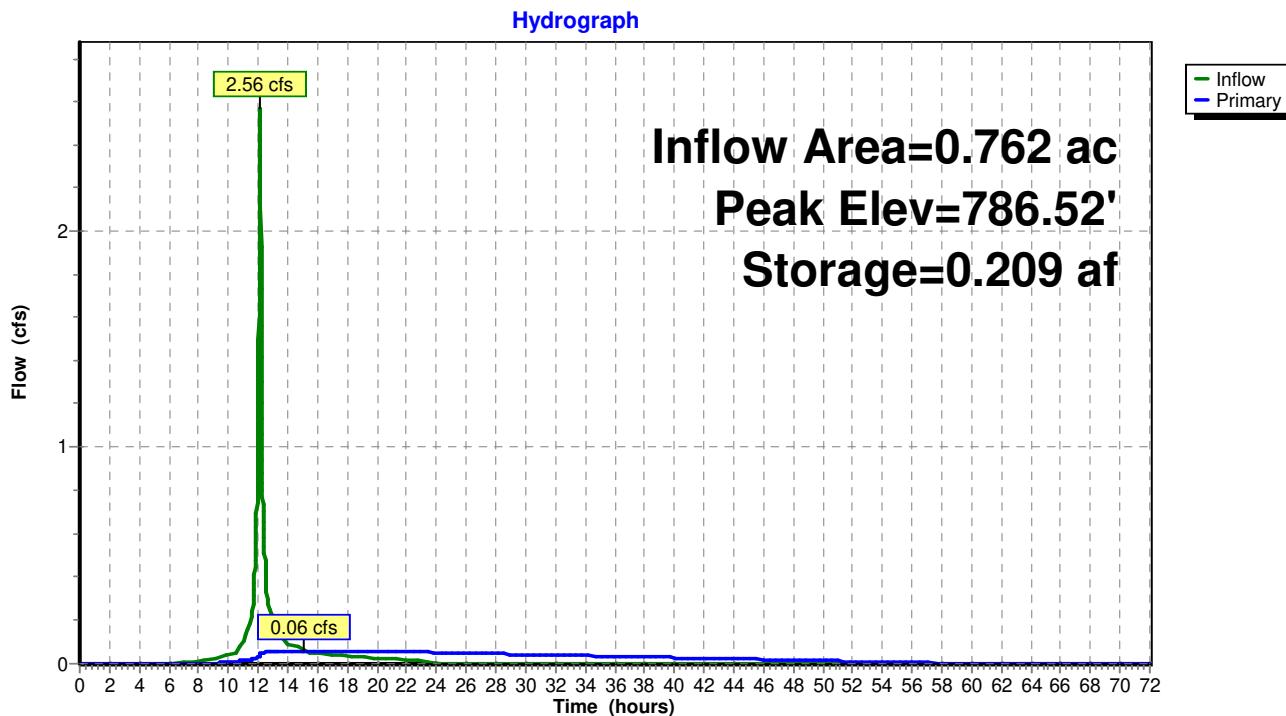
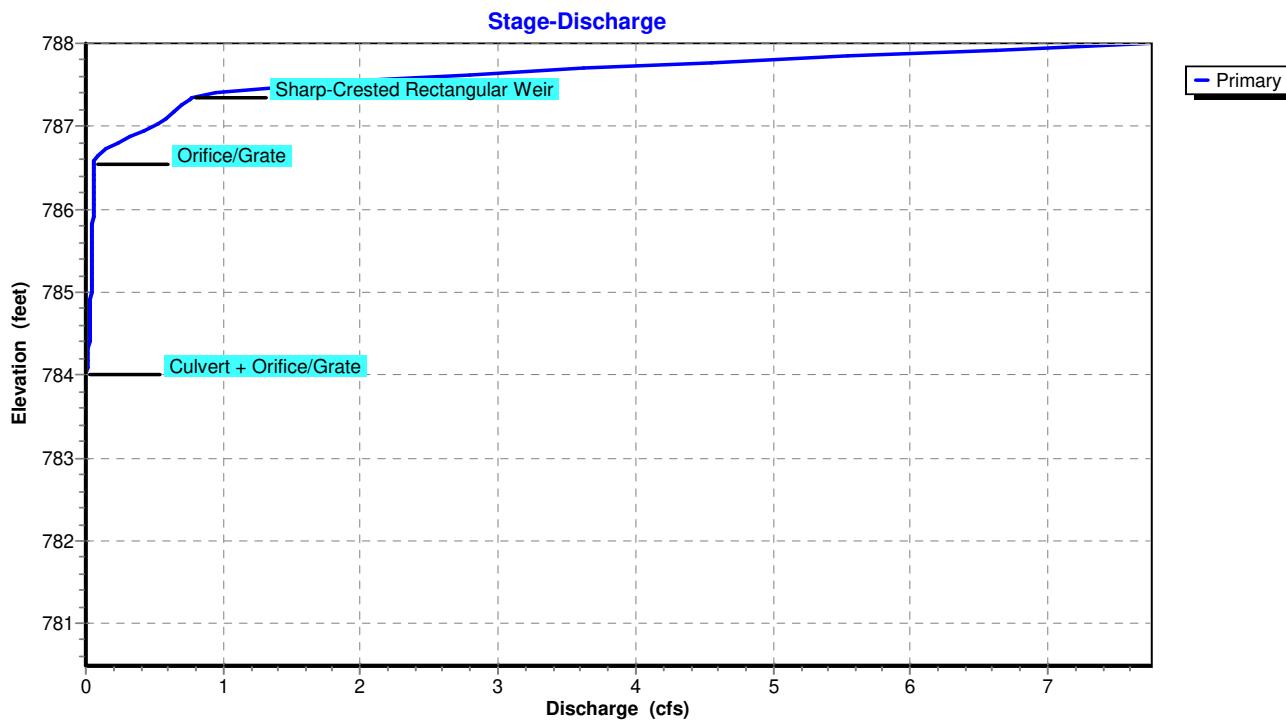
Plug-Flow detention time= 2,185.8 min calculated for 0.025 af (18% of inflow)
Center-of-Mass det. time= 901.2 min (1,692.6 - 791.4)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 780.50' | 0.243 af | 90.0" Round Pipe Storage L= 240.0' |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 784.00' | 18.0" Round Culvert L= 19.0' RCP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 784.00' / 783.75' S= 0.0132 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 1.77 sf |
| #2 | Device 1 | 784.00' | 1.2" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #3 | Device 1 | 786.55' | 6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 787.35' | 4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s) |

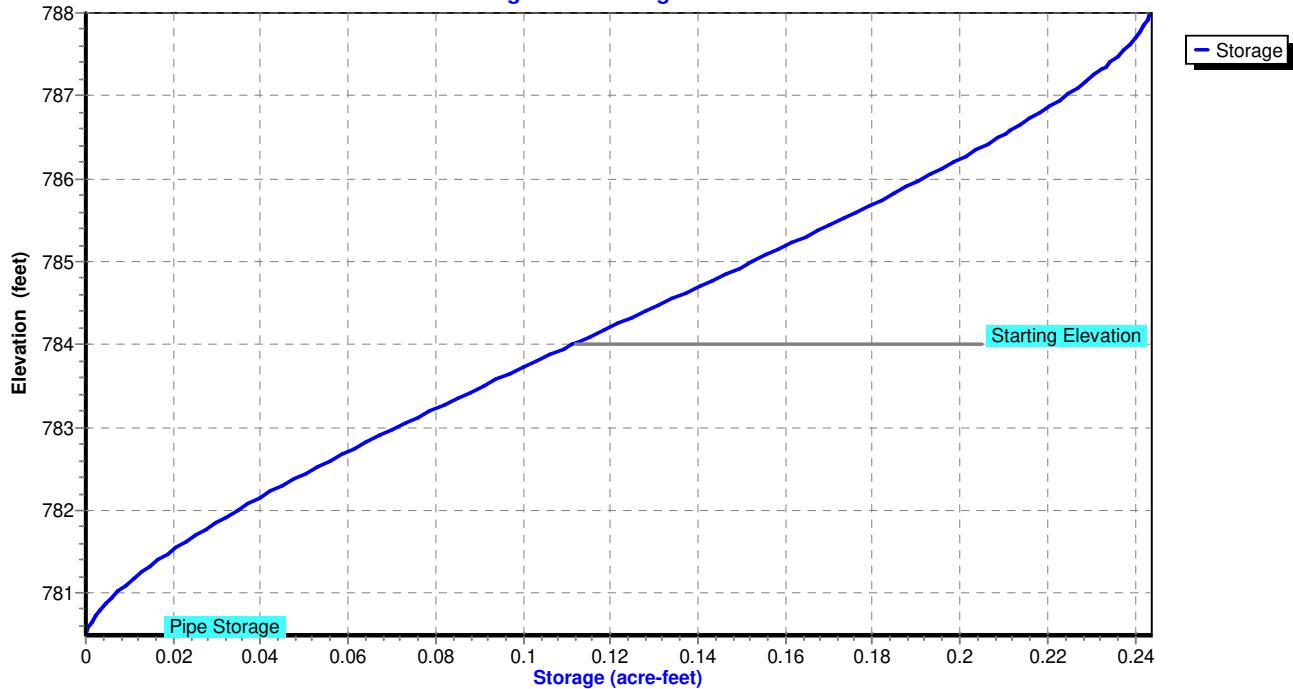
Primary OutFlow Max=0.06 cfs @ 15.10 hrs HW=786.52' TW=0.00' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 0.06 cfs of 9.99 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 0.06 cfs @ 7.57 fps)
- 3=Orifice/Grate (Controls 0.00 cfs)
- 4=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: Oversized Pipe**Pond 1P: Oversized Pipe**

Pond 1P: Oversized Pipe

Stage-Area-Storage



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Hydrograph for Pond 1P: Oversized Pipe

| Time (hours) | Inflow (cfs) | Storage (acre-feet) | Elevation (feet) | Primary (cfs) |
|-----------------|-----------------|------------------------|---------------------|------------------|
| 0.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 2.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 4.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 6.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 8.00 | 0.01 | 0.112 | 784.02 | 0.00 |
| 10.00 | 0.04 | 0.115 | 784.10 | 0.01 |
| 12.00 | 1.23 | 0.143 | 784.77 | 0.03 |
| 14.00 | 0.09 | 0.207 | 786.46 | 0.06 |
| 16.00 | 0.05 | 0.209 | 786.49 | 0.06 |
| 18.00 | 0.04 | 0.206 | 786.41 | 0.06 |
| 20.00 | 0.03 | 0.201 | 786.28 | 0.06 |
| 22.00 | 0.02 | 0.196 | 786.13 | 0.05 |
| 24.00 | 0.01 | 0.189 | 785.95 | 0.05 |
| 26.00 | 0.00 | 0.181 | 785.73 | 0.05 |
| 28.00 | 0.00 | 0.173 | 785.52 | 0.05 |
| 30.00 | 0.00 | 0.166 | 785.34 | 0.04 |
| 32.00 | 0.00 | 0.159 | 785.16 | 0.04 |
| 34.00 | 0.00 | 0.153 | 785.01 | 0.04 |
| 36.00 | 0.00 | 0.147 | 784.86 | 0.03 |
| 38.00 | 0.00 | 0.141 | 784.73 | 0.03 |
| 40.00 | 0.00 | 0.137 | 784.61 | 0.03 |
| 42.00 | 0.00 | 0.132 | 784.50 | 0.03 |
| 44.00 | 0.00 | 0.128 | 784.41 | 0.02 |
| 46.00 | 0.00 | 0.125 | 784.32 | 0.02 |
| 48.00 | 0.00 | 0.122 | 784.25 | 0.02 |
| 50.00 | 0.00 | 0.119 | 784.19 | 0.01 |
| 52.00 | 0.00 | 0.117 | 784.14 | 0.01 |
| 54.00 | 0.00 | 0.115 | 784.10 | 0.01 |
| 56.00 | 0.00 | 0.114 | 784.07 | 0.01 |
| 58.00 | 0.00 | 0.114 | 784.05 | 0.00 |
| 60.00 | 0.00 | 0.113 | 784.04 | 0.00 |
| 62.00 | 0.00 | 0.113 | 784.03 | 0.00 |
| 64.00 | 0.00 | 0.113 | 784.03 | 0.00 |
| 66.00 | 0.00 | 0.112 | 784.03 | 0.00 |
| 68.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 70.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 72.00 | 0.00 | 0.112 | 784.02 | 0.00 |

Retreat Center - Copy3

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Stage-Discharge for Pond 1P: Oversized Pipe

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 780.50 | 0.00 | 783.05 | 0.00 | 785.60 | 0.05 |
| 780.55 | 0.00 | 783.10 | 0.00 | 785.65 | 0.05 |
| 780.60 | 0.00 | 783.15 | 0.00 | 785.70 | 0.05 |
| 780.65 | 0.00 | 783.20 | 0.00 | 785.75 | 0.05 |
| 780.70 | 0.00 | 783.25 | 0.00 | 785.80 | 0.05 |
| 780.75 | 0.00 | 783.30 | 0.00 | 785.85 | 0.05 |
| 780.80 | 0.00 | 783.35 | 0.00 | 785.90 | 0.05 |
| 780.85 | 0.00 | 783.40 | 0.00 | 785.95 | 0.05 |
| 780.90 | 0.00 | 783.45 | 0.00 | 786.00 | 0.05 |
| 780.95 | 0.00 | 783.50 | 0.00 | 786.05 | 0.05 |
| 781.00 | 0.00 | 783.55 | 0.00 | 786.10 | 0.05 |
| 781.05 | 0.00 | 783.60 | 0.00 | 786.15 | 0.05 |
| 781.10 | 0.00 | 783.65 | 0.00 | 786.20 | 0.06 |
| 781.15 | 0.00 | 783.70 | 0.00 | 786.25 | 0.06 |
| 781.20 | 0.00 | 783.75 | 0.00 | 786.30 | 0.06 |
| 781.25 | 0.00 | 783.80 | 0.00 | 786.35 | 0.06 |
| 781.30 | 0.00 | 783.85 | 0.00 | 786.40 | 0.06 |
| 781.35 | 0.00 | 783.90 | 0.00 | 786.45 | 0.06 |
| 781.40 | 0.00 | 783.95 | 0.00 | 786.50 | 0.06 |
| 781.45 | 0.00 | 784.00 | 0.00 | 786.55 | 0.06 |
| 781.50 | 0.00 | 784.05 | 0.00 | 786.60 | 0.07 |
| 781.55 | 0.00 | 784.10 | 0.01 | 786.65 | 0.09 |
| 781.60 | 0.00 | 784.15 | 0.01 | 786.70 | 0.13 |
| 781.65 | 0.00 | 784.20 | 0.01 | 786.75 | 0.17 |
| 781.70 | 0.00 | 784.25 | 0.02 | 786.80 | 0.23 |
| 781.75 | 0.00 | 784.30 | 0.02 | 786.85 | 0.29 |
| 781.80 | 0.00 | 784.35 | 0.02 | 786.90 | 0.36 |
| 781.85 | 0.00 | 784.40 | 0.02 | 786.95 | 0.43 |
| 781.90 | 0.00 | 784.45 | 0.02 | 787.00 | 0.49 |
| 781.95 | 0.00 | 784.50 | 0.03 | 787.05 | 0.54 |
| 782.00 | 0.00 | 784.55 | 0.03 | 787.10 | 0.58 |
| 782.05 | 0.00 | 784.60 | 0.03 | 787.15 | 0.63 |
| 782.10 | 0.00 | 784.65 | 0.03 | 787.20 | 0.67 |
| 782.15 | 0.00 | 784.70 | 0.03 | 787.25 | 0.70 |
| 782.20 | 0.00 | 784.75 | 0.03 | 787.30 | 0.74 |
| 782.25 | 0.00 | 784.80 | 0.03 | 787.35 | 0.77 |
| 782.30 | 0.00 | 784.85 | 0.03 | 787.40 | 0.95 |
| 782.35 | 0.00 | 784.90 | 0.03 | 787.45 | 1.24 |
| 782.40 | 0.00 | 784.95 | 0.04 | 787.50 | 1.62 |
| 782.45 | 0.00 | 785.00 | 0.04 | 787.55 | 2.05 |
| 782.50 | 0.00 | 785.05 | 0.04 | 787.60 | 2.53 |
| 782.55 | 0.00 | 785.10 | 0.04 | 787.65 | 3.06 |
| 782.60 | 0.00 | 785.15 | 0.04 | 787.70 | 3.63 |
| 782.65 | 0.00 | 785.20 | 0.04 | 787.75 | 4.24 |
| 782.70 | 0.00 | 785.25 | 0.04 | 787.80 | 4.88 |
| 782.75 | 0.00 | 785.30 | 0.04 | 787.85 | 5.55 |
| 782.80 | 0.00 | 785.35 | 0.04 | 787.90 | 6.25 |
| 782.85 | 0.00 | 785.40 | 0.04 | 787.95 | 6.99 |
| 782.90 | 0.00 | 785.45 | 0.04 | 788.00 | 7.74 |
| 782.95 | 0.00 | 785.50 | 0.05 | | |
| 783.00 | 0.00 | 785.55 | 0.05 | | |

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Stage-Area-Storage for Pond 1P: Oversized Pipe

| Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) |
|---------------------|------------------------|---------------------|------------------------|---------------------|------------------------|
| 780.50 | 0.000 | 783.05 | 0.073 | 785.60 | 0.176 |
| 780.55 | 0.000 | 783.10 | 0.075 | 785.65 | 0.178 |
| 780.60 | 0.001 | 783.15 | 0.077 | 785.70 | 0.180 |
| 780.65 | 0.001 | 783.20 | 0.079 | 785.75 | 0.182 |
| 780.70 | 0.002 | 783.25 | 0.081 | 785.80 | 0.184 |
| 780.75 | 0.002 | 783.30 | 0.083 | 785.85 | 0.186 |
| 780.80 | 0.003 | 783.35 | 0.085 | 785.90 | 0.188 |
| 780.85 | 0.004 | 783.40 | 0.087 | 785.95 | 0.189 |
| 780.90 | 0.005 | 783.45 | 0.089 | 786.00 | 0.191 |
| 780.95 | 0.006 | 783.50 | 0.091 | 786.05 | 0.193 |
| 781.00 | 0.007 | 783.55 | 0.093 | 786.10 | 0.195 |
| 781.05 | 0.008 | 783.60 | 0.095 | 786.15 | 0.197 |
| 781.10 | 0.009 | 783.65 | 0.097 | 786.20 | 0.198 |
| 781.15 | 0.010 | 783.70 | 0.099 | 786.25 | 0.200 |
| 781.20 | 0.011 | 783.75 | 0.101 | 786.30 | 0.202 |
| 781.25 | 0.013 | 783.80 | 0.103 | 786.35 | 0.204 |
| 781.30 | 0.014 | 783.85 | 0.105 | 786.40 | 0.205 |
| 781.35 | 0.015 | 783.90 | 0.107 | 786.45 | 0.207 |
| 781.40 | 0.017 | 783.95 | 0.109 | 786.50 | 0.209 |
| 781.45 | 0.018 | 784.00 | 0.111 | 786.55 | 0.210 |
| 781.50 | 0.019 | 784.05 | 0.113 | 786.60 | 0.212 |
| 781.55 | 0.021 | 784.10 | 0.116 | 786.65 | 0.214 |
| 781.60 | 0.022 | 784.15 | 0.118 | 786.70 | 0.215 |
| 781.65 | 0.024 | 784.20 | 0.120 | 786.75 | 0.217 |
| 781.70 | 0.025 | 784.25 | 0.122 | 786.80 | 0.218 |
| 781.75 | 0.027 | 784.30 | 0.124 | 786.85 | 0.220 |
| 781.80 | 0.028 | 784.35 | 0.126 | 786.90 | 0.221 |
| 781.85 | 0.030 | 784.40 | 0.128 | 786.95 | 0.223 |
| 781.90 | 0.031 | 784.45 | 0.130 | 787.00 | 0.224 |
| 781.95 | 0.033 | 784.50 | 0.132 | 787.05 | 0.226 |
| 782.00 | 0.035 | 784.55 | 0.134 | 787.10 | 0.227 |
| 782.05 | 0.036 | 784.60 | 0.136 | 787.15 | 0.228 |
| 782.10 | 0.038 | 784.65 | 0.138 | 787.20 | 0.229 |
| 782.15 | 0.040 | 784.70 | 0.140 | 787.25 | 0.231 |
| 782.20 | 0.041 | 784.75 | 0.142 | 787.30 | 0.232 |
| 782.25 | 0.043 | 784.80 | 0.144 | 787.35 | 0.233 |
| 782.30 | 0.045 | 784.85 | 0.146 | 787.40 | 0.234 |
| 782.35 | 0.047 | 784.90 | 0.148 | 787.45 | 0.235 |
| 782.40 | 0.048 | 784.95 | 0.150 | 787.50 | 0.236 |
| 782.45 | 0.050 | 785.00 | 0.152 | 787.55 | 0.237 |
| 782.50 | 0.052 | 785.05 | 0.155 | 787.60 | 0.238 |
| 782.55 | 0.054 | 785.10 | 0.157 | 787.65 | 0.239 |
| 782.60 | 0.056 | 785.15 | 0.159 | 787.70 | 0.240 |
| 782.65 | 0.058 | 785.20 | 0.161 | 787.75 | 0.241 |
| 782.70 | 0.060 | 785.25 | 0.163 | 787.80 | 0.242 |
| 782.75 | 0.061 | 785.30 | 0.165 | 787.85 | 0.242 |
| 782.80 | 0.063 | 785.35 | 0.166 | 787.90 | 0.243 |
| 782.85 | 0.065 | 785.40 | 0.168 | 787.95 | 0.243 |
| 782.90 | 0.067 | 785.45 | 0.170 | 788.00 | 0.243 |
| 782.95 | 0.069 | 785.50 | 0.172 | | |
| 783.00 | 0.071 | 785.55 | 0.174 | | |

Retreat Center - Copy3

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Proposed Conditions
MSE 24-hr 4 10-Year Rainfall=4.44"
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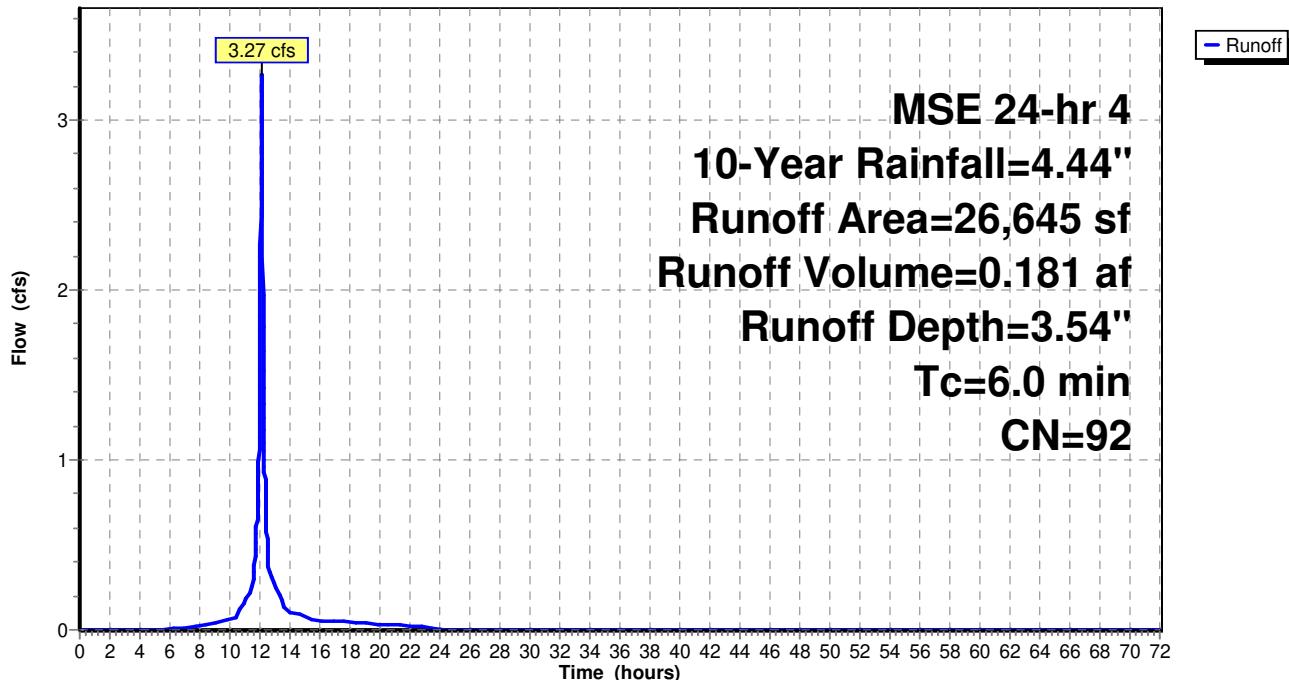
Summary for Subcatchment A1: Project Detained

Runoff = 3.27 cfs @ 12.13 hrs, Volume= 0.181 af, Depth= 3.54"
Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 10-Year Rainfall=4.44"

| Area (sf) | CN | Description |
|-----------|-------|-------------------------------|
| 13,722 | 98 | Paved parking, HSG B |
| * | 8,443 | Roof |
| 4,480 | 61 | >75% Grass cover, Good, HSG B |
| 26,645 | 92 | Weighted Average |
| 4,480 | | 16.81% Pervious Area |
| 22,165 | | 83.19% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A1: Project Detained**Hydrograph**

Hydrograph for Subcatchment A1: Project Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 4.44 | 3.54 | 0.00 |
| 1.00 | 0.02 | 0.00 | 0.00 | 52.00 | 4.44 | 3.54 | 0.00 |
| 2.00 | 0.05 | 0.00 | 0.00 | 53.00 | 4.44 | 3.54 | 0.00 |
| 3.00 | 0.09 | 0.00 | 0.00 | 54.00 | 4.44 | 3.54 | 0.00 |
| 4.00 | 0.14 | 0.00 | 0.00 | 55.00 | 4.44 | 3.54 | 0.00 |
| 5.00 | 0.20 | 0.00 | 0.00 | 56.00 | 4.44 | 3.54 | 0.00 |
| 6.00 | 0.27 | 0.01 | 0.01 | 57.00 | 4.44 | 3.54 | 0.00 |
| 7.00 | 0.35 | 0.03 | 0.02 | 58.00 | 4.44 | 3.54 | 0.00 |
| 8.00 | 0.44 | 0.06 | 0.02 | 59.00 | 4.44 | 3.54 | 0.00 |
| 9.00 | 0.54 | 0.11 | 0.03 | 60.00 | 4.44 | 3.54 | 0.00 |
| 10.00 | 0.70 | 0.20 | 0.07 | 61.00 | 4.44 | 3.54 | 0.00 |
| 11.00 | 0.96 | 0.37 | 0.17 | 62.00 | 4.44 | 3.54 | 0.00 |
| 12.00 | 2.08 | 1.31 | 1.62 | 63.00 | 4.44 | 3.54 | 0.00 |
| 13.00 | 3.48 | 2.62 | 0.26 | 64.00 | 4.44 | 3.54 | 0.00 |
| 14.00 | 3.74 | 2.86 | 0.11 | 65.00 | 4.44 | 3.54 | 0.00 |
| 15.00 | 3.90 | 3.02 | 0.09 | 66.00 | 4.44 | 3.54 | 0.00 |
| 16.00 | 4.00 | 3.12 | 0.06 | 67.00 | 4.44 | 3.54 | 0.00 |
| 17.00 | 4.09 | 3.20 | 0.05 | 68.00 | 4.44 | 3.54 | 0.00 |
| 18.00 | 4.17 | 3.28 | 0.04 | 69.00 | 4.44 | 3.54 | 0.00 |
| 19.00 | 4.24 | 3.35 | 0.04 | 70.00 | 4.44 | 3.54 | 0.00 |
| 20.00 | 4.30 | 3.40 | 0.03 | 71.00 | 4.44 | 3.54 | 0.00 |
| 21.00 | 4.35 | 3.45 | 0.03 | 72.00 | 4.44 | 3.54 | 0.00 |
| 22.00 | 4.39 | 3.49 | 0.02 | | | | |
| 23.00 | 4.42 | 3.52 | 0.02 | | | | |
| 24.00 | 4.44 | 3.54 | 0.01 | | | | |
| 25.00 | 4.44 | 3.54 | 0.00 | | | | |
| 26.00 | 4.44 | 3.54 | 0.00 | | | | |
| 27.00 | 4.44 | 3.54 | 0.00 | | | | |
| 28.00 | 4.44 | 3.54 | 0.00 | | | | |
| 29.00 | 4.44 | 3.54 | 0.00 | | | | |
| 30.00 | 4.44 | 3.54 | 0.00 | | | | |
| 31.00 | 4.44 | 3.54 | 0.00 | | | | |
| 32.00 | 4.44 | 3.54 | 0.00 | | | | |
| 33.00 | 4.44 | 3.54 | 0.00 | | | | |
| 34.00 | 4.44 | 3.54 | 0.00 | | | | |
| 35.00 | 4.44 | 3.54 | 0.00 | | | | |
| 36.00 | 4.44 | 3.54 | 0.00 | | | | |
| 37.00 | 4.44 | 3.54 | 0.00 | | | | |
| 38.00 | 4.44 | 3.54 | 0.00 | | | | |
| 39.00 | 4.44 | 3.54 | 0.00 | | | | |
| 40.00 | 4.44 | 3.54 | 0.00 | | | | |
| 41.00 | 4.44 | 3.54 | 0.00 | | | | |
| 42.00 | 4.44 | 3.54 | 0.00 | | | | |
| 43.00 | 4.44 | 3.54 | 0.00 | | | | |
| 44.00 | 4.44 | 3.54 | 0.00 | | | | |
| 45.00 | 4.44 | 3.54 | 0.00 | | | | |
| 46.00 | 4.44 | 3.54 | 0.00 | | | | |
| 47.00 | 4.44 | 3.54 | 0.00 | | | | |
| 48.00 | 4.44 | 3.54 | 0.00 | | | | |
| 49.00 | 4.44 | 3.54 | 0.00 | | | | |
| 50.00 | 4.44 | 3.54 | 0.00 | | | | |

Retreat Center - Copy3

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Proposed Conditions
MSE 24-hr 4 10-Year Rainfall=4.44"
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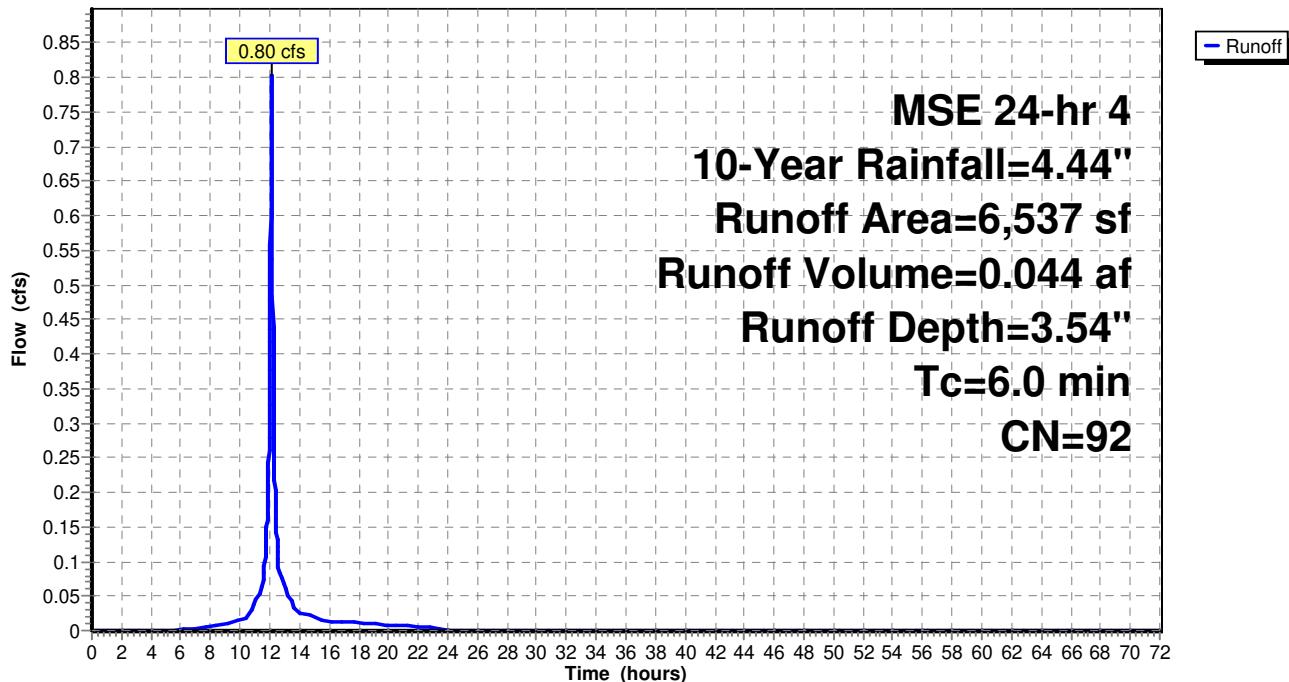
Summary for Subcatchment A2: Runon Detained

Runoff = 0.80 cfs @ 12.13 hrs, Volume= 0.044 af, Depth= 3.54"
 Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 10-Year Rainfall=4.44"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| * 5,529 | 98 | Roof |
| 1,008 | 61 | >75% Grass cover, Good, HSG B |
| 6,537 | 92 | Weighted Average |
| 1,008 | | 15.42% Pervious Area |
| 5,529 | | 84.58% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A2: Runon Detained**Hydrograph**

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Hydrograph for Subcatchment A2: Runon Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 4.44 | 3.54 | 0.00 |
| 1.00 | 0.02 | 0.00 | 0.00 | 52.00 | 4.44 | 3.54 | 0.00 |
| 2.00 | 0.05 | 0.00 | 0.00 | 53.00 | 4.44 | 3.54 | 0.00 |
| 3.00 | 0.09 | 0.00 | 0.00 | 54.00 | 4.44 | 3.54 | 0.00 |
| 4.00 | 0.14 | 0.00 | 0.00 | 55.00 | 4.44 | 3.54 | 0.00 |
| 5.00 | 0.20 | 0.00 | 0.00 | 56.00 | 4.44 | 3.54 | 0.00 |
| 6.00 | 0.27 | 0.01 | 0.00 | 57.00 | 4.44 | 3.54 | 0.00 |
| 7.00 | 0.35 | 0.03 | 0.00 | 58.00 | 4.44 | 3.54 | 0.00 |
| 8.00 | 0.44 | 0.06 | 0.01 | 59.00 | 4.44 | 3.54 | 0.00 |
| 9.00 | 0.54 | 0.11 | 0.01 | 60.00 | 4.44 | 3.54 | 0.00 |
| 10.00 | 0.70 | 0.20 | 0.02 | 61.00 | 4.44 | 3.54 | 0.00 |
| 11.00 | 0.96 | 0.37 | 0.04 | 62.00 | 4.44 | 3.54 | 0.00 |
| 12.00 | 2.08 | 1.31 | 0.40 | 63.00 | 4.44 | 3.54 | 0.00 |
| 13.00 | 3.48 | 2.62 | 0.06 | 64.00 | 4.44 | 3.54 | 0.00 |
| 14.00 | 3.74 | 2.86 | 0.03 | 65.00 | 4.44 | 3.54 | 0.00 |
| 15.00 | 3.90 | 3.02 | 0.02 | 66.00 | 4.44 | 3.54 | 0.00 |
| 16.00 | 4.00 | 3.12 | 0.01 | 67.00 | 4.44 | 3.54 | 0.00 |
| 17.00 | 4.09 | 3.20 | 0.01 | 68.00 | 4.44 | 3.54 | 0.00 |
| 18.00 | 4.17 | 3.28 | 0.01 | 69.00 | 4.44 | 3.54 | 0.00 |
| 19.00 | 4.24 | 3.35 | 0.01 | 70.00 | 4.44 | 3.54 | 0.00 |
| 20.00 | 4.30 | 3.40 | 0.01 | 71.00 | 4.44 | 3.54 | 0.00 |
| 21.00 | 4.35 | 3.45 | 0.01 | 72.00 | 4.44 | 3.54 | 0.00 |
| 22.00 | 4.39 | 3.49 | 0.01 | | | | |
| 23.00 | 4.42 | 3.52 | 0.00 | | | | |
| 24.00 | 4.44 | 3.54 | 0.00 | | | | |
| 25.00 | 4.44 | 3.54 | 0.00 | | | | |
| 26.00 | 4.44 | 3.54 | 0.00 | | | | |
| 27.00 | 4.44 | 3.54 | 0.00 | | | | |
| 28.00 | 4.44 | 3.54 | 0.00 | | | | |
| 29.00 | 4.44 | 3.54 | 0.00 | | | | |
| 30.00 | 4.44 | 3.54 | 0.00 | | | | |
| 31.00 | 4.44 | 3.54 | 0.00 | | | | |
| 32.00 | 4.44 | 3.54 | 0.00 | | | | |
| 33.00 | 4.44 | 3.54 | 0.00 | | | | |
| 34.00 | 4.44 | 3.54 | 0.00 | | | | |
| 35.00 | 4.44 | 3.54 | 0.00 | | | | |
| 36.00 | 4.44 | 3.54 | 0.00 | | | | |
| 37.00 | 4.44 | 3.54 | 0.00 | | | | |
| 38.00 | 4.44 | 3.54 | 0.00 | | | | |
| 39.00 | 4.44 | 3.54 | 0.00 | | | | |
| 40.00 | 4.44 | 3.54 | 0.00 | | | | |
| 41.00 | 4.44 | 3.54 | 0.00 | | | | |
| 42.00 | 4.44 | 3.54 | 0.00 | | | | |
| 43.00 | 4.44 | 3.54 | 0.00 | | | | |
| 44.00 | 4.44 | 3.54 | 0.00 | | | | |
| 45.00 | 4.44 | 3.54 | 0.00 | | | | |
| 46.00 | 4.44 | 3.54 | 0.00 | | | | |
| 47.00 | 4.44 | 3.54 | 0.00 | | | | |
| 48.00 | 4.44 | 3.54 | 0.00 | | | | |
| 49.00 | 4.44 | 3.54 | 0.00 | | | | |
| 50.00 | 4.44 | 3.54 | 0.00 | | | | |

Retreat Center - Copy3

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MSE 24-hr 4 10-Year Rainfall=4.44"
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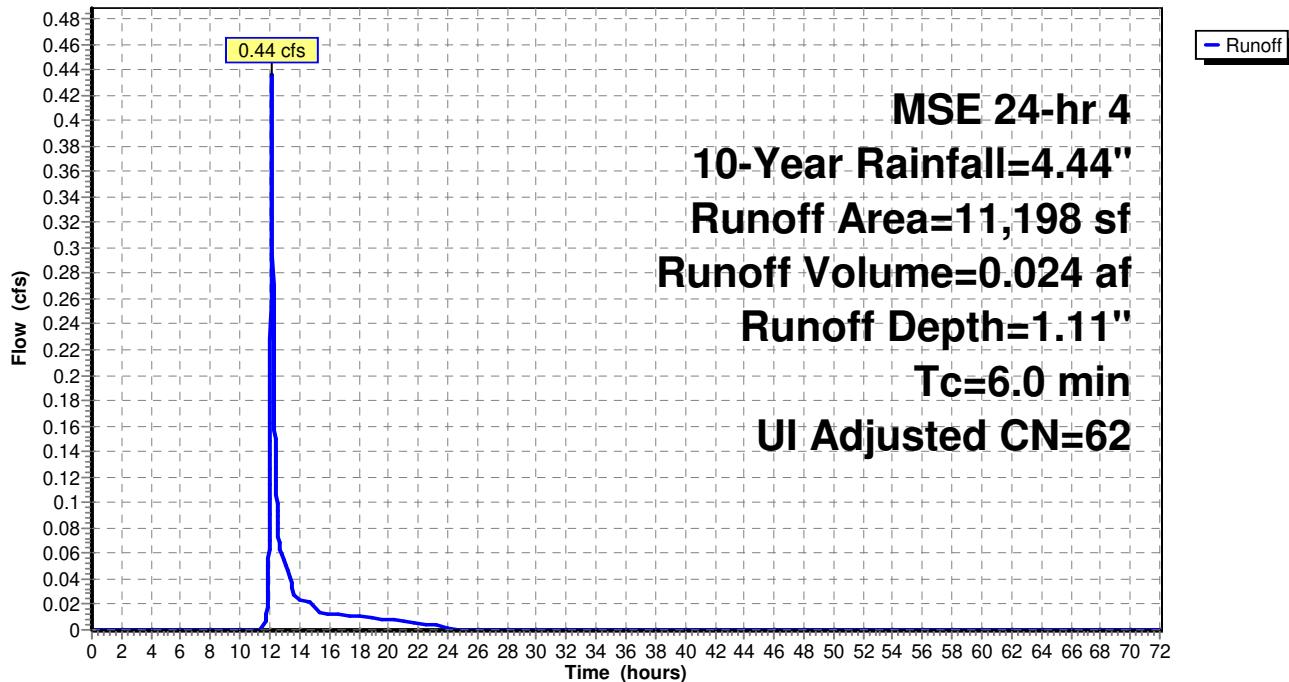
Summary for Subcatchment A3: Project Undetained

Runoff = 0.44 cfs @ 12.14 hrs, Volume= 0.024 af, Depth= 1.11"
Routed to Reach R2 : Post Developed

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 10-Year Rainfall=4.44"

| Area (sf) | CN | Adj | Description |
|-----------|----|-----|-------------------------------|
| 739 | 98 | | Unconnected pavement, HSG B |
| 10,459 | 61 | | >75% Grass cover, Good, HSG B |
| 11,198 | 63 | 62 | Weighted Average, UI Adjusted |
| 10,459 | | | 93.40% Pervious Area |
| 739 | | | 6.60% Impervious Area |
| 739 | | | 100.00% Unconnected |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-----|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A3: Project Undetained**Hydrograph**

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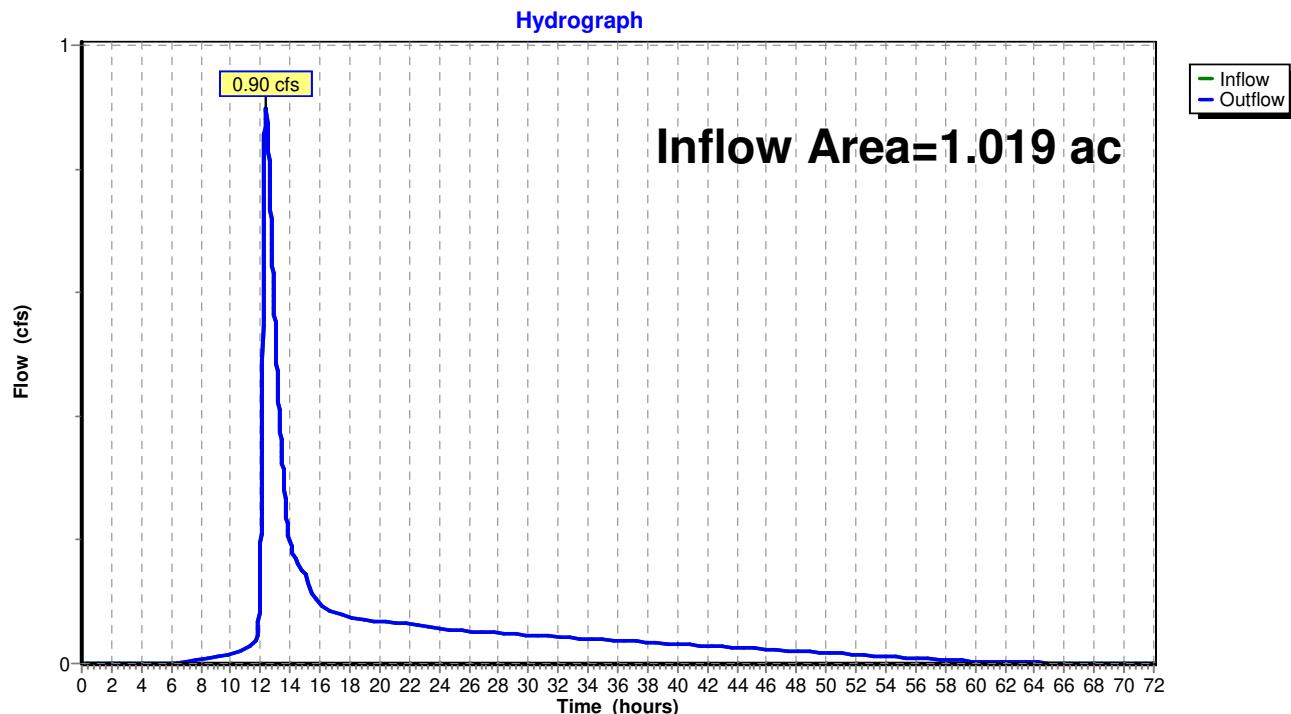
Hydrograph for Subcatchment A3: Project Undetained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 4.44 | 1.11 | 0.00 |
| 1.00 | 0.02 | 0.00 | 0.00 | 52.00 | 4.44 | 1.11 | 0.00 |
| 2.00 | 0.05 | 0.00 | 0.00 | 53.00 | 4.44 | 1.11 | 0.00 |
| 3.00 | 0.09 | 0.00 | 0.00 | 54.00 | 4.44 | 1.11 | 0.00 |
| 4.00 | 0.14 | 0.00 | 0.00 | 55.00 | 4.44 | 1.11 | 0.00 |
| 5.00 | 0.20 | 0.00 | 0.00 | 56.00 | 4.44 | 1.11 | 0.00 |
| 6.00 | 0.27 | 0.00 | 0.00 | 57.00 | 4.44 | 1.11 | 0.00 |
| 7.00 | 0.35 | 0.00 | 0.00 | 58.00 | 4.44 | 1.11 | 0.00 |
| 8.00 | 0.44 | 0.00 | 0.00 | 59.00 | 4.44 | 1.11 | 0.00 |
| 9.00 | 0.54 | 0.00 | 0.00 | 60.00 | 4.44 | 1.11 | 0.00 |
| 10.00 | 0.70 | 0.00 | 0.00 | 61.00 | 4.44 | 1.11 | 0.00 |
| 11.00 | 0.96 | 0.00 | 0.00 | 62.00 | 4.44 | 1.11 | 0.00 |
| 12.00 | 2.08 | 0.10 | 0.13 | 63.00 | 4.44 | 1.11 | 0.00 |
| 13.00 | 3.48 | 0.61 | 0.05 | 64.00 | 4.44 | 1.11 | 0.00 |
| 14.00 | 3.74 | 0.73 | 0.02 | 65.00 | 4.44 | 1.11 | 0.00 |
| 15.00 | 3.90 | 0.81 | 0.02 | 66.00 | 4.44 | 1.11 | 0.00 |
| 16.00 | 4.00 | 0.86 | 0.01 | 67.00 | 4.44 | 1.11 | 0.00 |
| 17.00 | 4.09 | 0.91 | 0.01 | 68.00 | 4.44 | 1.11 | 0.00 |
| 18.00 | 4.17 | 0.95 | 0.01 | 69.00 | 4.44 | 1.11 | 0.00 |
| 19.00 | 4.24 | 0.99 | 0.01 | 70.00 | 4.44 | 1.11 | 0.00 |
| 20.00 | 4.30 | 1.02 | 0.01 | 71.00 | 4.44 | 1.11 | 0.00 |
| 21.00 | 4.35 | 1.05 | 0.01 | 72.00 | 4.44 | 1.11 | 0.00 |
| 22.00 | 4.39 | 1.08 | 0.01 | | | | |
| 23.00 | 4.42 | 1.09 | 0.00 | | | | |
| 24.00 | 4.44 | 1.11 | 0.00 | | | | |
| 25.00 | 4.44 | 1.11 | 0.00 | | | | |
| 26.00 | 4.44 | 1.11 | 0.00 | | | | |
| 27.00 | 4.44 | 1.11 | 0.00 | | | | |
| 28.00 | 4.44 | 1.11 | 0.00 | | | | |
| 29.00 | 4.44 | 1.11 | 0.00 | | | | |
| 30.00 | 4.44 | 1.11 | 0.00 | | | | |
| 31.00 | 4.44 | 1.11 | 0.00 | | | | |
| 32.00 | 4.44 | 1.11 | 0.00 | | | | |
| 33.00 | 4.44 | 1.11 | 0.00 | | | | |
| 34.00 | 4.44 | 1.11 | 0.00 | | | | |
| 35.00 | 4.44 | 1.11 | 0.00 | | | | |
| 36.00 | 4.44 | 1.11 | 0.00 | | | | |
| 37.00 | 4.44 | 1.11 | 0.00 | | | | |
| 38.00 | 4.44 | 1.11 | 0.00 | | | | |
| 39.00 | 4.44 | 1.11 | 0.00 | | | | |
| 40.00 | 4.44 | 1.11 | 0.00 | | | | |
| 41.00 | 4.44 | 1.11 | 0.00 | | | | |
| 42.00 | 4.44 | 1.11 | 0.00 | | | | |
| 43.00 | 4.44 | 1.11 | 0.00 | | | | |
| 44.00 | 4.44 | 1.11 | 0.00 | | | | |
| 45.00 | 4.44 | 1.11 | 0.00 | | | | |
| 46.00 | 4.44 | 1.11 | 0.00 | | | | |
| 47.00 | 4.44 | 1.11 | 0.00 | | | | |
| 48.00 | 4.44 | 1.11 | 0.00 | | | | |
| 49.00 | 4.44 | 1.11 | 0.00 | | | | |
| 50.00 | 4.44 | 1.11 | 0.00 | | | | |

Summary for Reach R2: Post Developed

Inflow Area = 1.019 ac, 64.07% Impervious, Inflow Depth > 2.92" for 10-Year event
Inflow = 0.90 cfs @ 12.37 hrs, Volume= 0.248 af
Outflow = 0.90 cfs @ 12.37 hrs, Volume= 0.248 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R2: Post Developed

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Hydrograph for Reach R2: Post Developed

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.02 | 0.02 | |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.01 | 0.01 | |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.01 | 0.01 | |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.01 | 0.01 | |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.01 | 0.01 | |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.01 | 0.01 | |
| 6.00 | 0.00 | 0.00 | 0.00 | 57.00 | 0.01 | 0.01 | |
| 7.00 | 0.00 | 0.00 | 0.00 | 58.00 | 0.01 | 0.01 | |
| 8.00 | 0.01 | 0.01 | | 59.00 | 0.00 | 0.00 | |
| 9.00 | 0.01 | 0.01 | | 60.00 | 0.00 | 0.00 | |
| 10.00 | 0.02 | 0.02 | | 61.00 | 0.00 | 0.00 | |
| 11.00 | 0.02 | 0.02 | | 62.00 | 0.00 | 0.00 | |
| 12.00 | 0.17 | 0.17 | | 63.00 | 0.00 | 0.00 | |
| 13.00 | 0.54 | 0.54 | | 64.00 | 0.00 | 0.00 | |
| 14.00 | 0.19 | 0.19 | | 65.00 | 0.00 | 0.00 | |
| 15.00 | 0.15 | 0.15 | | 66.00 | 0.00 | 0.00 | |
| 16.00 | 0.10 | 0.10 | | 67.00 | 0.00 | 0.00 | |
| 17.00 | 0.08 | 0.08 | | 68.00 | 0.00 | 0.00 | |
| 18.00 | 0.08 | 0.08 | | 69.00 | 0.00 | 0.00 | |
| 19.00 | 0.07 | 0.07 | | 70.00 | 0.00 | 0.00 | |
| 20.00 | 0.07 | 0.07 | | 71.00 | 0.00 | 0.00 | |
| 21.00 | 0.07 | 0.07 | | 72.00 | 0.00 | 0.00 | |
| 22.00 | 0.06 | 0.06 | | | | | |
| 23.00 | 0.06 | 0.06 | | | | | |
| 24.00 | 0.06 | 0.06 | | | | | |
| 25.00 | 0.05 | 0.05 | | | | | |
| 26.00 | 0.05 | 0.05 | | | | | |
| 27.00 | 0.05 | 0.05 | | | | | |
| 28.00 | 0.05 | 0.05 | | | | | |
| 29.00 | 0.05 | 0.05 | | | | | |
| 30.00 | 0.05 | 0.05 | | | | | |
| 31.00 | 0.04 | 0.04 | | | | | |
| 32.00 | 0.04 | 0.04 | | | | | |
| 33.00 | 0.04 | 0.04 | | | | | |
| 34.00 | 0.04 | 0.04 | | | | | |
| 35.00 | 0.04 | 0.04 | | | | | |
| 36.00 | 0.04 | 0.04 | | | | | |
| 37.00 | 0.04 | 0.04 | | | | | |
| 38.00 | 0.03 | 0.03 | | | | | |
| 39.00 | 0.03 | 0.03 | | | | | |
| 40.00 | 0.03 | 0.03 | | | | | |
| 41.00 | 0.03 | 0.03 | | | | | |
| 42.00 | 0.03 | 0.03 | | | | | |
| 43.00 | 0.03 | 0.03 | | | | | |
| 44.00 | 0.03 | 0.03 | | | | | |
| 45.00 | 0.02 | 0.02 | | | | | |
| 46.00 | 0.02 | 0.02 | | | | | |
| 47.00 | 0.02 | 0.02 | | | | | |
| 48.00 | 0.02 | 0.02 | | | | | |
| 49.00 | 0.02 | 0.02 | | | | | |
| 50.00 | 0.02 | 0.02 | | | | | |

Summary for Pond 1P: Oversized Pipe

Inflow Area = 0.762 ac, 83.46% Impervious, Inflow Depth = 3.54" for 10-Year event
 Inflow = 4.07 cfs @ 12.13 hrs, Volume= 0.225 af
 Outflow = 0.78 cfs @ 12.44 hrs, Volume= 0.224 af, Atten= 81%, Lag= 18.3 min
 Primary = 0.78 cfs @ 12.44 hrs, Volume= 0.224 af

Routed to Reach R2 : Post Developed

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Starting Elev= 784.00' Surf.Area= 0.041 ac Storage= 0.111 af

Peak Elev= 787.36' @ 12.44 hrs Surf.Area= 0.023 ac Storage= 0.233 af (0.122 af above start)

Plug-Flow detention time= 1,324.2 min calculated for 0.113 af (50% of inflow)
 Center-of-Mass det. time= 639.9 min (1,419.8 - 779.9)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 780.50' | 0.243 af | 90.0" Round Pipe Storage L= 240.0' |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 784.00' | 18.0" Round Culvert L= 19.0' RCP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 784.00' / 783.75' S= 0.0132 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 1.77 sf |
| #2 | Device 1 | 784.00' | 1.2" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #3 | Device 1 | 786.55' | 6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 787.35' | 4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s) |

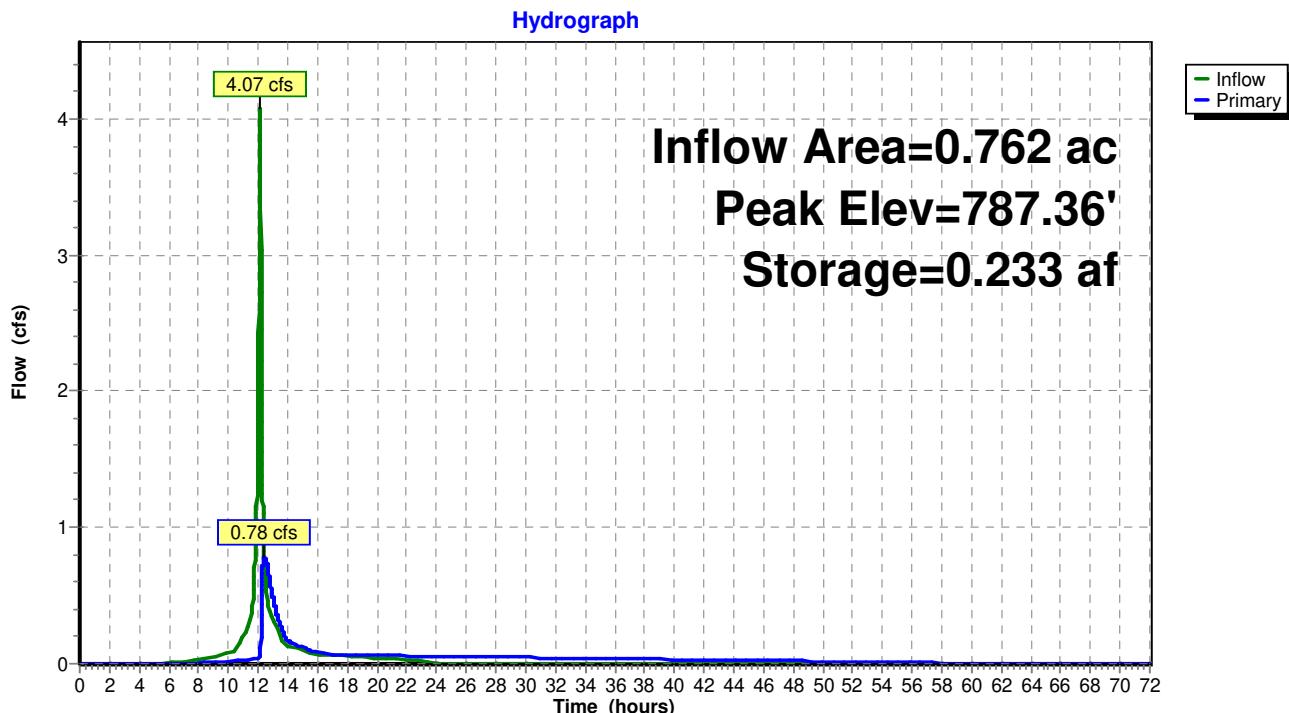
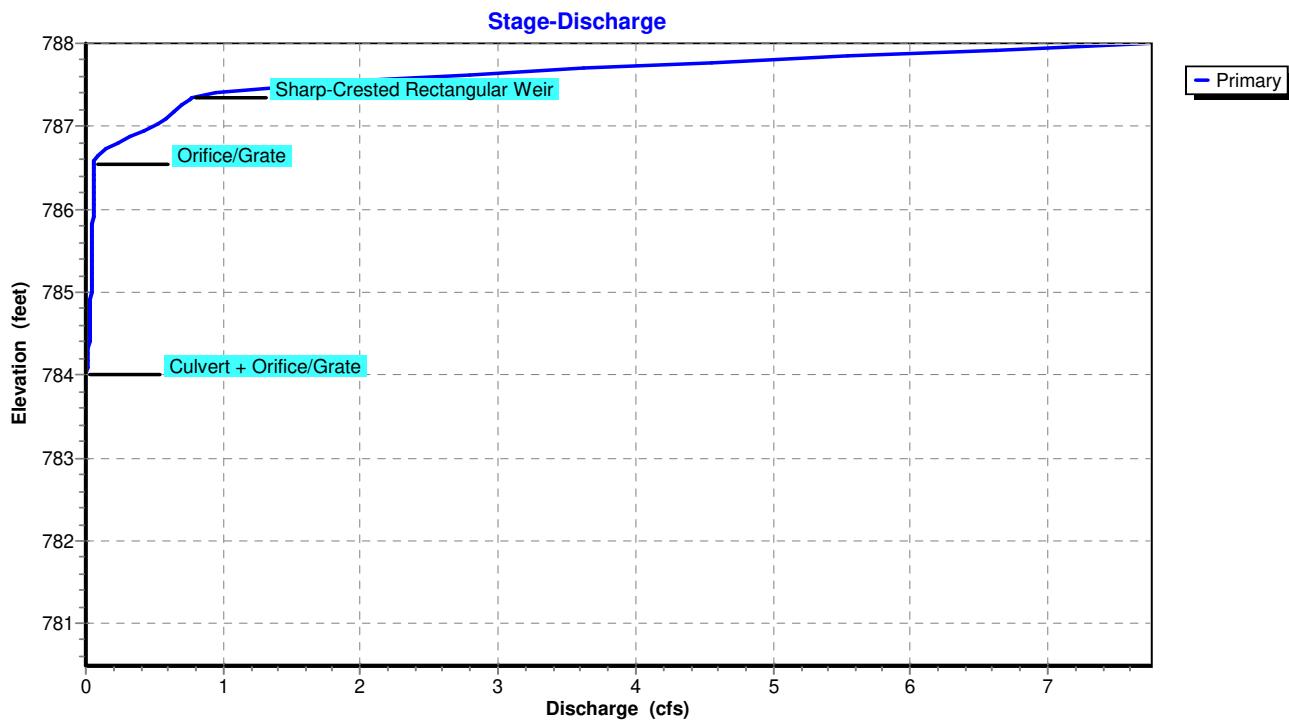
Primary OutFlow Max=0.78 cfs @ 12.44 hrs HW=787.36' TW=0.00' (Dynamic Tailwater)

↑1=Culvert (Passes 0.78 cfs of 12.12 cfs potential flow)

 ↑2=Orifice/Grate (Orifice Controls 0.07 cfs @ 8.76 fps)

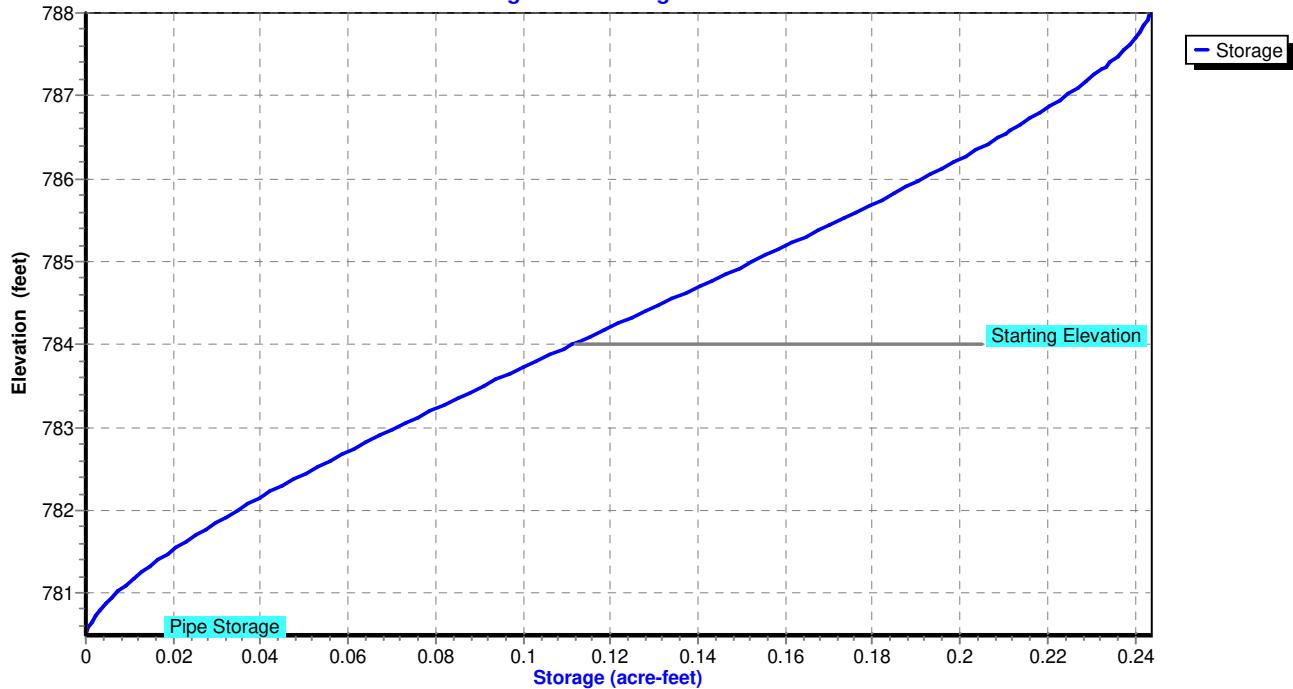
 ↑3=Orifice/Grate (Orifice Controls 0.71 cfs @ 3.59 fps)

 ↑4=Sharp-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.26 fps)

Pond 1P: Oversized Pipe**Pond 1P: Oversized Pipe**

Pond 1P: Oversized Pipe

Stage-Area-Storage



Hydrograph for Pond 1P: Oversized Pipe

| Time (hours) | Inflow (cfs) | Storage (acre-feet) | Elevation (feet) | Primary (cfs) |
|-----------------|-----------------|------------------------|---------------------|------------------|
| 0.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 2.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 4.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 6.00 | 0.01 | 0.112 | 784.01 | 0.00 |
| 8.00 | 0.03 | 0.115 | 784.08 | 0.01 |
| 10.00 | 0.08 | 0.121 | 784.24 | 0.02 |
| 12.00 | 2.02 | 0.171 | 785.45 | 0.04 |
| 14.00 | 0.13 | 0.217 | 786.75 | 0.17 |
| 16.00 | 0.07 | 0.213 | 786.64 | 0.08 |
| 18.00 | 0.06 | 0.212 | 786.59 | 0.06 |
| 20.00 | 0.04 | 0.210 | 786.52 | 0.06 |
| 22.00 | 0.03 | 0.206 | 786.40 | 0.06 |
| 24.00 | 0.01 | 0.200 | 786.23 | 0.06 |
| 26.00 | 0.00 | 0.191 | 785.98 | 0.05 |
| 28.00 | 0.00 | 0.182 | 785.76 | 0.05 |
| 30.00 | 0.00 | 0.174 | 785.55 | 0.05 |
| 32.00 | 0.00 | 0.167 | 785.36 | 0.04 |
| 34.00 | 0.00 | 0.160 | 785.19 | 0.04 |
| 36.00 | 0.00 | 0.154 | 785.03 | 0.04 |
| 38.00 | 0.00 | 0.148 | 784.88 | 0.03 |
| 40.00 | 0.00 | 0.142 | 784.75 | 0.03 |
| 42.00 | 0.00 | 0.137 | 784.63 | 0.03 |
| 44.00 | 0.00 | 0.133 | 784.52 | 0.03 |
| 46.00 | 0.00 | 0.129 | 784.42 | 0.02 |
| 48.00 | 0.00 | 0.125 | 784.33 | 0.02 |
| 50.00 | 0.00 | 0.122 | 784.26 | 0.02 |
| 52.00 | 0.00 | 0.119 | 784.19 | 0.01 |
| 54.00 | 0.00 | 0.117 | 784.14 | 0.01 |
| 56.00 | 0.00 | 0.116 | 784.10 | 0.01 |
| 58.00 | 0.00 | 0.114 | 784.07 | 0.01 |
| 60.00 | 0.00 | 0.114 | 784.06 | 0.00 |
| 62.00 | 0.00 | 0.113 | 784.04 | 0.00 |
| 64.00 | 0.00 | 0.113 | 784.04 | 0.00 |
| 66.00 | 0.00 | 0.113 | 784.03 | 0.00 |
| 68.00 | 0.00 | 0.112 | 784.03 | 0.00 |
| 70.00 | 0.00 | 0.112 | 784.02 | 0.00 |
| 72.00 | 0.00 | 0.112 | 784.02 | 0.00 |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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MSE 24-hr 4 10-Year Rainfall=4.44"
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Stage-Discharge for Pond 1P: Oversized Pipe

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 780.50 | 0.00 | 783.05 | 0.00 | 785.60 | 0.05 |
| 780.55 | 0.00 | 783.10 | 0.00 | 785.65 | 0.05 |
| 780.60 | 0.00 | 783.15 | 0.00 | 785.70 | 0.05 |
| 780.65 | 0.00 | 783.20 | 0.00 | 785.75 | 0.05 |
| 780.70 | 0.00 | 783.25 | 0.00 | 785.80 | 0.05 |
| 780.75 | 0.00 | 783.30 | 0.00 | 785.85 | 0.05 |
| 780.80 | 0.00 | 783.35 | 0.00 | 785.90 | 0.05 |
| 780.85 | 0.00 | 783.40 | 0.00 | 785.95 | 0.05 |
| 780.90 | 0.00 | 783.45 | 0.00 | 786.00 | 0.05 |
| 780.95 | 0.00 | 783.50 | 0.00 | 786.05 | 0.05 |
| 781.00 | 0.00 | 783.55 | 0.00 | 786.10 | 0.05 |
| 781.05 | 0.00 | 783.60 | 0.00 | 786.15 | 0.05 |
| 781.10 | 0.00 | 783.65 | 0.00 | 786.20 | 0.06 |
| 781.15 | 0.00 | 783.70 | 0.00 | 786.25 | 0.06 |
| 781.20 | 0.00 | 783.75 | 0.00 | 786.30 | 0.06 |
| 781.25 | 0.00 | 783.80 | 0.00 | 786.35 | 0.06 |
| 781.30 | 0.00 | 783.85 | 0.00 | 786.40 | 0.06 |
| 781.35 | 0.00 | 783.90 | 0.00 | 786.45 | 0.06 |
| 781.40 | 0.00 | 783.95 | 0.00 | 786.50 | 0.06 |
| 781.45 | 0.00 | 784.00 | 0.00 | 786.55 | 0.06 |
| 781.50 | 0.00 | 784.05 | 0.00 | 786.60 | 0.07 |
| 781.55 | 0.00 | 784.10 | 0.01 | 786.65 | 0.09 |
| 781.60 | 0.00 | 784.15 | 0.01 | 786.70 | 0.13 |
| 781.65 | 0.00 | 784.20 | 0.01 | 786.75 | 0.17 |
| 781.70 | 0.00 | 784.25 | 0.02 | 786.80 | 0.23 |
| 781.75 | 0.00 | 784.30 | 0.02 | 786.85 | 0.29 |
| 781.80 | 0.00 | 784.35 | 0.02 | 786.90 | 0.36 |
| 781.85 | 0.00 | 784.40 | 0.02 | 786.95 | 0.43 |
| 781.90 | 0.00 | 784.45 | 0.02 | 787.00 | 0.49 |
| 781.95 | 0.00 | 784.50 | 0.03 | 787.05 | 0.54 |
| 782.00 | 0.00 | 784.55 | 0.03 | 787.10 | 0.58 |
| 782.05 | 0.00 | 784.60 | 0.03 | 787.15 | 0.63 |
| 782.10 | 0.00 | 784.65 | 0.03 | 787.20 | 0.67 |
| 782.15 | 0.00 | 784.70 | 0.03 | 787.25 | 0.70 |
| 782.20 | 0.00 | 784.75 | 0.03 | 787.30 | 0.74 |
| 782.25 | 0.00 | 784.80 | 0.03 | 787.35 | 0.77 |
| 782.30 | 0.00 | 784.85 | 0.03 | 787.40 | 0.95 |
| 782.35 | 0.00 | 784.90 | 0.03 | 787.45 | 1.24 |
| 782.40 | 0.00 | 784.95 | 0.04 | 787.50 | 1.62 |
| 782.45 | 0.00 | 785.00 | 0.04 | 787.55 | 2.05 |
| 782.50 | 0.00 | 785.05 | 0.04 | 787.60 | 2.53 |
| 782.55 | 0.00 | 785.10 | 0.04 | 787.65 | 3.06 |
| 782.60 | 0.00 | 785.15 | 0.04 | 787.70 | 3.63 |
| 782.65 | 0.00 | 785.20 | 0.04 | 787.75 | 4.24 |
| 782.70 | 0.00 | 785.25 | 0.04 | 787.80 | 4.88 |
| 782.75 | 0.00 | 785.30 | 0.04 | 787.85 | 5.55 |
| 782.80 | 0.00 | 785.35 | 0.04 | 787.90 | 6.25 |
| 782.85 | 0.00 | 785.40 | 0.04 | 787.95 | 6.99 |
| 782.90 | 0.00 | 785.45 | 0.04 | 788.00 | 7.74 |
| 782.95 | 0.00 | 785.50 | 0.05 | | |
| 783.00 | 0.00 | 785.55 | 0.05 | | |

Retreat Center - Copy3

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Stage-Area-Storage for Pond 1P: Oversized Pipe

| Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) |
|---------------------|------------------------|---------------------|------------------------|---------------------|------------------------|
| 780.50 | 0.000 | 783.05 | 0.073 | 785.60 | 0.176 |
| 780.55 | 0.000 | 783.10 | 0.075 | 785.65 | 0.178 |
| 780.60 | 0.001 | 783.15 | 0.077 | 785.70 | 0.180 |
| 780.65 | 0.001 | 783.20 | 0.079 | 785.75 | 0.182 |
| 780.70 | 0.002 | 783.25 | 0.081 | 785.80 | 0.184 |
| 780.75 | 0.002 | 783.30 | 0.083 | 785.85 | 0.186 |
| 780.80 | 0.003 | 783.35 | 0.085 | 785.90 | 0.188 |
| 780.85 | 0.004 | 783.40 | 0.087 | 785.95 | 0.189 |
| 780.90 | 0.005 | 783.45 | 0.089 | 786.00 | 0.191 |
| 780.95 | 0.006 | 783.50 | 0.091 | 786.05 | 0.193 |
| 781.00 | 0.007 | 783.55 | 0.093 | 786.10 | 0.195 |
| 781.05 | 0.008 | 783.60 | 0.095 | 786.15 | 0.197 |
| 781.10 | 0.009 | 783.65 | 0.097 | 786.20 | 0.198 |
| 781.15 | 0.010 | 783.70 | 0.099 | 786.25 | 0.200 |
| 781.20 | 0.011 | 783.75 | 0.101 | 786.30 | 0.202 |
| 781.25 | 0.013 | 783.80 | 0.103 | 786.35 | 0.204 |
| 781.30 | 0.014 | 783.85 | 0.105 | 786.40 | 0.205 |
| 781.35 | 0.015 | 783.90 | 0.107 | 786.45 | 0.207 |
| 781.40 | 0.017 | 783.95 | 0.109 | 786.50 | 0.209 |
| 781.45 | 0.018 | 784.00 | 0.111 | 786.55 | 0.210 |
| 781.50 | 0.019 | 784.05 | 0.113 | 786.60 | 0.212 |
| 781.55 | 0.021 | 784.10 | 0.116 | 786.65 | 0.214 |
| 781.60 | 0.022 | 784.15 | 0.118 | 786.70 | 0.215 |
| 781.65 | 0.024 | 784.20 | 0.120 | 786.75 | 0.217 |
| 781.70 | 0.025 | 784.25 | 0.122 | 786.80 | 0.218 |
| 781.75 | 0.027 | 784.30 | 0.124 | 786.85 | 0.220 |
| 781.80 | 0.028 | 784.35 | 0.126 | 786.90 | 0.221 |
| 781.85 | 0.030 | 784.40 | 0.128 | 786.95 | 0.223 |
| 781.90 | 0.031 | 784.45 | 0.130 | 787.00 | 0.224 |
| 781.95 | 0.033 | 784.50 | 0.132 | 787.05 | 0.226 |
| 782.00 | 0.035 | 784.55 | 0.134 | 787.10 | 0.227 |
| 782.05 | 0.036 | 784.60 | 0.136 | 787.15 | 0.228 |
| 782.10 | 0.038 | 784.65 | 0.138 | 787.20 | 0.229 |
| 782.15 | 0.040 | 784.70 | 0.140 | 787.25 | 0.231 |
| 782.20 | 0.041 | 784.75 | 0.142 | 787.30 | 0.232 |
| 782.25 | 0.043 | 784.80 | 0.144 | 787.35 | 0.233 |
| 782.30 | 0.045 | 784.85 | 0.146 | 787.40 | 0.234 |
| 782.35 | 0.047 | 784.90 | 0.148 | 787.45 | 0.235 |
| 782.40 | 0.048 | 784.95 | 0.150 | 787.50 | 0.236 |
| 782.45 | 0.050 | 785.00 | 0.152 | 787.55 | 0.237 |
| 782.50 | 0.052 | 785.05 | 0.155 | 787.60 | 0.238 |
| 782.55 | 0.054 | 785.10 | 0.157 | 787.65 | 0.239 |
| 782.60 | 0.056 | 785.15 | 0.159 | 787.70 | 0.240 |
| 782.65 | 0.058 | 785.20 | 0.161 | 787.75 | 0.241 |
| 782.70 | 0.060 | 785.25 | 0.163 | 787.80 | 0.242 |
| 782.75 | 0.061 | 785.30 | 0.165 | 787.85 | 0.242 |
| 782.80 | 0.063 | 785.35 | 0.166 | 787.90 | 0.243 |
| 782.85 | 0.065 | 785.40 | 0.168 | 787.95 | 0.243 |
| 782.90 | 0.067 | 785.45 | 0.170 | 788.00 | 0.243 |
| 782.95 | 0.069 | 785.50 | 0.172 | | |
| 783.00 | 0.071 | 785.55 | 0.174 | | |

Retreat Center - Copy3

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MSE 24-hr 4 100-Year Rainfall=7.60"
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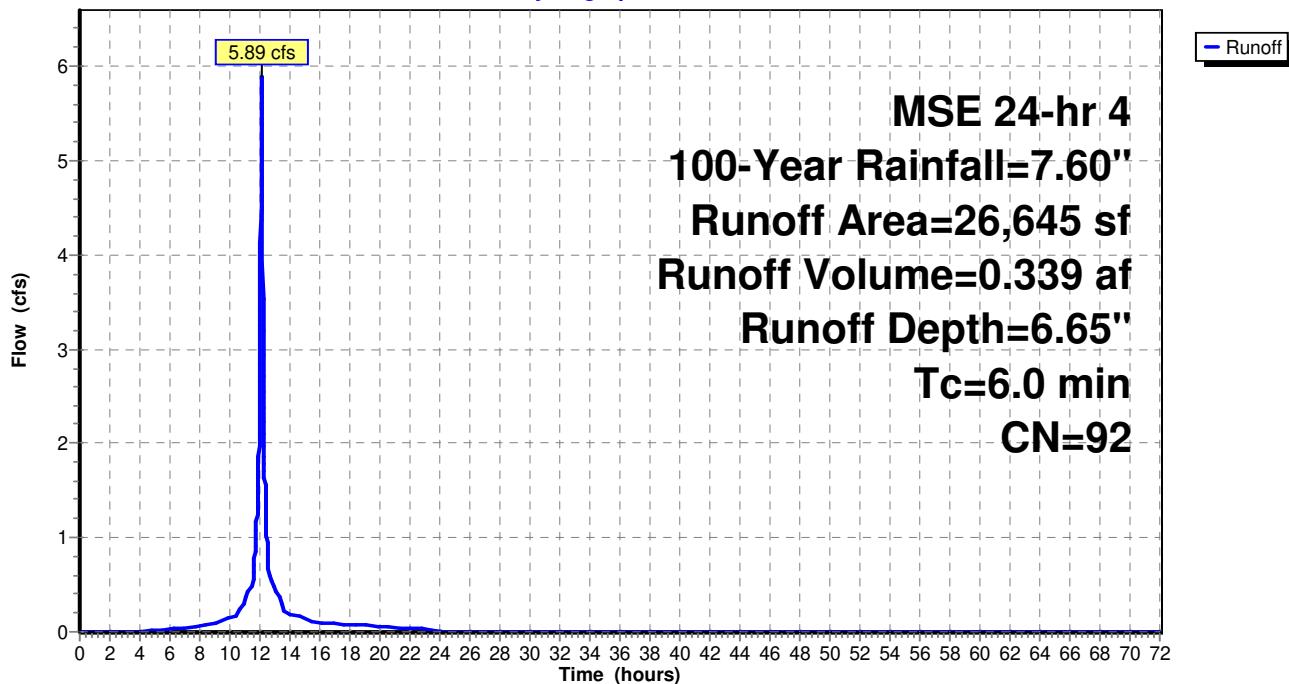
Summary for Subcatchment A1: Project Detained

Runoff = 5.89 cfs @ 12.13 hrs, Volume= 0.339 af, Depth= 6.65"
Routed to Pond 1P : Oversized Pipe

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 100-Year Rainfall=7.60"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| 13,722 | 98 | Paved parking, HSG B |
| * | | |
| 8,443 | 98 | Roof |
| 4,480 | 61 | >75% Grass cover, Good, HSG B |
| 26,645 | 92 | Weighted Average |
| 4,480 | | 16.81% Pervious Area |
| 22,165 | | 83.19% Impervious Area |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A1: Project Detained**Hydrograph**

Retreat Center - Copy3

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MSE 24-hr 4 100-Year Rainfall=7.60"
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Hydrograph for Subcatchment A1: Project Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 7.60 | 6.65 | 0.00 |
| 1.00 | 0.04 | 0.00 | 0.00 | 52.00 | 7.60 | 6.65 | 0.00 |
| 2.00 | 0.09 | 0.00 | 0.00 | 53.00 | 7.60 | 6.65 | 0.00 |
| 3.00 | 0.16 | 0.00 | 0.00 | 54.00 | 7.60 | 6.65 | 0.00 |
| 4.00 | 0.25 | 0.01 | 0.01 | 55.00 | 7.60 | 6.65 | 0.00 |
| 5.00 | 0.35 | 0.03 | 0.02 | 56.00 | 7.60 | 6.65 | 0.00 |
| 6.00 | 0.47 | 0.07 | 0.03 | 57.00 | 7.60 | 6.65 | 0.00 |
| 7.00 | 0.60 | 0.14 | 0.05 | 58.00 | 7.60 | 6.65 | 0.00 |
| 8.00 | 0.75 | 0.23 | 0.06 | 59.00 | 7.60 | 6.65 | 0.00 |
| 9.00 | 0.92 | 0.34 | 0.08 | 60.00 | 7.60 | 6.65 | 0.00 |
| 10.00 | 1.20 | 0.56 | 0.14 | 61.00 | 7.60 | 6.65 | 0.00 |
| 11.00 | 1.64 | 0.92 | 0.35 | 62.00 | 7.60 | 6.65 | 0.00 |
| 12.00 | 3.56 | 2.70 | 3.00 | 63.00 | 7.60 | 6.65 | 0.00 |
| 13.00 | 5.96 | 5.03 | 0.46 | 64.00 | 7.60 | 6.65 | 0.00 |
| 14.00 | 6.40 | 5.46 | 0.19 | 65.00 | 7.60 | 6.65 | 0.00 |
| 15.00 | 6.68 | 5.74 | 0.16 | 66.00 | 7.60 | 6.65 | 0.00 |
| 16.00 | 6.85 | 5.90 | 0.10 | 67.00 | 7.60 | 6.65 | 0.00 |
| 17.00 | 7.00 | 6.05 | 0.09 | 68.00 | 7.60 | 6.65 | 0.00 |
| 18.00 | 7.13 | 6.19 | 0.08 | 69.00 | 7.60 | 6.65 | 0.00 |
| 19.00 | 7.25 | 6.30 | 0.07 | 70.00 | 7.60 | 6.65 | 0.00 |
| 20.00 | 7.35 | 6.40 | 0.06 | 71.00 | 7.60 | 6.65 | 0.00 |
| 21.00 | 7.44 | 6.49 | 0.05 | 72.00 | 7.60 | 6.65 | 0.00 |
| 22.00 | 7.51 | 6.56 | 0.04 | | | | |
| 23.00 | 7.56 | 6.61 | 0.03 | | | | |
| 24.00 | 7.60 | 6.65 | 0.02 | | | | |
| 25.00 | 7.60 | 6.65 | 0.00 | | | | |
| 26.00 | 7.60 | 6.65 | 0.00 | | | | |
| 27.00 | 7.60 | 6.65 | 0.00 | | | | |
| 28.00 | 7.60 | 6.65 | 0.00 | | | | |
| 29.00 | 7.60 | 6.65 | 0.00 | | | | |
| 30.00 | 7.60 | 6.65 | 0.00 | | | | |
| 31.00 | 7.60 | 6.65 | 0.00 | | | | |
| 32.00 | 7.60 | 6.65 | 0.00 | | | | |
| 33.00 | 7.60 | 6.65 | 0.00 | | | | |
| 34.00 | 7.60 | 6.65 | 0.00 | | | | |
| 35.00 | 7.60 | 6.65 | 0.00 | | | | |
| 36.00 | 7.60 | 6.65 | 0.00 | | | | |
| 37.00 | 7.60 | 6.65 | 0.00 | | | | |
| 38.00 | 7.60 | 6.65 | 0.00 | | | | |
| 39.00 | 7.60 | 6.65 | 0.00 | | | | |
| 40.00 | 7.60 | 6.65 | 0.00 | | | | |
| 41.00 | 7.60 | 6.65 | 0.00 | | | | |
| 42.00 | 7.60 | 6.65 | 0.00 | | | | |
| 43.00 | 7.60 | 6.65 | 0.00 | | | | |
| 44.00 | 7.60 | 6.65 | 0.00 | | | | |
| 45.00 | 7.60 | 6.65 | 0.00 | | | | |
| 46.00 | 7.60 | 6.65 | 0.00 | | | | |
| 47.00 | 7.60 | 6.65 | 0.00 | | | | |
| 48.00 | 7.60 | 6.65 | 0.00 | | | | |
| 49.00 | 7.60 | 6.65 | 0.00 | | | | |
| 50.00 | 7.60 | 6.65 | 0.00 | | | | |

Summary for Subcatchment A2: Runon Detained

Runoff = 1.45 cfs @ 12.13 hrs, Volume= 0.083 af, Depth= 6.65"
Routed to Pond 1P : Oversized Pipe

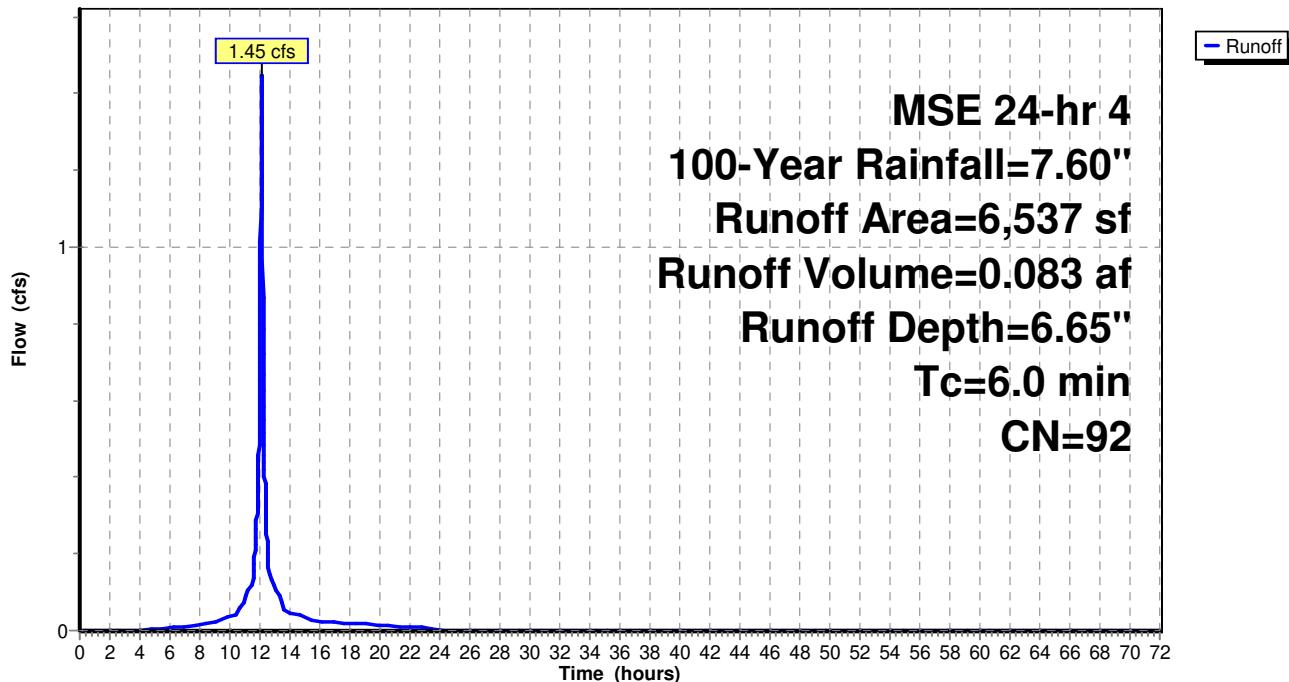
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 100-Year Rainfall=7.60"

| Area (sf) | CN | Description |
|-----------|----|-------------------------------|
| * 5,529 | 98 | Roof |
| 1,008 | 61 | >75% Grass cover, Good, HSG B |
| 6,537 | 92 | Weighted Average |
| 1,008 | | 15.42% Pervious Area |
| 5,529 | | 84.58% Impervious Area |

| Tc | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-----|------------------|------------------|----------------------|-------------------|-------------|
| 6.0 | Direct Entry, | | | | |

Subcatchment A2: Runon Detained

Hydrograph



Hydrograph for Subcatchment A2: Runon Detained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 7.60 | 6.65 | 0.00 |
| 1.00 | 0.04 | 0.00 | 0.00 | 52.00 | 7.60 | 6.65 | 0.00 |
| 2.00 | 0.09 | 0.00 | 0.00 | 53.00 | 7.60 | 6.65 | 0.00 |
| 3.00 | 0.16 | 0.00 | 0.00 | 54.00 | 7.60 | 6.65 | 0.00 |
| 4.00 | 0.25 | 0.01 | 0.00 | 55.00 | 7.60 | 6.65 | 0.00 |
| 5.00 | 0.35 | 0.03 | 0.00 | 56.00 | 7.60 | 6.65 | 0.00 |
| 6.00 | 0.47 | 0.07 | 0.01 | 57.00 | 7.60 | 6.65 | 0.00 |
| 7.00 | 0.60 | 0.14 | 0.01 | 58.00 | 7.60 | 6.65 | 0.00 |
| 8.00 | 0.75 | 0.23 | 0.02 | 59.00 | 7.60 | 6.65 | 0.00 |
| 9.00 | 0.92 | 0.34 | 0.02 | 60.00 | 7.60 | 6.65 | 0.00 |
| 10.00 | 1.20 | 0.56 | 0.04 | 61.00 | 7.60 | 6.65 | 0.00 |
| 11.00 | 1.64 | 0.92 | 0.08 | 62.00 | 7.60 | 6.65 | 0.00 |
| 12.00 | 3.56 | 2.70 | 0.74 | 63.00 | 7.60 | 6.65 | 0.00 |
| 13.00 | 5.96 | 5.03 | 0.11 | 64.00 | 7.60 | 6.65 | 0.00 |
| 14.00 | 6.40 | 5.46 | 0.05 | 65.00 | 7.60 | 6.65 | 0.00 |
| 15.00 | 6.68 | 5.74 | 0.04 | 66.00 | 7.60 | 6.65 | 0.00 |
| 16.00 | 6.85 | 5.90 | 0.02 | 67.00 | 7.60 | 6.65 | 0.00 |
| 17.00 | 7.00 | 6.05 | 0.02 | 68.00 | 7.60 | 6.65 | 0.00 |
| 18.00 | 7.13 | 6.19 | 0.02 | 69.00 | 7.60 | 6.65 | 0.00 |
| 19.00 | 7.25 | 6.30 | 0.02 | 70.00 | 7.60 | 6.65 | 0.00 |
| 20.00 | 7.35 | 6.40 | 0.01 | 71.00 | 7.60 | 6.65 | 0.00 |
| 21.00 | 7.44 | 6.49 | 0.01 | 72.00 | 7.60 | 6.65 | 0.00 |
| 22.00 | 7.51 | 6.56 | 0.01 | | | | |
| 23.00 | 7.56 | 6.61 | 0.01 | | | | |
| 24.00 | 7.60 | 6.65 | 0.00 | | | | |
| 25.00 | 7.60 | 6.65 | 0.00 | | | | |
| 26.00 | 7.60 | 6.65 | 0.00 | | | | |
| 27.00 | 7.60 | 6.65 | 0.00 | | | | |
| 28.00 | 7.60 | 6.65 | 0.00 | | | | |
| 29.00 | 7.60 | 6.65 | 0.00 | | | | |
| 30.00 | 7.60 | 6.65 | 0.00 | | | | |
| 31.00 | 7.60 | 6.65 | 0.00 | | | | |
| 32.00 | 7.60 | 6.65 | 0.00 | | | | |
| 33.00 | 7.60 | 6.65 | 0.00 | | | | |
| 34.00 | 7.60 | 6.65 | 0.00 | | | | |
| 35.00 | 7.60 | 6.65 | 0.00 | | | | |
| 36.00 | 7.60 | 6.65 | 0.00 | | | | |
| 37.00 | 7.60 | 6.65 | 0.00 | | | | |
| 38.00 | 7.60 | 6.65 | 0.00 | | | | |
| 39.00 | 7.60 | 6.65 | 0.00 | | | | |
| 40.00 | 7.60 | 6.65 | 0.00 | | | | |
| 41.00 | 7.60 | 6.65 | 0.00 | | | | |
| 42.00 | 7.60 | 6.65 | 0.00 | | | | |
| 43.00 | 7.60 | 6.65 | 0.00 | | | | |
| 44.00 | 7.60 | 6.65 | 0.00 | | | | |
| 45.00 | 7.60 | 6.65 | 0.00 | | | | |
| 46.00 | 7.60 | 6.65 | 0.00 | | | | |
| 47.00 | 7.60 | 6.65 | 0.00 | | | | |
| 48.00 | 7.60 | 6.65 | 0.00 | | | | |
| 49.00 | 7.60 | 6.65 | 0.00 | | | | |
| 50.00 | 7.60 | 6.65 | 0.00 | | | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Proposed Conditions

MSE 24-hr 4 100-Year Rainfall=7.60"

Printed 9/16/2024

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Summary for Subcatchment A3: Project Undetained

Runoff = 1.36 cfs @ 12.14 hrs, Volume= 0.070 af, Depth= 3.25"
Routed to Reach R2 : Post Developed

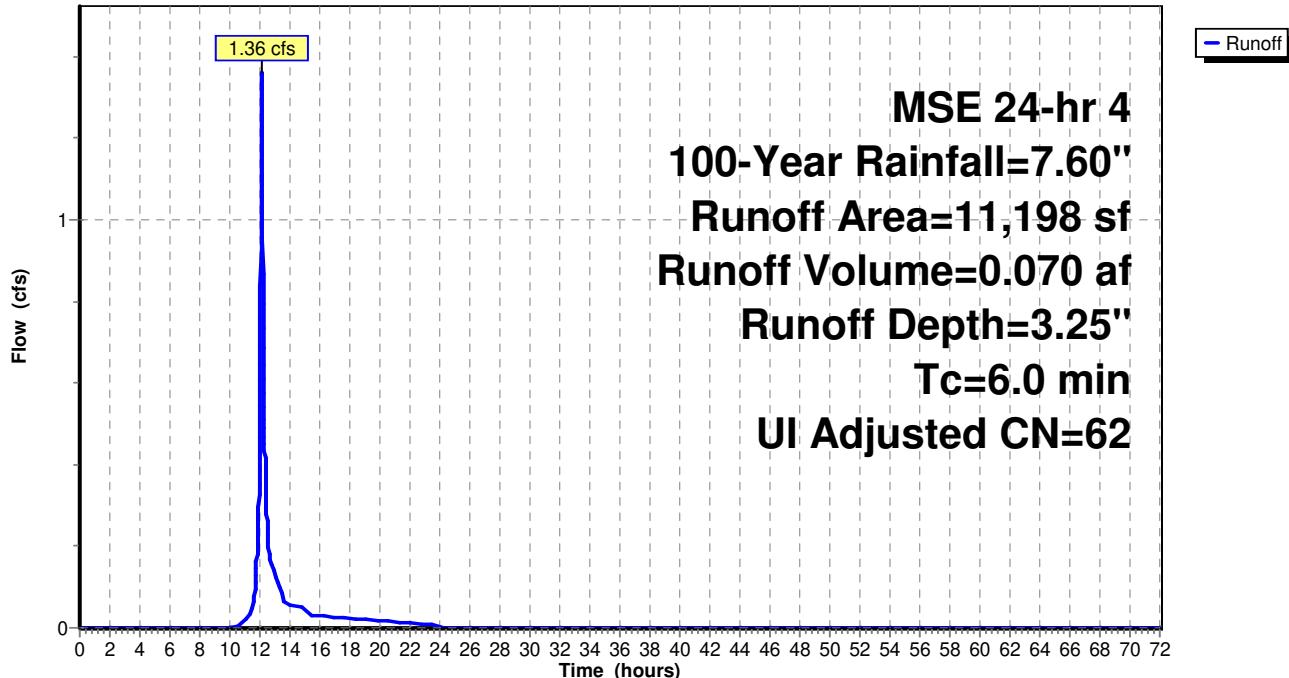
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
MSE 24-hr 4 100-Year Rainfall=7.60"

| Area (sf) | CN | Adj | Description |
|-----------|----|-----|-------------------------------|
| 739 | 98 | | Unconnected pavement, HSG B |
| 10,459 | 61 | | >75% Grass cover, Good, HSG B |
| 11,198 | 63 | 62 | Weighted Average, UI Adjusted |
| 10,459 | | | 93.40% Pervious Area |
| 739 | | | 6.60% Impervious Area |
| 739 | | | 100.00% Unconnected |

| Tc (min) | Length (feet) | Slope (ft/ft) | Velocity (ft/sec) | Capacity (cfs) | Description |
|-------------|------------------|------------------|----------------------|-------------------|---------------|
| 6.0 | | | | | Direct Entry, |

Subcatchment A3: Project Undetained

Hydrograph



Hydrograph for Subcatchment A3: Project Undetained

| Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) | Time (hours) | Precip. (inches) | Excess (inches) | Runoff (cfs) |
|-----------------|---------------------|--------------------|-----------------|-----------------|---------------------|--------------------|-----------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 7.60 | 3.25 | 0.00 |
| 1.00 | 0.04 | 0.00 | 0.00 | 52.00 | 7.60 | 3.25 | 0.00 |
| 2.00 | 0.09 | 0.00 | 0.00 | 53.00 | 7.60 | 3.25 | 0.00 |
| 3.00 | 0.16 | 0.00 | 0.00 | 54.00 | 7.60 | 3.25 | 0.00 |
| 4.00 | 0.25 | 0.00 | 0.00 | 55.00 | 7.60 | 3.25 | 0.00 |
| 5.00 | 0.35 | 0.00 | 0.00 | 56.00 | 7.60 | 3.25 | 0.00 |
| 6.00 | 0.47 | 0.00 | 0.00 | 57.00 | 7.60 | 3.25 | 0.00 |
| 7.00 | 0.60 | 0.00 | 0.00 | 58.00 | 7.60 | 3.25 | 0.00 |
| 8.00 | 0.75 | 0.00 | 0.00 | 59.00 | 7.60 | 3.25 | 0.00 |
| 9.00 | 0.92 | 0.00 | 0.00 | 60.00 | 7.60 | 3.25 | 0.00 |
| 10.00 | 1.20 | 0.00 | 0.00 | 61.00 | 7.60 | 3.25 | 0.00 |
| 11.00 | 1.64 | 0.03 | 0.02 | 62.00 | 7.60 | 3.25 | 0.00 |
| 12.00 | 3.56 | 0.64 | 0.54 | 63.00 | 7.60 | 3.25 | 0.00 |
| 13.00 | 5.96 | 2.06 | 0.13 | 64.00 | 7.60 | 3.25 | 0.00 |
| 14.00 | 6.40 | 2.37 | 0.06 | 65.00 | 7.60 | 3.25 | 0.00 |
| 15.00 | 6.68 | 2.57 | 0.05 | 66.00 | 7.60 | 3.25 | 0.00 |
| 16.00 | 6.85 | 2.69 | 0.03 | 67.00 | 7.60 | 3.25 | 0.00 |
| 17.00 | 7.00 | 2.80 | 0.03 | 68.00 | 7.60 | 3.25 | 0.00 |
| 18.00 | 7.13 | 2.90 | 0.02 | 69.00 | 7.60 | 3.25 | 0.00 |
| 19.00 | 7.25 | 2.99 | 0.02 | 70.00 | 7.60 | 3.25 | 0.00 |
| 20.00 | 7.35 | 3.06 | 0.02 | 71.00 | 7.60 | 3.25 | 0.00 |
| 21.00 | 7.44 | 3.13 | 0.02 | 72.00 | 7.60 | 3.25 | 0.00 |
| 22.00 | 7.51 | 3.18 | 0.01 | | | | |
| 23.00 | 7.56 | 3.22 | 0.01 | | | | |
| 24.00 | 7.60 | 3.25 | 0.01 | | | | |
| 25.00 | 7.60 | 3.25 | 0.00 | | | | |
| 26.00 | 7.60 | 3.25 | 0.00 | | | | |
| 27.00 | 7.60 | 3.25 | 0.00 | | | | |
| 28.00 | 7.60 | 3.25 | 0.00 | | | | |
| 29.00 | 7.60 | 3.25 | 0.00 | | | | |
| 30.00 | 7.60 | 3.25 | 0.00 | | | | |
| 31.00 | 7.60 | 3.25 | 0.00 | | | | |
| 32.00 | 7.60 | 3.25 | 0.00 | | | | |
| 33.00 | 7.60 | 3.25 | 0.00 | | | | |
| 34.00 | 7.60 | 3.25 | 0.00 | | | | |
| 35.00 | 7.60 | 3.25 | 0.00 | | | | |
| 36.00 | 7.60 | 3.25 | 0.00 | | | | |
| 37.00 | 7.60 | 3.25 | 0.00 | | | | |
| 38.00 | 7.60 | 3.25 | 0.00 | | | | |
| 39.00 | 7.60 | 3.25 | 0.00 | | | | |
| 40.00 | 7.60 | 3.25 | 0.00 | | | | |
| 41.00 | 7.60 | 3.25 | 0.00 | | | | |
| 42.00 | 7.60 | 3.25 | 0.00 | | | | |
| 43.00 | 7.60 | 3.25 | 0.00 | | | | |
| 44.00 | 7.60 | 3.25 | 0.00 | | | | |
| 45.00 | 7.60 | 3.25 | 0.00 | | | | |
| 46.00 | 7.60 | 3.25 | 0.00 | | | | |
| 47.00 | 7.60 | 3.25 | 0.00 | | | | |
| 48.00 | 7.60 | 3.25 | 0.00 | | | | |
| 49.00 | 7.60 | 3.25 | 0.00 | | | | |
| 50.00 | 7.60 | 3.25 | 0.00 | | | | |

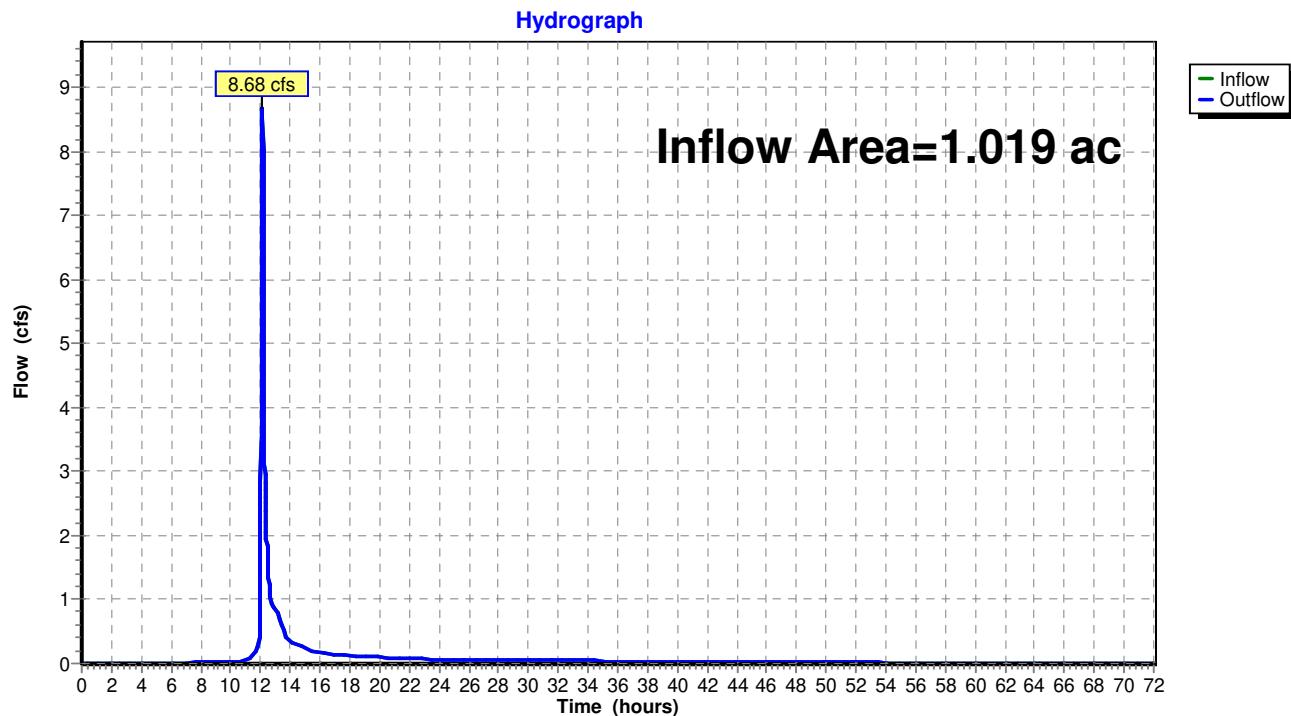
Summary for Reach R2: Post Developed

Inflow Area = 1.019 ac, 64.07% Impervious, Inflow Depth = 5.78" for 100-Year event

Inflow = 8.68 cfs @ 12.13 hrs, Volume= 0.491 af

Outflow = 8.68 cfs @ 12.13 hrs, Volume= 0.491 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Reach R2: Post Developed

Hydrograph for Reach R2: Post Developed

| Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) | Time (hours) | Inflow (cfs) | Elevation (feet) | Outflow (cfs) |
|-----------------|-----------------|---------------------|------------------|-----------------|-----------------|---------------------|------------------|
| 0.00 | 0.00 | 0.00 | 0.00 | 51.00 | 0.02 | 0.02 | 0.02 |
| 1.00 | 0.00 | 0.00 | 0.00 | 52.00 | 0.02 | 0.02 | 0.02 |
| 2.00 | 0.00 | 0.00 | 0.00 | 53.00 | 0.02 | 0.02 | 0.02 |
| 3.00 | 0.00 | 0.00 | 0.00 | 54.00 | 0.01 | 0.01 | 0.01 |
| 4.00 | 0.00 | 0.00 | 0.00 | 55.00 | 0.01 | 0.01 | 0.01 |
| 5.00 | 0.00 | 0.00 | 0.00 | 56.00 | 0.01 | 0.01 | 0.01 |
| 6.00 | 0.01 | 0.01 | 0.01 | 57.00 | 0.01 | 0.01 | 0.01 |
| 7.00 | 0.01 | 0.01 | 0.01 | 58.00 | 0.01 | 0.01 | 0.01 |
| 8.00 | 0.02 | 0.02 | 0.02 | 59.00 | 0.01 | 0.01 | 0.01 |
| 9.00 | 0.02 | 0.02 | 0.02 | 60.00 | 0.01 | 0.01 | 0.01 |
| 10.00 | 0.03 | 0.03 | 0.03 | 61.00 | 0.00 | 0.00 | 0.00 |
| 11.00 | 0.06 | 0.06 | 0.06 | 62.00 | 0.00 | 0.00 | 0.00 |
| 12.00 | 1.41 | 1.41 | 1.41 | 63.00 | 0.00 | 0.00 | 0.00 |
| 13.00 | 0.83 | 0.83 | 0.83 | 64.00 | 0.00 | 0.00 | 0.00 |
| 14.00 | 0.34 | 0.34 | 0.34 | 65.00 | 0.00 | 0.00 | 0.00 |
| 15.00 | 0.26 | 0.26 | 0.26 | 66.00 | 0.00 | 0.00 | 0.00 |
| 16.00 | 0.16 | 0.16 | 0.16 | 67.00 | 0.00 | 0.00 | 0.00 |
| 17.00 | 0.14 | 0.14 | 0.14 | 68.00 | 0.00 | 0.00 | 0.00 |
| 18.00 | 0.13 | 0.13 | 0.13 | 69.00 | 0.00 | 0.00 | 0.00 |
| 19.00 | 0.11 | 0.11 | 0.11 | 70.00 | 0.00 | 0.00 | 0.00 |
| 20.00 | 0.10 | 0.10 | 0.10 | 71.00 | 0.00 | 0.00 | 0.00 |
| 21.00 | 0.09 | 0.09 | 0.09 | 72.00 | 0.00 | 0.00 | 0.00 |
| 22.00 | 0.07 | 0.07 | | | | | |
| 23.00 | 0.07 | 0.07 | | | | | |
| 24.00 | 0.06 | 0.06 | | | | | |
| 25.00 | 0.06 | 0.06 | | | | | |
| 26.00 | 0.06 | 0.06 | | | | | |
| 27.00 | 0.05 | 0.05 | | | | | |
| 28.00 | 0.05 | 0.05 | | | | | |
| 29.00 | 0.05 | 0.05 | | | | | |
| 30.00 | 0.05 | 0.05 | | | | | |
| 31.00 | 0.05 | 0.05 | | | | | |
| 32.00 | 0.05 | 0.05 | | | | | |
| 33.00 | 0.04 | 0.04 | | | | | |
| 34.00 | 0.04 | 0.04 | | | | | |
| 35.00 | 0.04 | 0.04 | | | | | |
| 36.00 | 0.04 | 0.04 | | | | | |
| 37.00 | 0.04 | 0.04 | | | | | |
| 38.00 | 0.04 | 0.04 | | | | | |
| 39.00 | 0.04 | 0.04 | | | | | |
| 40.00 | 0.03 | 0.03 | | | | | |
| 41.00 | 0.03 | 0.03 | | | | | |
| 42.00 | 0.03 | 0.03 | | | | | |
| 43.00 | 0.03 | 0.03 | | | | | |
| 44.00 | 0.03 | 0.03 | | | | | |
| 45.00 | 0.03 | 0.03 | | | | | |
| 46.00 | 0.03 | 0.03 | | | | | |
| 47.00 | 0.02 | 0.02 | | | | | |
| 48.00 | 0.02 | 0.02 | | | | | |
| 49.00 | 0.02 | 0.02 | | | | | |
| 50.00 | 0.02 | 0.02 | | | | | |

Summary for Pond 1P: Oversized Pipe

Inflow Area = 0.762 ac, 83.46% Impervious, Inflow Depth = 6.65" for 100-Year event
Inflow = 7.34 cfs @ 12.13 hrs, Volume= 0.422 af
Outflow = 7.32 cfs @ 12.13 hrs, Volume= 0.421 af, Atten= 0%, Lag= 0.3 min
Primary = 7.32 cfs @ 12.13 hrs, Volume= 0.421 af

Routed to Reach R2 : Post Developed

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs
Starting Elev= 784.00' Surf.Area= 0.041 ac Storage= 0.111 af
Peak Elev= 787.97' @ 12.13 hrs Surf.Area= 0.005 ac Storage= 0.243 af (0.132 af above start)

Plug-Flow detention time= 617.2 min calculated for 0.310 af (73% of inflow)
Center-of-Mass det. time= 384.0 min (1,150.1 - 766.2)

| Volume | Invert | Avail.Storage | Storage Description |
|--------|---------|---------------|--|
| #1 | 780.50' | 0.243 af | 90.0" Round Pipe Storage L= 240.0' |

| Device | Routing | Invert | Outlet Devices |
|--------|----------|---------|---|
| #1 | Primary | 784.00' | 18.0" Round Culvert L= 19.0' RCP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 784.00' / 783.75' S= 0.0132 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 1.77 sf |
| #2 | Device 1 | 784.00' | 1.2" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #3 | Device 1 | 786.55' | 6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads |
| #4 | Device 1 | 787.35' | 4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s) |

Primary OutFlow Max=7.30 cfs @ 12.13 hrs HW=787.97' TW=0.00' (Dynamic Tailwater)

↑1=Culvert (Passes 7.30 cfs of 13.47 cfs potential flow)

 2=Orifice/Grate (Orifice Controls 0.07 cfs @ 9.53 fps)

 3=Orifice/Grate (Orifice Controls 1.02 cfs @ 5.21 fps)

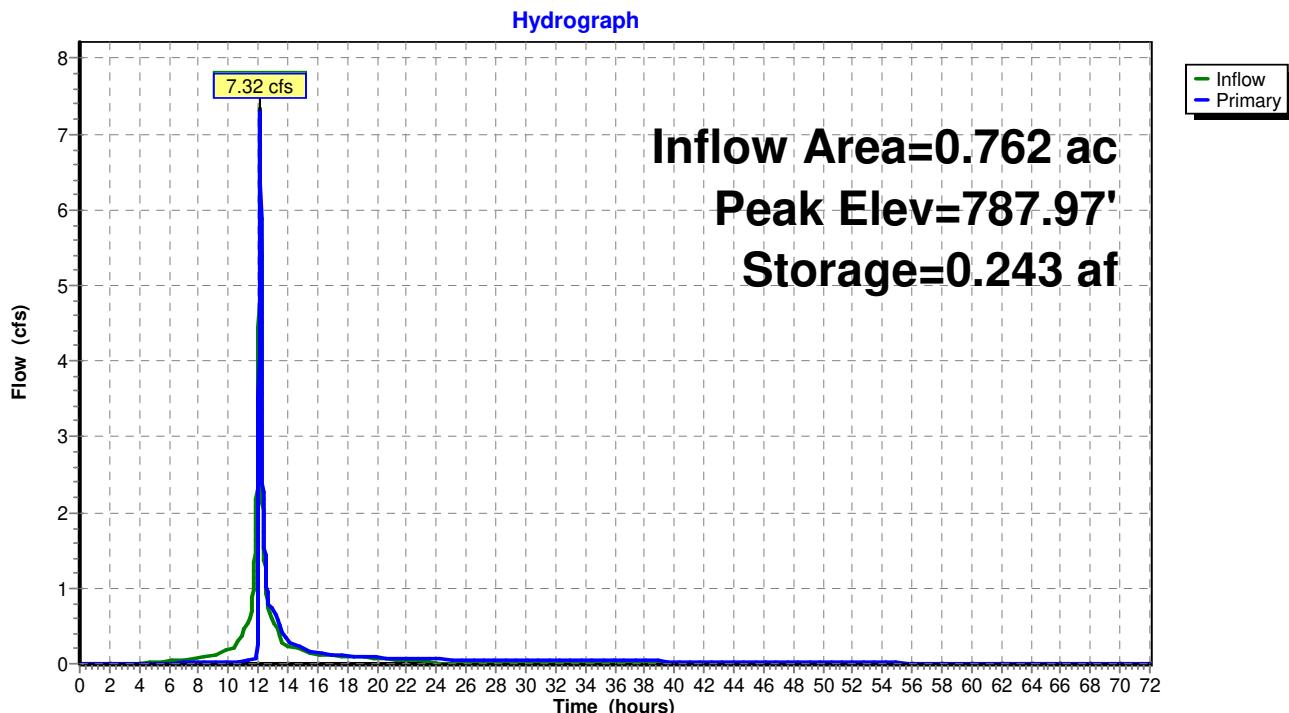
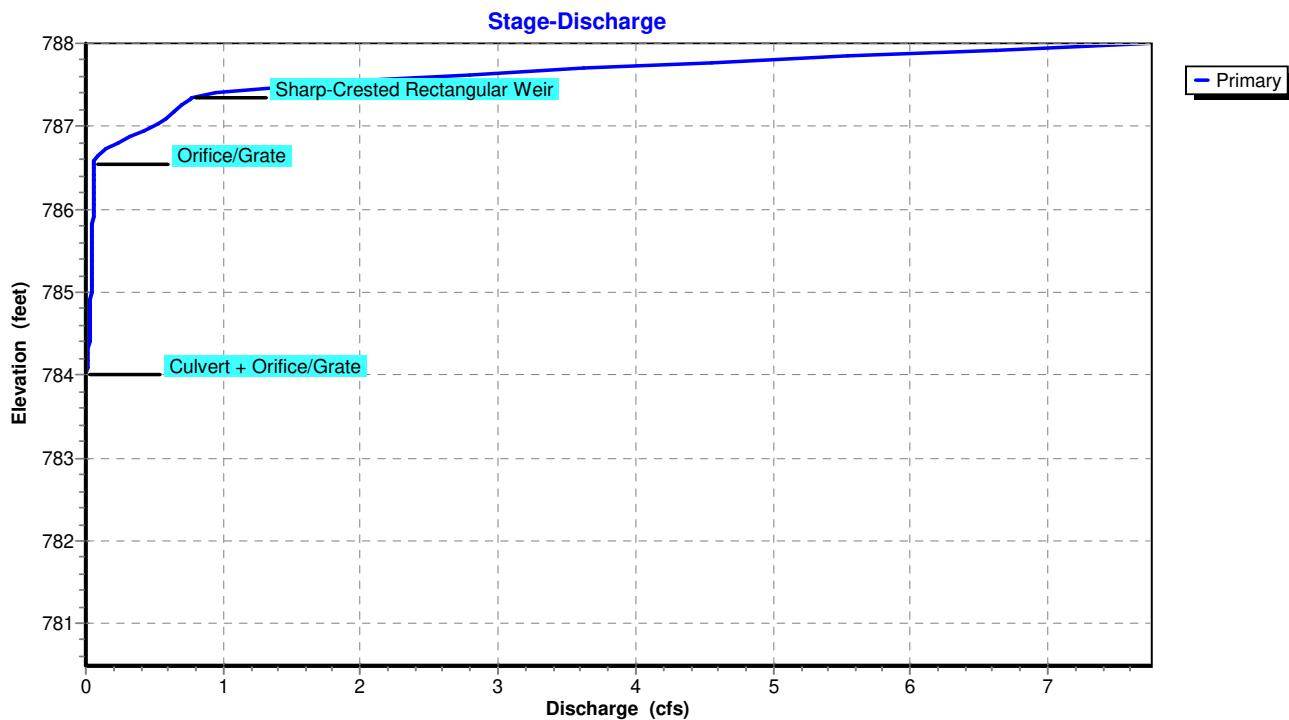
 4=Sharp-Crested Rectangular Weir (Weir Controls 6.20 cfs @ 2.58 fps)

Retreat Center - Copy3

Prepared by Vierbicher Associates

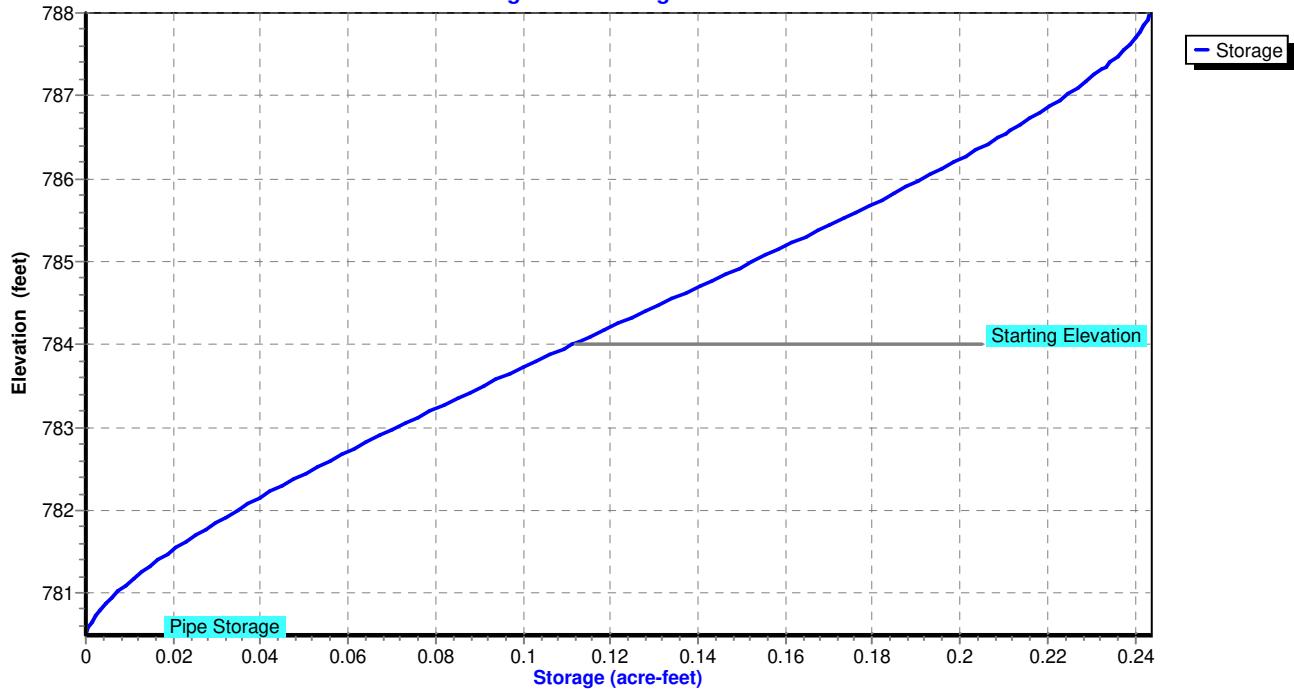
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Proposed Conditions
MSE 24-hr 4 100-Year Rainfall=7.60"
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Pond 1P: Oversized Pipe**Pond 1P: Oversized Pipe**

Pond 1P: Oversized Pipe

Stage-Area-Storage



Hydrograph for Pond 1P: Oversized Pipe

| Time (hours) | Inflow (cfs) | Storage (acre-feet) | Elevation (feet) | Primary (cfs) |
|-----------------|-----------------|------------------------|---------------------|------------------|
| 0.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 2.00 | 0.00 | 0.111 | 784.00 | 0.00 |
| 4.00 | 0.01 | 0.112 | 784.01 | 0.00 |
| 6.00 | 0.04 | 0.115 | 784.10 | 0.01 |
| 8.00 | 0.08 | 0.123 | 784.28 | 0.02 |
| 10.00 | 0.18 | 0.139 | 784.67 | 0.03 |
| 12.00 | 3.73 | 0.234 | 787.38 | 0.87 |
| 14.00 | 0.23 | 0.220 | 786.85 | 0.29 |
| 16.00 | 0.12 | 0.215 | 786.71 | 0.13 |
| 18.00 | 0.10 | 0.214 | 786.67 | 0.10 |
| 20.00 | 0.07 | 0.213 | 786.63 | 0.08 |
| 22.00 | 0.05 | 0.211 | 786.58 | 0.06 |
| 24.00 | 0.02 | 0.207 | 786.46 | 0.06 |
| 26.00 | 0.00 | 0.198 | 786.19 | 0.06 |
| 28.00 | 0.00 | 0.189 | 785.94 | 0.05 |
| 30.00 | 0.00 | 0.181 | 785.72 | 0.05 |
| 32.00 | 0.00 | 0.173 | 785.52 | 0.05 |
| 34.00 | 0.00 | 0.166 | 785.33 | 0.04 |
| 36.00 | 0.00 | 0.159 | 785.16 | 0.04 |
| 38.00 | 0.00 | 0.153 | 785.00 | 0.04 |
| 40.00 | 0.00 | 0.147 | 784.86 | 0.03 |
| 42.00 | 0.00 | 0.141 | 784.73 | 0.03 |
| 44.00 | 0.00 | 0.136 | 784.61 | 0.03 |
| 46.00 | 0.00 | 0.132 | 784.50 | 0.03 |
| 48.00 | 0.00 | 0.128 | 784.40 | 0.02 |
| 50.00 | 0.00 | 0.125 | 784.32 | 0.02 |
| 52.00 | 0.00 | 0.122 | 784.25 | 0.02 |
| 54.00 | 0.00 | 0.119 | 784.18 | 0.01 |
| 56.00 | 0.00 | 0.117 | 784.14 | 0.01 |
| 58.00 | 0.00 | 0.115 | 784.10 | 0.01 |
| 60.00 | 0.00 | 0.114 | 784.07 | 0.01 |
| 62.00 | 0.00 | 0.114 | 784.05 | 0.00 |
| 64.00 | 0.00 | 0.113 | 784.04 | 0.00 |
| 66.00 | 0.00 | 0.113 | 784.03 | 0.00 |
| 68.00 | 0.00 | 0.113 | 784.03 | 0.00 |
| 70.00 | 0.00 | 0.112 | 784.03 | 0.00 |
| 72.00 | 0.00 | 0.112 | 784.02 | 0.00 |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Proposed Conditions
MSE 24-hr 4 100-Year Rainfall=7.60"
Printed 9/16/2024
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Stage-Discharge for Pond 1P: Oversized Pipe

| Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) | Elevation (feet) | Primary (cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 780.50 | 0.00 | 783.05 | 0.00 | 785.60 | 0.05 |
| 780.55 | 0.00 | 783.10 | 0.00 | 785.65 | 0.05 |
| 780.60 | 0.00 | 783.15 | 0.00 | 785.70 | 0.05 |
| 780.65 | 0.00 | 783.20 | 0.00 | 785.75 | 0.05 |
| 780.70 | 0.00 | 783.25 | 0.00 | 785.80 | 0.05 |
| 780.75 | 0.00 | 783.30 | 0.00 | 785.85 | 0.05 |
| 780.80 | 0.00 | 783.35 | 0.00 | 785.90 | 0.05 |
| 780.85 | 0.00 | 783.40 | 0.00 | 785.95 | 0.05 |
| 780.90 | 0.00 | 783.45 | 0.00 | 786.00 | 0.05 |
| 780.95 | 0.00 | 783.50 | 0.00 | 786.05 | 0.05 |
| 781.00 | 0.00 | 783.55 | 0.00 | 786.10 | 0.05 |
| 781.05 | 0.00 | 783.60 | 0.00 | 786.15 | 0.05 |
| 781.10 | 0.00 | 783.65 | 0.00 | 786.20 | 0.06 |
| 781.15 | 0.00 | 783.70 | 0.00 | 786.25 | 0.06 |
| 781.20 | 0.00 | 783.75 | 0.00 | 786.30 | 0.06 |
| 781.25 | 0.00 | 783.80 | 0.00 | 786.35 | 0.06 |
| 781.30 | 0.00 | 783.85 | 0.00 | 786.40 | 0.06 |
| 781.35 | 0.00 | 783.90 | 0.00 | 786.45 | 0.06 |
| 781.40 | 0.00 | 783.95 | 0.00 | 786.50 | 0.06 |
| 781.45 | 0.00 | 784.00 | 0.00 | 786.55 | 0.06 |
| 781.50 | 0.00 | 784.05 | 0.00 | 786.60 | 0.07 |
| 781.55 | 0.00 | 784.10 | 0.01 | 786.65 | 0.09 |
| 781.60 | 0.00 | 784.15 | 0.01 | 786.70 | 0.13 |
| 781.65 | 0.00 | 784.20 | 0.01 | 786.75 | 0.17 |
| 781.70 | 0.00 | 784.25 | 0.02 | 786.80 | 0.23 |
| 781.75 | 0.00 | 784.30 | 0.02 | 786.85 | 0.29 |
| 781.80 | 0.00 | 784.35 | 0.02 | 786.90 | 0.36 |
| 781.85 | 0.00 | 784.40 | 0.02 | 786.95 | 0.43 |
| 781.90 | 0.00 | 784.45 | 0.02 | 787.00 | 0.49 |
| 781.95 | 0.00 | 784.50 | 0.03 | 787.05 | 0.54 |
| 782.00 | 0.00 | 784.55 | 0.03 | 787.10 | 0.58 |
| 782.05 | 0.00 | 784.60 | 0.03 | 787.15 | 0.63 |
| 782.10 | 0.00 | 784.65 | 0.03 | 787.20 | 0.67 |
| 782.15 | 0.00 | 784.70 | 0.03 | 787.25 | 0.70 |
| 782.20 | 0.00 | 784.75 | 0.03 | 787.30 | 0.74 |
| 782.25 | 0.00 | 784.80 | 0.03 | 787.35 | 0.77 |
| 782.30 | 0.00 | 784.85 | 0.03 | 787.40 | 0.95 |
| 782.35 | 0.00 | 784.90 | 0.03 | 787.45 | 1.24 |
| 782.40 | 0.00 | 784.95 | 0.04 | 787.50 | 1.62 |
| 782.45 | 0.00 | 785.00 | 0.04 | 787.55 | 2.05 |
| 782.50 | 0.00 | 785.05 | 0.04 | 787.60 | 2.53 |
| 782.55 | 0.00 | 785.10 | 0.04 | 787.65 | 3.06 |
| 782.60 | 0.00 | 785.15 | 0.04 | 787.70 | 3.63 |
| 782.65 | 0.00 | 785.20 | 0.04 | 787.75 | 4.24 |
| 782.70 | 0.00 | 785.25 | 0.04 | 787.80 | 4.88 |
| 782.75 | 0.00 | 785.30 | 0.04 | 787.85 | 5.55 |
| 782.80 | 0.00 | 785.35 | 0.04 | 787.90 | 6.25 |
| 782.85 | 0.00 | 785.40 | 0.04 | 787.95 | 6.99 |
| 782.90 | 0.00 | 785.45 | 0.04 | 788.00 | 7.74 |
| 782.95 | 0.00 | 785.50 | 0.05 | | |
| 783.00 | 0.00 | 785.55 | 0.05 | | |

Retreat Center - Copy3

Prepared by Vierbicher Associates

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Proposed Conditions
MSE 24-hr 4 100-Year Rainfall=7.60"
 Printed 9/16/2024
 Page 60

Stage-Area-Storage for Pond 1P: Oversized Pipe

| Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) | Elevation (feet) | Storage (acre-feet) |
|---------------------|------------------------|---------------------|------------------------|---------------------|------------------------|
| 780.50 | 0.000 | 783.05 | 0.073 | 785.60 | 0.176 |
| 780.55 | 0.000 | 783.10 | 0.075 | 785.65 | 0.178 |
| 780.60 | 0.001 | 783.15 | 0.077 | 785.70 | 0.180 |
| 780.65 | 0.001 | 783.20 | 0.079 | 785.75 | 0.182 |
| 780.70 | 0.002 | 783.25 | 0.081 | 785.80 | 0.184 |
| 780.75 | 0.002 | 783.30 | 0.083 | 785.85 | 0.186 |
| 780.80 | 0.003 | 783.35 | 0.085 | 785.90 | 0.188 |
| 780.85 | 0.004 | 783.40 | 0.087 | 785.95 | 0.189 |
| 780.90 | 0.005 | 783.45 | 0.089 | 786.00 | 0.191 |
| 780.95 | 0.006 | 783.50 | 0.091 | 786.05 | 0.193 |
| 781.00 | 0.007 | 783.55 | 0.093 | 786.10 | 0.195 |
| 781.05 | 0.008 | 783.60 | 0.095 | 786.15 | 0.197 |
| 781.10 | 0.009 | 783.65 | 0.097 | 786.20 | 0.198 |
| 781.15 | 0.010 | 783.70 | 0.099 | 786.25 | 0.200 |
| 781.20 | 0.011 | 783.75 | 0.101 | 786.30 | 0.202 |
| 781.25 | 0.013 | 783.80 | 0.103 | 786.35 | 0.204 |
| 781.30 | 0.014 | 783.85 | 0.105 | 786.40 | 0.205 |
| 781.35 | 0.015 | 783.90 | 0.107 | 786.45 | 0.207 |
| 781.40 | 0.017 | 783.95 | 0.109 | 786.50 | 0.209 |
| 781.45 | 0.018 | 784.00 | 0.111 | 786.55 | 0.210 |
| 781.50 | 0.019 | 784.05 | 0.113 | 786.60 | 0.212 |
| 781.55 | 0.021 | 784.10 | 0.116 | 786.65 | 0.214 |
| 781.60 | 0.022 | 784.15 | 0.118 | 786.70 | 0.215 |
| 781.65 | 0.024 | 784.20 | 0.120 | 786.75 | 0.217 |
| 781.70 | 0.025 | 784.25 | 0.122 | 786.80 | 0.218 |
| 781.75 | 0.027 | 784.30 | 0.124 | 786.85 | 0.220 |
| 781.80 | 0.028 | 784.35 | 0.126 | 786.90 | 0.221 |
| 781.85 | 0.030 | 784.40 | 0.128 | 786.95 | 0.223 |
| 781.90 | 0.031 | 784.45 | 0.130 | 787.00 | 0.224 |
| 781.95 | 0.033 | 784.50 | 0.132 | 787.05 | 0.226 |
| 782.00 | 0.035 | 784.55 | 0.134 | 787.10 | 0.227 |
| 782.05 | 0.036 | 784.60 | 0.136 | 787.15 | 0.228 |
| 782.10 | 0.038 | 784.65 | 0.138 | 787.20 | 0.229 |
| 782.15 | 0.040 | 784.70 | 0.140 | 787.25 | 0.231 |
| 782.20 | 0.041 | 784.75 | 0.142 | 787.30 | 0.232 |
| 782.25 | 0.043 | 784.80 | 0.144 | 787.35 | 0.233 |
| 782.30 | 0.045 | 784.85 | 0.146 | 787.40 | 0.234 |
| 782.35 | 0.047 | 784.90 | 0.148 | 787.45 | 0.235 |
| 782.40 | 0.048 | 784.95 | 0.150 | 787.50 | 0.236 |
| 782.45 | 0.050 | 785.00 | 0.152 | 787.55 | 0.237 |
| 782.50 | 0.052 | 785.05 | 0.155 | 787.60 | 0.238 |
| 782.55 | 0.054 | 785.10 | 0.157 | 787.65 | 0.239 |
| 782.60 | 0.056 | 785.15 | 0.159 | 787.70 | 0.240 |
| 782.65 | 0.058 | 785.20 | 0.161 | 787.75 | 0.241 |
| 782.70 | 0.060 | 785.25 | 0.163 | 787.80 | 0.242 |
| 782.75 | 0.061 | 785.30 | 0.165 | 787.85 | 0.242 |
| 782.80 | 0.063 | 785.35 | 0.166 | 787.90 | 0.243 |
| 782.85 | 0.065 | 785.40 | 0.168 | 787.95 | 0.243 |
| 782.90 | 0.067 | 785.45 | 0.170 | 788.00 | 0.243 |
| 782.95 | 0.069 | 785.50 | 0.172 | | |
| 783.00 | 0.071 | 785.55 | 0.174 | | |

5 Sediment Reduction Calculations

Data file name: M:\Duncan G. Stroik Architect\200196_LaCrosse Retreat Center\Design Development\Stormwater and Erosion Control\Modeling\TSS Modeling\Underg
 WinSLAMM Version 10.5.0
 Rain file name: C:\WinSLAMM Files\Rain Files\WisReg - Madison WI 1981.RAN
 Particulate Solids Concentration file name: C:\WinSLAMM Files\v10.1 WI_AVG01.pscx
 Runoff Coefficient file name: C:\WinSLAMM Files\WI_SL06 Dec06.rsvx
 Residential Street Delivery file name: C:\WinSLAMM Files\WI_Res and Other Urban Dec06.std
 Institutional Street Delivery file name: C:\WinSLAMM Files\WI_Com Inst Indust Dec06.std
 Commercial Street Delivery file name: C:\WinSLAMM Files\WI_Com Inst Indust Dec06.std
 Industrial Street Delivery file name: C:\WinSLAMM Files\WI_Com Inst Indust Dec06.std
 Other Urban Street Delivery file name: C:\WinSLAMM Files\WI_Res and Other Urban Dec06.std
 Freeway Street Delivery file name: C:\WinSLAMM Files\Freeway Dec06.std
 Apply Street Delivery Files to Adjust the After Event Load Street Dirt Mass Balance: False
 Pollutant Relative Concentration file name: C:\WinSLAMM Files\WI_GEO03.ppdx
 Source Area PSD and Peak to Average Flow Ratio File: C:\WinSLAMM Files\NURP Source Area PSD Files.csv
 Cost Data file name:
 Seed for random number generator: -42
 Study period starting date: 01/01/81 Study period ending date: 12/31/81
 Start of Winter Season: 12/02 End of Winter Season: 03/12
 Date: 08-14-2024 Time: 12:21:13
 Site information:

LU# 1 - Institutional: Project Detained A1 Total area (ac): 0.705
 1 - Roofs 1: 0.198 ac. Pitched Connected PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 13 - Paved Parking 1: 0.051 ac. Connected PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 25 - Driveways 1: 0.230 ac. Connected PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 31 - Sidewalks 1: 0.033 ac. Connected PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 51 - Small Landscaped Areas 1: 0.193 ac. Normal Silty PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz

 LU# 2 - Institutional: Runon Detained A2 Total area (ac): 0.110
 1 - Roofs 1: 0.074 ac. Pitched Connected PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 31 - Sidewalks 1: 0.013 ac. Connected PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 51 - Small Landscaped Areas 1: 0.023 ac. Normal Silty PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz

 LU# 3 - Institutional: Project Undetained A3 Total area (ac): 0.182
 57 - Undeveloped Areas 1: 0.167 ac. Normal Silty PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz
 78 - Other Part Con Imp Areas 1: 0.015 ac. Disconnected Normal Silty PSD File: C:\WinSLAMM Files\NURP.cpz Source Area PSD File: C:\WinSLAMM Files\NURP.cpz

Control Practice 1: Wet Detention Pond CP# 1 (DS) - DS Wet Pond # 1
 Particle Size Distribution file name: Not needed - calculated by program

Initial stage elevation (ft): 3.5

Peak to Average Flow Ratio: 3.8

Maximum flow allowed into pond (cfs): No maximum value entered

Outlet Characteristics:

Outlet type: Orifice 1

1. Orifice diameter (ft): 0.08
2. Number of orifices: 1
3. Invert elevation above datum (ft): 3.5

Outlet type: Orifice 2

1. Orifice diameter (ft): 0.5
2. Number of orifices: 1
3. Invert elevation above datum (ft): 5

Outlet type: Broad Crested Weir

1. Weir crest length (ft): 0.01
2. Weir crest width (ft): 0.01
3. Height from datum to bottom of weir opening: 7.49

Pond stage and surface area

| Entry Number | Stage (ft) | Pond Area (acres) | Natural Seepage (in/hr) | Other Outflow (cfs) |
|--------------|------------|-------------------|-------------------------|---------------------|
| 0 | 0.00 | 0.0000 | 0.00 | 0.00 |
| 1 | 0.01 | 0.0402 | 0.00 | 0.00 |
| 2 | 0.50 | 0.0402 | 0.00 | 0.00 |
| 3 | 1.00 | 0.0402 | 0.00 | 0.00 |
| 4 | 1.50 | 0.0402 | 0.00 | 0.00 |
| 5 | 2.00 | 0.0402 | 0.00 | 0.00 |
| 6 | 2.50 | 0.0402 | 0.00 | 0.00 |
| 7 | 3.00 | 0.0402 | 0.00 | 0.00 |
| 8 | 3.50 | 0.0402 | 0.00 | 0.00 |
| 9 | 4.00 | 0.0402 | 0.00 | 0.00 |
| 10 | 4.50 | 0.0402 | 0.00 | 0.00 |
| 11 | 5.00 | 0.0402 | 0.00 | 0.00 |
| 12 | 5.50 | 0.0402 | 0.00 | 0.00 |
| 13 | 6.00 | 0.0402 | 0.00 | 0.00 |
| 14 | 7.00 | 0.0402 | 0.00 | 0.00 |
| 15 | 7.50 | 0.0402 | 0.00 | 0.00 |

SLAMM for Windows Version 10.5.0

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Data file name: M:\Duncan G. Stroik Architect\200196_LaCrosse Retreat Center\Design Development\Stormwater and Erosion Control\Modeling\TSS Modeling\Underg WinSLAMM Version 10.5.0

Rain file name: C:\WinSLAMM Files\Rain Files\WisReg - Madison WI 1981.RAN

Particulate Solids Concentration file name: C:\WinSLAMM Files\v10.1 WI_AVG01.pscx

Runoff Coefficient file name: C:\WinSLAMM Files\WI_SL06 Dec06.rsvx

Pollutant Relative Concentration file name: C:\WinSLAMM Files\WI_GEO03.ppdx

Residential Street Delivery file name: C:\WinSLAMM Files\WI_Res and Other Urban Dec06.std

Institutional Street Delivery file name: C:\WinSLAMM Files\WI_Com Inst Indust Dec06.std

Commercial Street Delivery file name: C:\WinSLAMM Files\WI_Com Inst Indust Dec06.std

Industrial Street Delivery file name: C:\WinSLAMM Files\WI_Com Inst Indust Dec06.std

Other Urban Street Delivery file name: C:\WinSLAMM Files\WI_Res and Other Urban Dec06.std

Freeway Street Delivery file name: C:\WinSLAMM Files\Freeway Dec06.std

Apply Street Delivery Files to Adjust the After Event Load Street Dirt Mass Balance: False

Source Area PSD and Peak to Average Flow Ratio File: C:\WinSLAMM Files\NURP Source Area PSD Files.csv

Cost Data file name:

Seed for random number generator: -42

Study period starting date: 01/01/81 Study period ending date: 12/31/81

Start of Winter Season: 12/02 End of Winter Season: 03/12

Model Run Start Date: 01/01/81 Model Run End Date: 12/31/81

Date of run: 08-14-2024 Time of run: 12:19:28

Total Area Modeled (acres): 0.997

Years in Model Run: 1.00

| | Runoff Volume (cu ft) | Percent Runoff Volume Reduction | Particulate Solids Conc. (mg/L) | Particulate Solids Yield (lbs) | Percent Particulate Solids Reduction |
|--|--------------------------|------------------------------------|------------------------------------|-----------------------------------|--------------------------------------|
| Total of all Land Uses without Controls: | 53392 | - | 87.15 | 290.5 | - |
| Outfall Total with Controls: | 53470 | -0.15% | 13.42 | 44.79 | 84.58% |
| Annualized Total After Outfall Controls: | 53616 | | | 44.91 | |

Exhibits

8.1 Stormwater Maintenance Agreement

DECLARATION OF CONDITIONS, COVENANTS AND RESTRICTIONS FOR MAINTENANCE OF STORMWATER MANAGEMENT MEASURES

RECITALS:

- A. Shrine of Our Lady of Guadalupe, Inc. is the owner of the property located at 5250 Justin Road in the City La Crosse, more particularly described on Exhibit A attached hereto (“Property”).
 - B. Owner desires to construct buildings and/or parking facilities on the Property in accordance with certain plans and specifications approved by the City.
 - C. The City requires Owner to record this Declaration regarding maintenance of stormwater management measures to be located on the Property. Owner agrees to maintain the stormwater management measures and to grant to the City the rights set forth below.

NOW, THEREFORE, in consideration of the declarations herein and other good and valuable consideration, the receipt and sufficiency of which are hereby acknowledged, the owner agrees as follows:

1.

Maintenance. Owner and its successors and assigns shall be responsible to repair and maintain the stormwater management measures located on the Property in good condition and in working order and such that the measures comply with the approved plans on file with the City Engineer. Said maintenance shall be at the Owner's sole cost and expense. Owner will conduct such maintenance or repair work in accordance with all applicable laws, codes, regulations, and similar requirements, and pursuant to the Maintenance Provisions attached hereto as Exhibit B.
 2.

Easement to City. If Owner fails to maintain the stormwater management measures as required in Section 1, then City shall have the right, after providing Owner with written notice of the maintenance issue ("Maintenance Notice") and thirty (30) days to comply with the City's maintenance request, to enter the Property in order to conduct the maintenance specified in the Maintenance Notice. City will conduct such maintenance work in accordance with all applicable laws, codes, regulations, and similar requirements and will not unreasonably interfere with Owner's use of the Property. All costs and expenses incurred by the City in conducting such maintenance may be charged to the owner of the Property by placing the amount on the tax roll for the Property as a special charge in accordance with Section 66.0627, Wis. Stats.
 3.

Term/Termination. The term of this Agreement shall commence on the date that this Agreement is filed of record with the Register of Deeds Office for La Crosse County, Wisconsin, and except as otherwise herein specifically provided, shall continue in perpetuity. Notwithstanding the foregoing, this Agreement may be terminated by recording with the Register of Deeds Office for La Crosse County, Wisconsin, a written instrument of termination signed by the City and all of the then-owners of the Property.
 4.

Miscellaneous.

 - (a)

Notices. Any notice, request or demand required or permitted under this Agreement shall be in writing and shall be deemed given when personally served or three (3) days after the same has been deposited with the United States

This space is reserved for recording data

| Return to:

City of La Crosse
Engineering Department
400 La Crosse Street
La Crosse, Wisconsin 54601

Tax Parcel No.: 17-50365 -100

4. Miscellaneous.

- (a) Notices. Any notice, request or demand required or permitted under this Agreement shall be in writing and shall be deemed given when personally served or three (3) days after the same has been deposited with the United States Post Office, registered or certified mail, return receipt requested, postage prepaid and addressed as follows:

If to Owner: Shrine of Our Lady of Guadalupe, Inc.
5250 Justin Rd.
PO Box 1237
La Crosse, WI 54601

Any party may change its address for the receipt of notice by written notice to the other.

- (b) Governing Law. This Agreement shall be governed and construed in accordance with the laws of the State of Wisconsin.
 - (c) Amendments or Further Agreements to be in Writing. This Agreement may not be modified in whole or in part unless such agreement is in writing and signed by all parties bound hereby.
 - (d) Covenants Running with the Land. All of the easements, restrictions, covenants and agreements set forth in this Agreement are intended to be and shall be construed as covenants running with the land, binding upon, inuring to the benefit of, and enforceable by the parties hereto and their respective successors and assigns.
 - (e) Partial Invalidity. If any provisions, or portions thereof, of this Agreement or the application thereof to any person or circumstance shall, to any extent, be invalid or unenforceable, the remainder of this Agreement, or the application of such provision, or portion thereof, to any other persons or circumstances shall not be affected thereby and each provision of this Agreement shall be valid and enforceable to the fullest extent permitted by law.

IN WITNESS WHEREOF, we have hereunto set our hands and seals this _____ day of _____, 20_____.




STATE OF WISCONSIN)
COUNTY OF LA CROSSE) SS

Personally came before me this _____ day of _____, 20_____, the above named _____, to me known to be the person(s) who executed the foregoing instrument and acknowledged the same.

NOTARY PUBLIC

My Commission Expires: _____

Drafted by: City of La Crosse
Engineering Department
400 La Crosse Street
La Crosse, Wisconsin 54601

EXHIBIT A

Part of the Northeast quarter of the Northwest quarter (NE/NW), Section 26, Township 15 North, Range 7 West, and also part of the Southeast quarter of the Southwest quarter (SE/SW), and part of the Southwest quarter of the Southeast quarter (SW /SE), and part of the Northwest quarter of the Southeast quarter (NW/SE) of Section 23, Township 15 North, Range 7 West. all located in the Town of Shelby, La Crosse County, Wisconsin, described as follows: Beginning at the South quarter corner of said Section 23, thence along the East line of said NE/NW, S01°51'01"W 330.00 feet; thence N35°06'45"W 411.61 feet to the North line of said NE/NW; thence N40°38'51"E 582.72 feet; thence S89°09'17"E 209.98 feet; thence N00°01'17"W 134.69 feet; thence N05°11'52"W 469.34 feet to the beginning of a 600.00 foot radius curve, concave to the Southeast; thence 332.56 feet along the arc of said curve, the chord of which bears N10°40'50.5"E 328.32 feet to the end of said curve; thence N26°33'33"E 103.23 feet; thence N17°38'18"E 140.11 feet to the arc of a 439 foot radius curve, concave to the Northeast, on the South right of way line of Justin Road; thence along said right of way line, 66.35 feet along the arc of said curve, the chord of which bears S77°42'23.5"E 66.29 feet; thence S17°38'18"W 151.44 feet; thence S26°33'33"W 108.38 feet to the beginning of a 534.00 foot radius curve concave to the Southeast; thence 295.98 feet along the arc of said curve, the chord of which bears S10°40'50.5"W 292.20 feet to the end of said curve; thence S05°11'52"E 472.32 feet; thence S00°01'17"E 138.67 feet; thence S89°09'17"E 216.39 feet; thence S00°12'20"E 180.00 feet; thence S47°21'47"W 400.00 feet to the South line of said SW/SE; thence along said South line N88°24'26"W 331.01 feet to the point of beginning. Said parcel contains 8.90 acres, and is subject to all easements. implied or recorded.

EXHIBIT B

Maintenance Provisions

An initial installation certification (as-built) stamped by a P.E. registered in the State of Wisconsin shall be submitted to the City Engineer upon completion of construction. The as-built shall be of sufficient detail to show the system was constructed and is functioning as designed. A statement by the certifying P.E. along with a drawing and digital photographs will suffice.

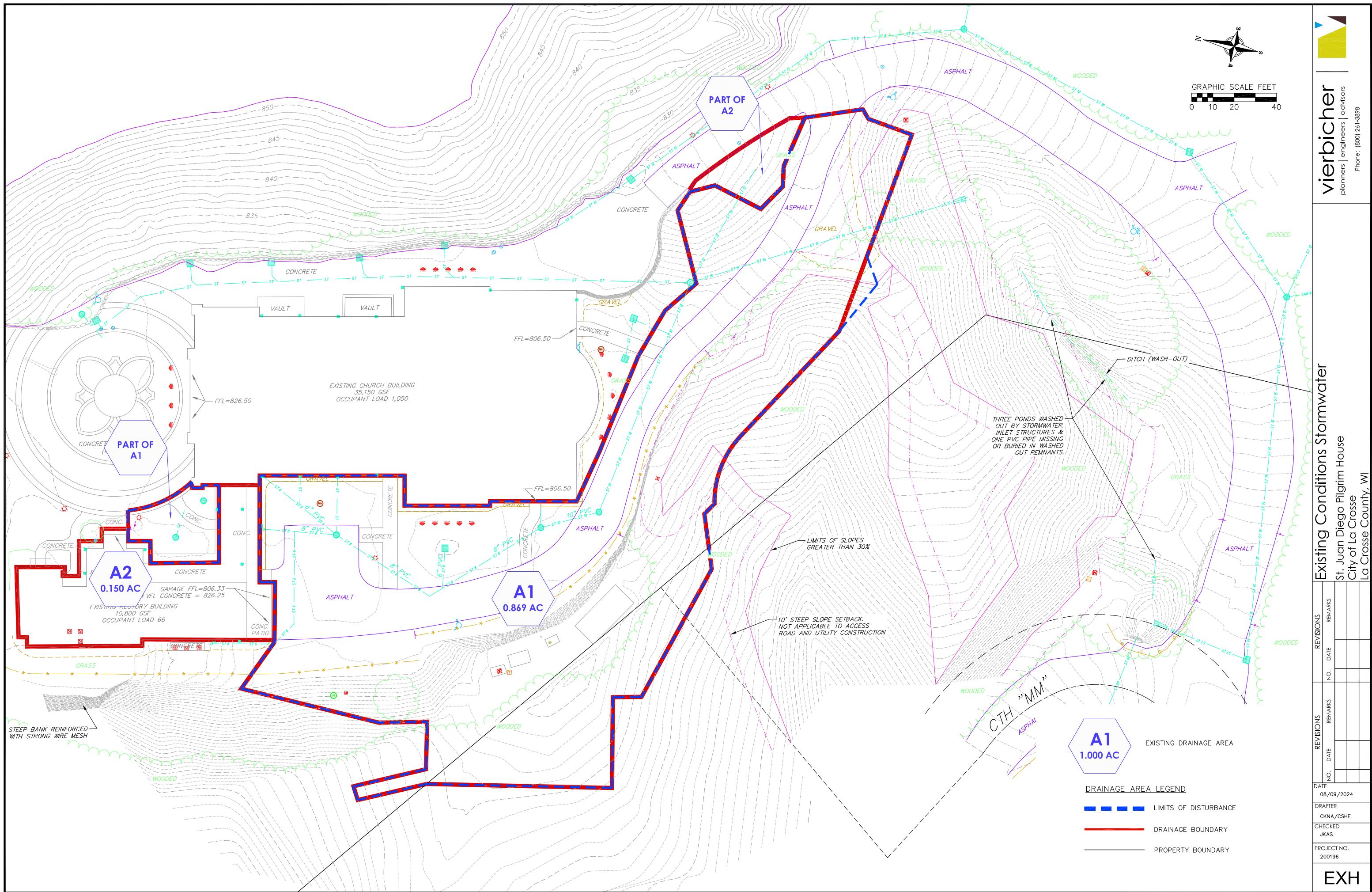
STORM SEWER SYSTEM

- The owner shall maintain all components of the storm sewer system located onsite.
- Installation and maintenance shall be in accordance with the manufacturer's guidelines. Any alterations to the approved storm sewer shall be approved by the City Engineer.
- At a minimum, the storm sewer system shall be inspected annually and cleaned as needed to maintain design capacity.
- Owner shall maintain records of inspections, cleaning and replacement of the storm sewer system all in accordance with Chapter 105 of the La Crosse General Ordinances.

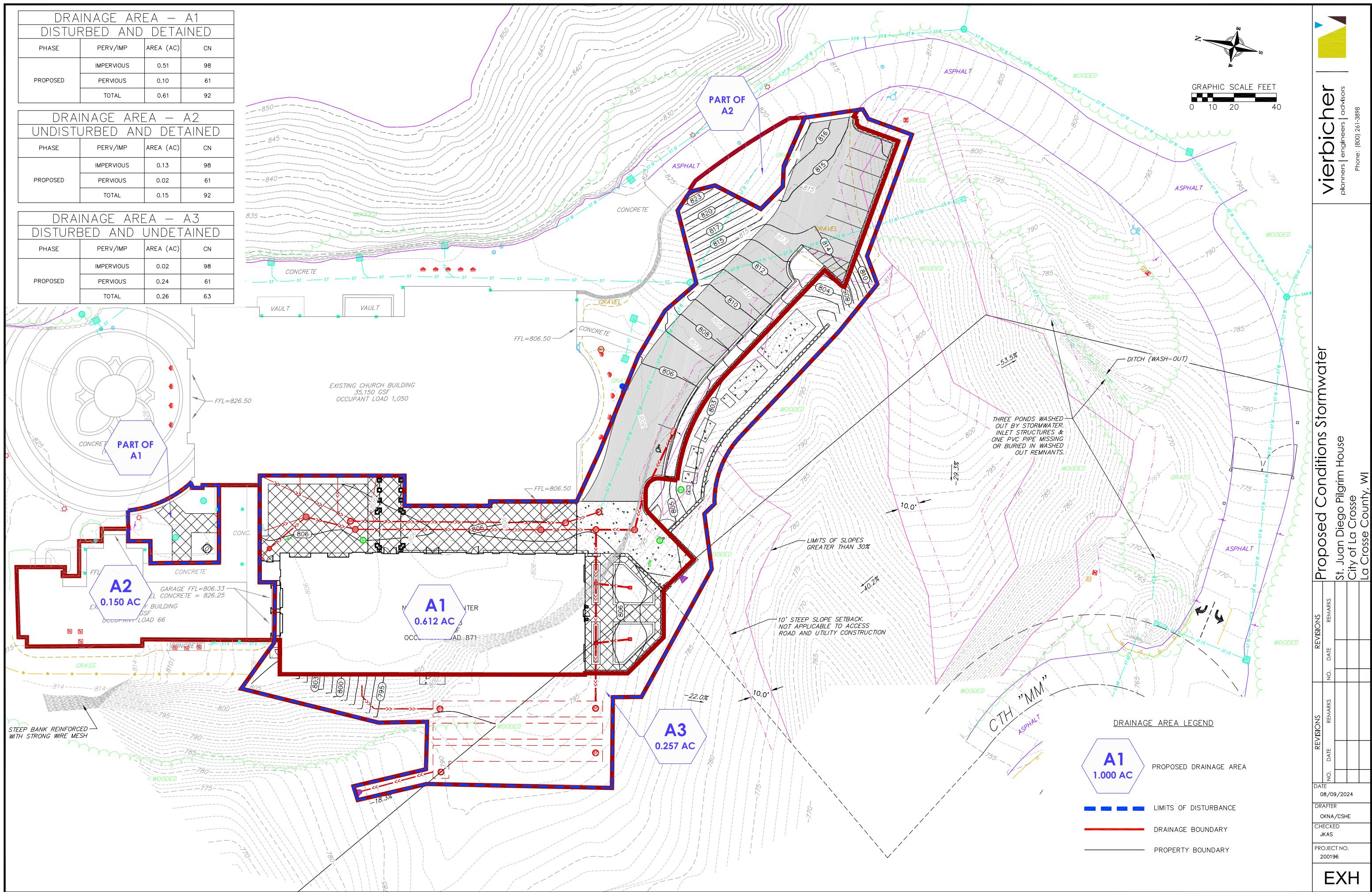
UNDERGROUND STORAGE SYSTEM

- Regular inspections shall be completed at a minimum of once per year, typically in spring. This information will be used to determine the sediment build up within the system. Annual inspections should include the following:
 - Locate the riser sections and cleanouts of the retention/detention system. The riser will typically be 24" in diameter or larger.
 - Remove the lid from a riser.
 - Measure the sediment buildup at each riser and cleanout location. Only certified confined space entry personnel having appropriate equipment should be permitted to enter the retention/detention System.
 - Inspect each manifold, all laterals, and outlet pipes for sediment build up, obstructions, or other problems. Obstructions should be removed at this time.
 - If measured sediment build up is 6 inches or more, cleaning should be performed at the earliest opportunity. A thorough cleaning of the system (manifolds and laterals) shall be performed by either manual methods or by a vacuum truck.
 - All material removed from the system is considered hazardous waste and should be disposed of properly.
- Any alterations to approved underground storage system shall be reviewed and approved by the City Engineer. Owner shall maintain records of inspections, cleaning and replacement of the Underground Storage System all in accordance with Chapter 105 of the La Crosse General Ordinances.

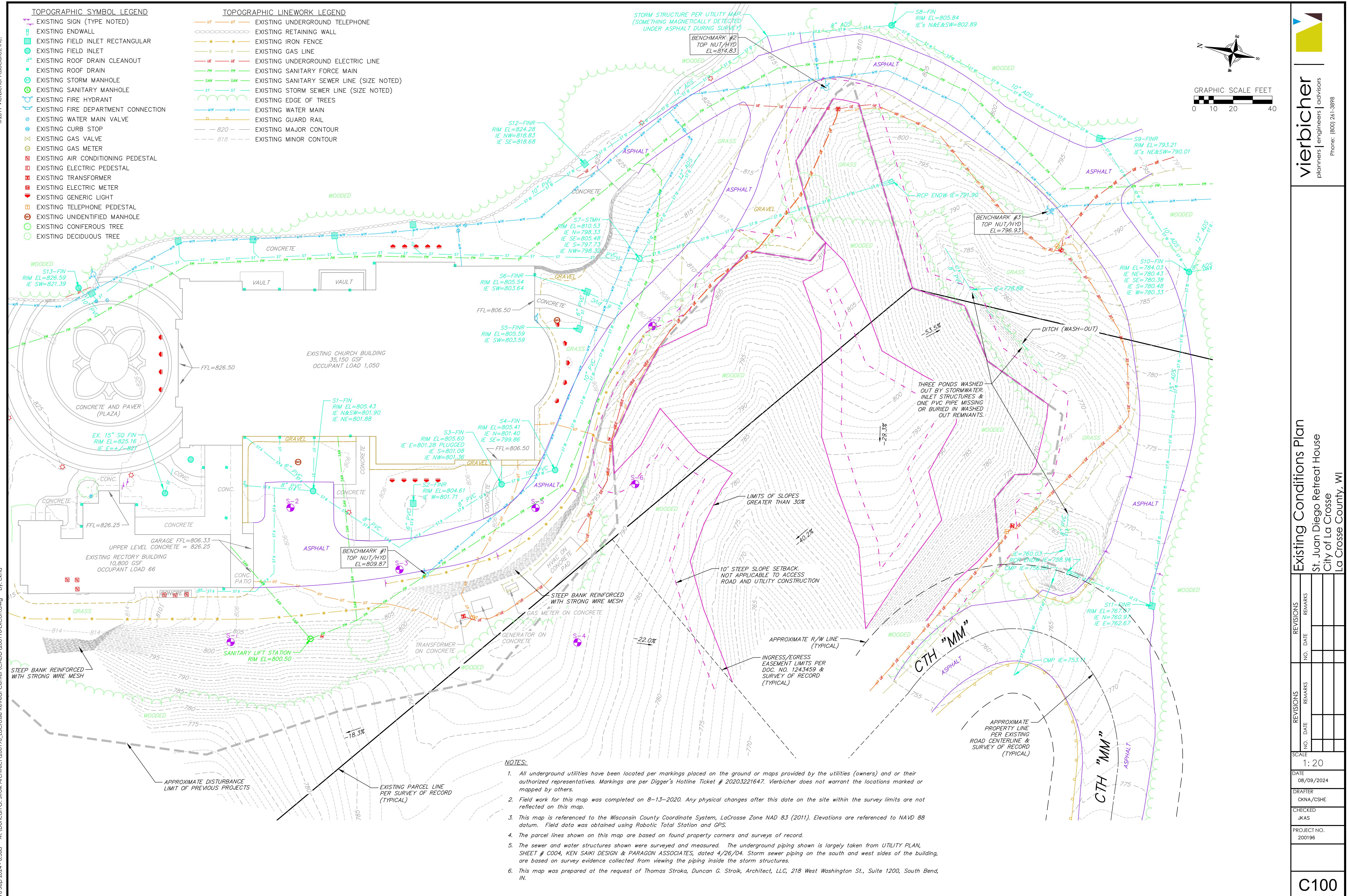
8.2 Pre-Developed Drainage Map



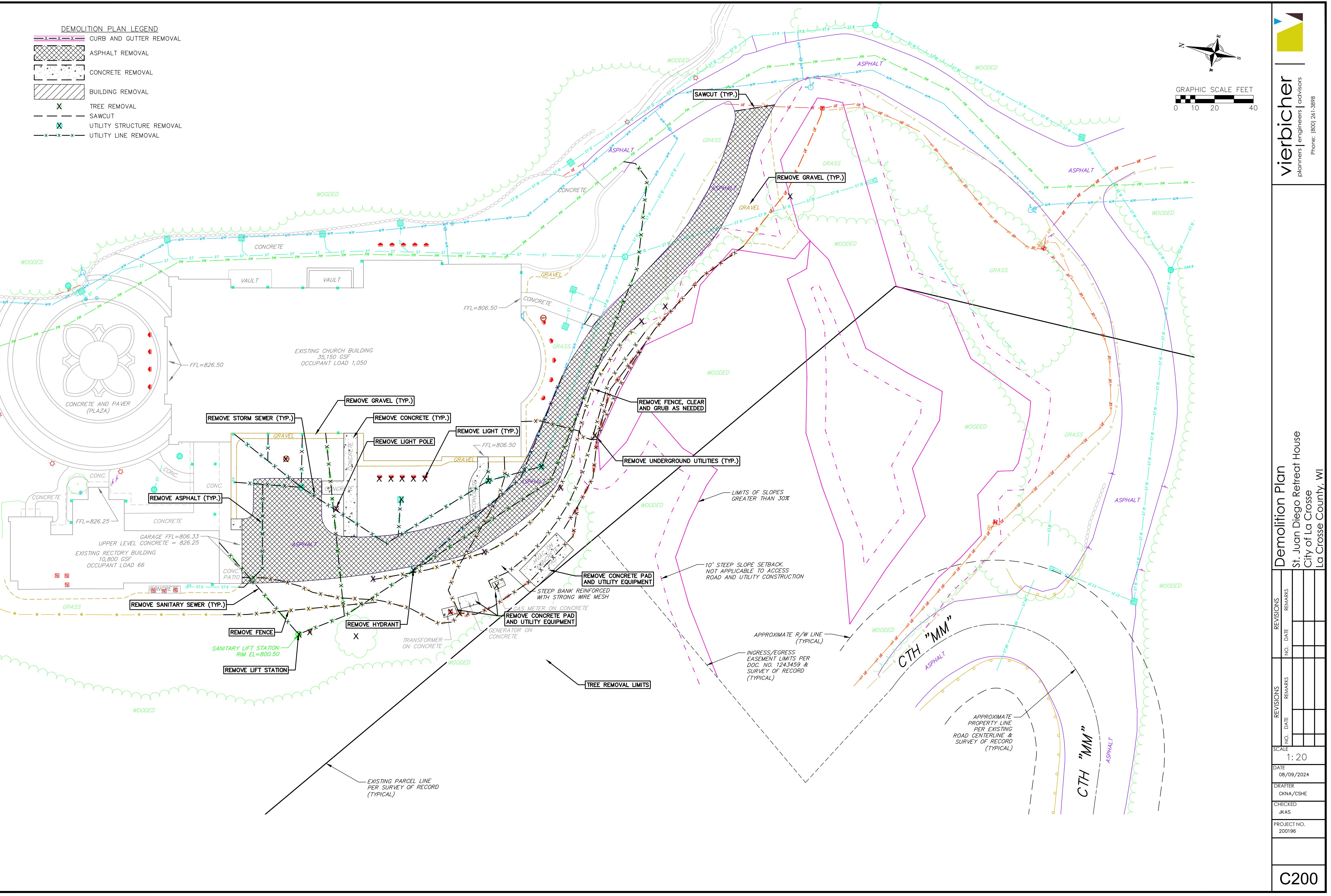
8.3 Post-Developed Drainage Map



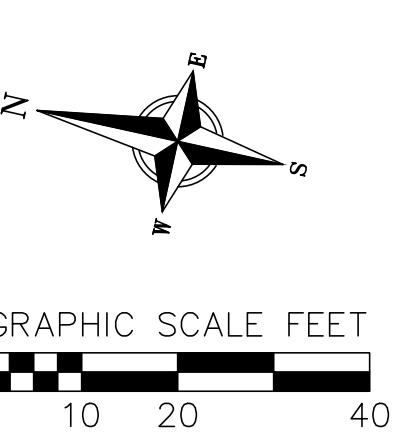
8.4 Construction Plans



16 Sep



| <u>SITE PLAN LEGEND</u> | |
|-------------------------|---------------------------|
| | PROPERTY BOUNDARY |
| | CURB AND GUTTER |
| | PROPOSED RETAINING WALL |
| | PROPOSED CONCRETE |
| | PROPOSED ASPHALT |
| | PROPOSED SIGN |
| | PROPOSED LIGHT POLE |
| | PROPOSED BOLLARD |
| | PROPOSED HANDICAP PARKING |

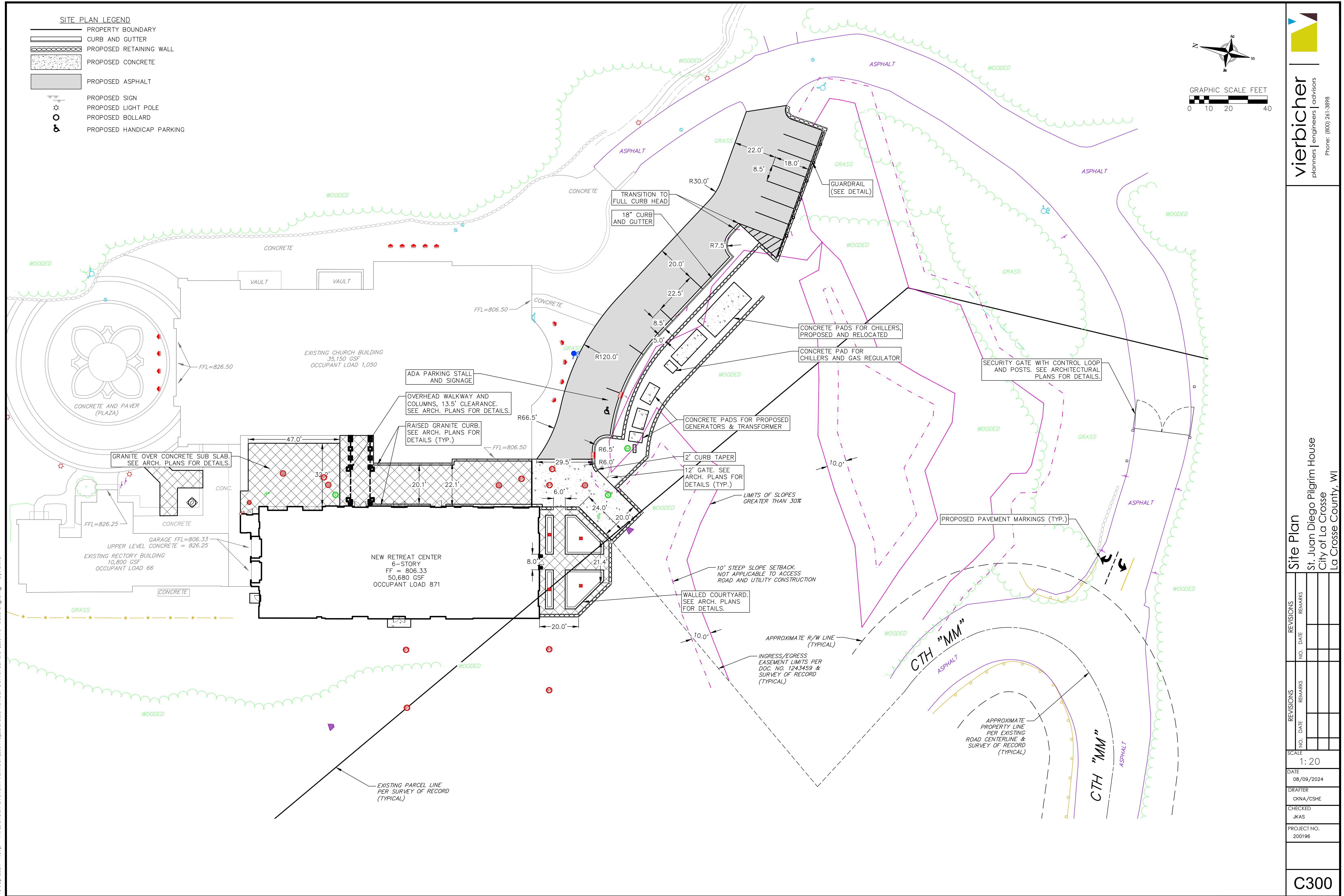


GRAPHIC SCALE FEET
A graphic scale showing markings at 0, 10, 20, and 40 feet. The first 10 feet are marked with a checkerboard pattern, followed by solid black segments for the remaining 30 feet.

vierbicher | planners | engineers | advisers
Phone: (000) 221-2000

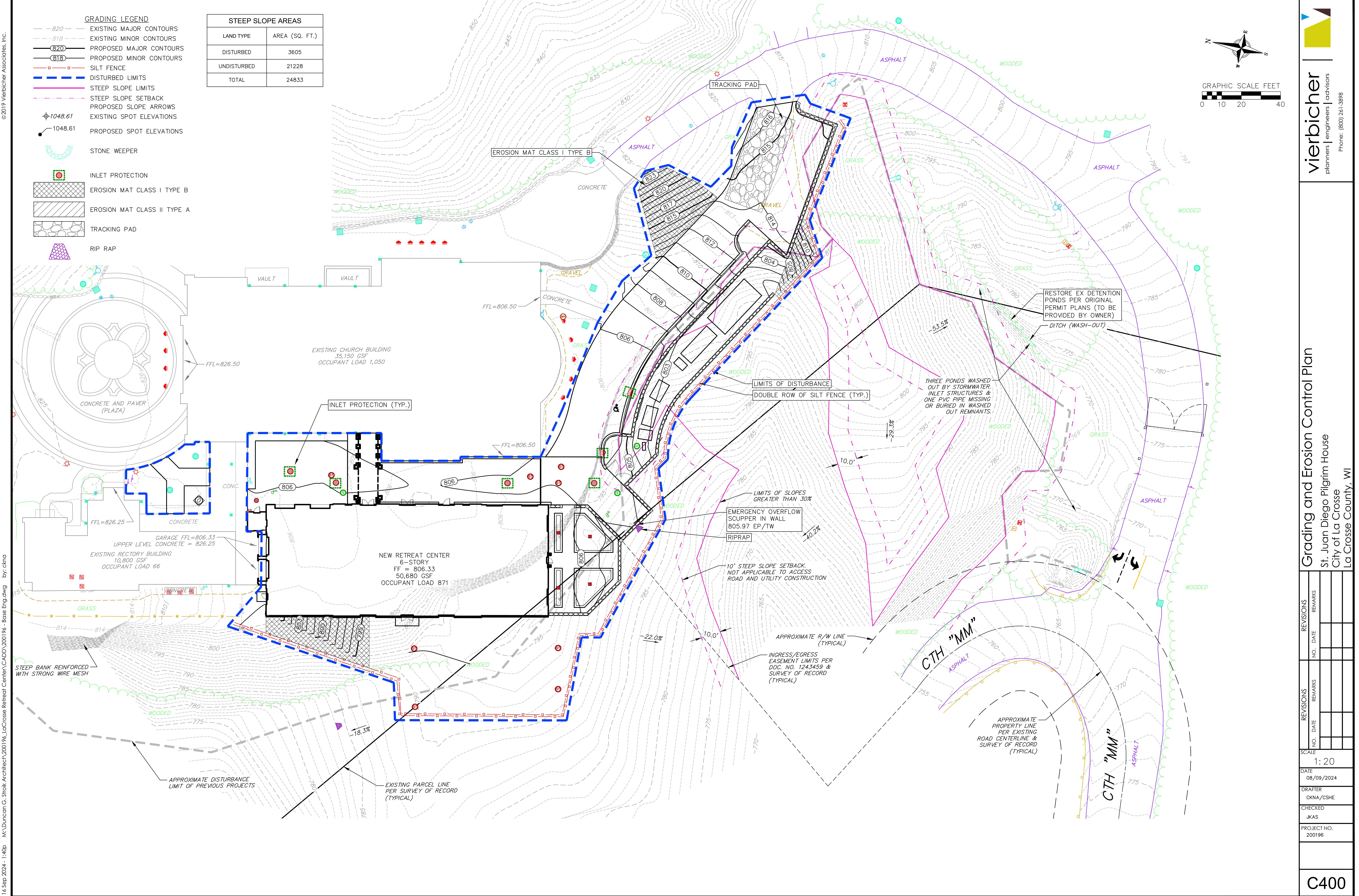
Site Plan

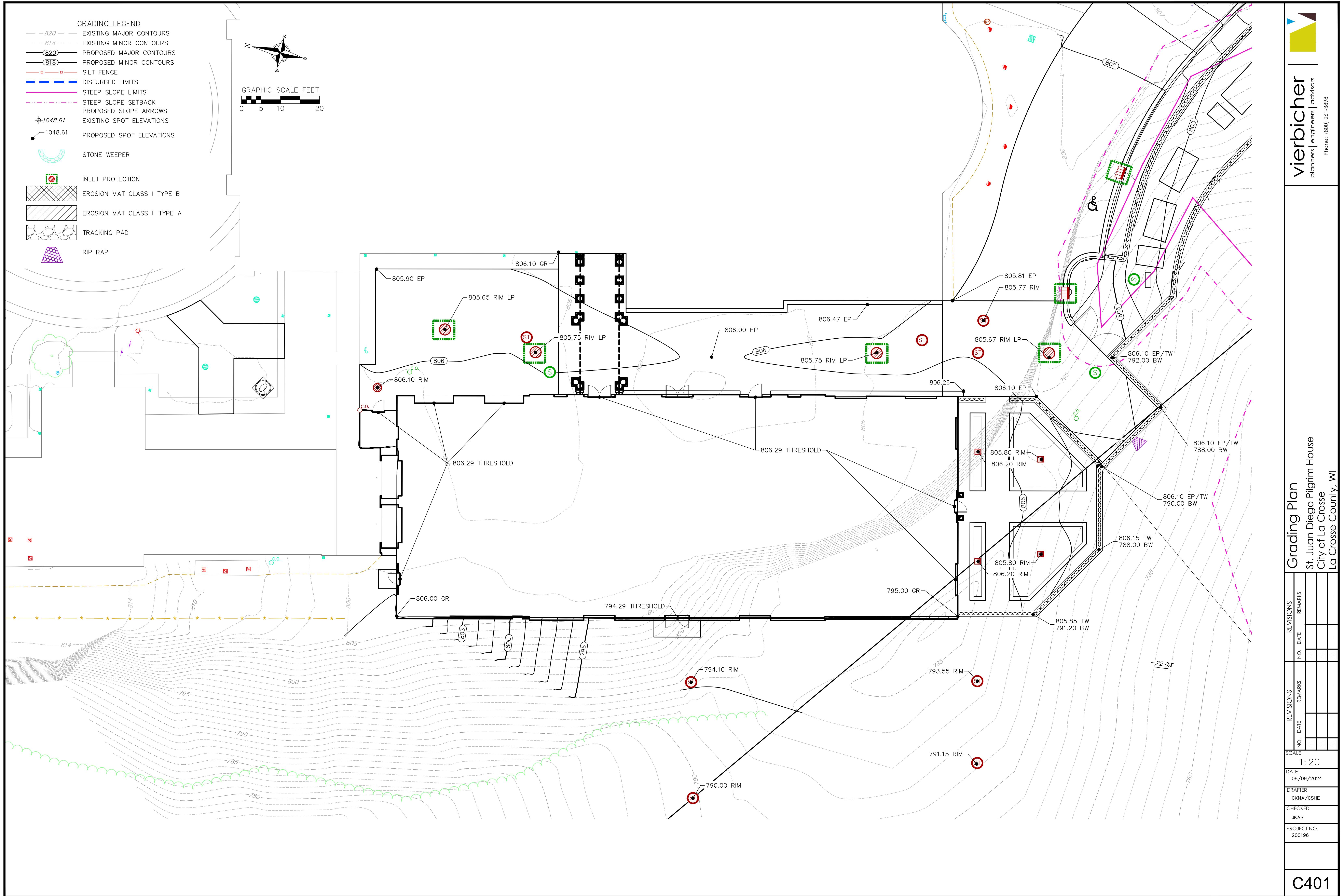
St. Juan Diego Pilgrim House City of La Crosse La Crosse County, WI



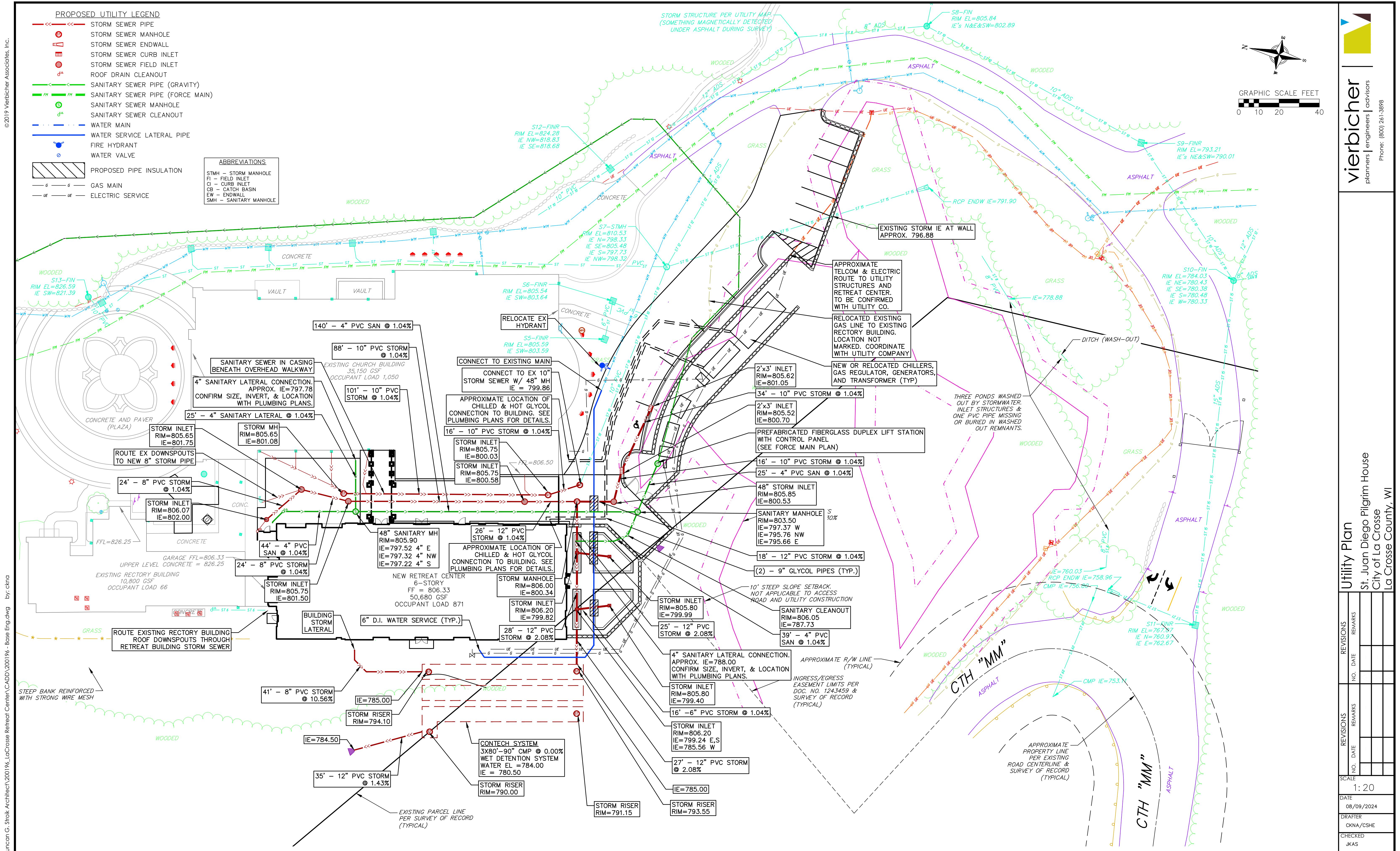
| GRADING LEGEND | |
|-----------------------------|-----------------------------|
| | STEEP SLOPE AREAS |
| — - 820 — | EXISTING MAJOR CONTOURS |
| — - 818 — | EXISTING MINOR CONTOURS |
| — 820 — | PROPOSED MAJOR CONTOURS |
| — 818 — | PROPOSED MINOR CONTOURS |
| — SILT FENCE — | SILT FENCE |
| — DISTURBED LIMITS — | DISTURBED LIMITS |
| — STEEP SLOPE LIMITS — | STEEP SLOPE LIMITS |
| - - - STEEP SLOPE SETBACK — | PROPOSED SLOPE ARROWS |
| PROPOSED SPOT ELEVATIONS | EXISTING SPOT ELEVATIONS |
| STONE WEEPER | STONE WEEPER |
| INLET PROTECTION | INLET PROTECTION |
| Erosion Mat Class I Type B | Erosion Mat Class I Type B |
| Erosion Mat Class II Type A | Erosion Mat Class II Type A |
| TRACKING PAD | TRACKING PAD |
| RIP RAP | RIP RAP |

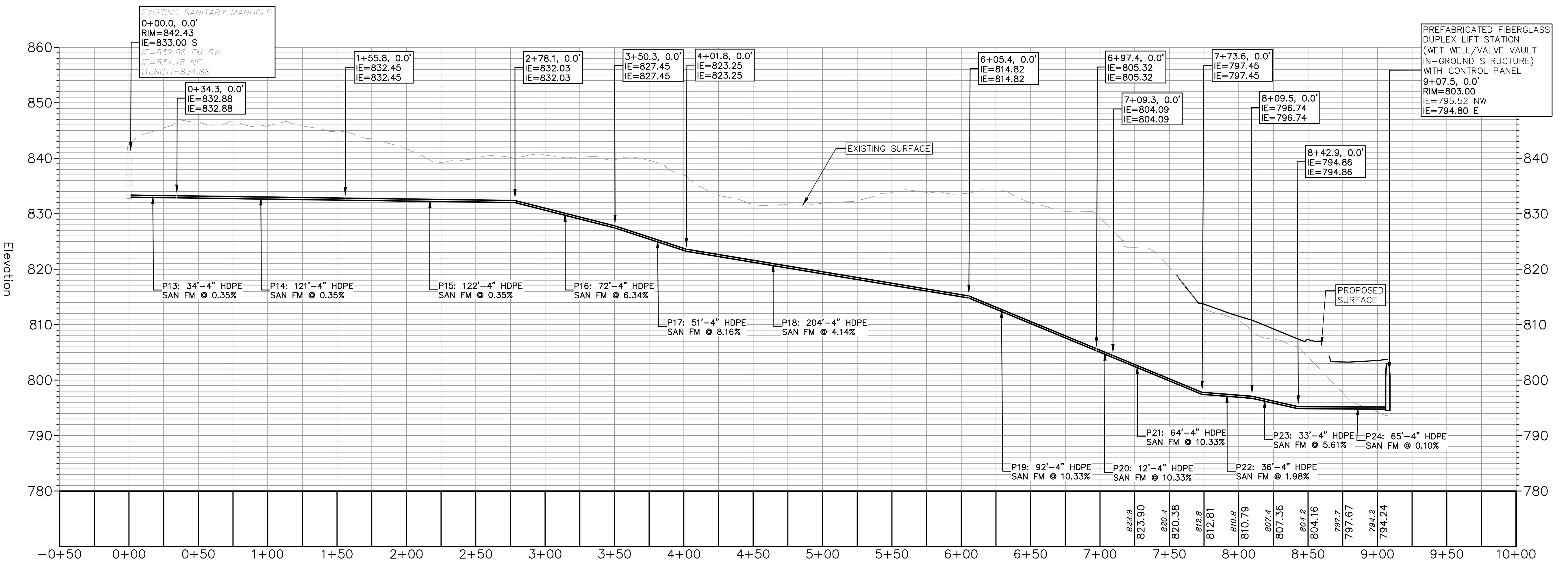
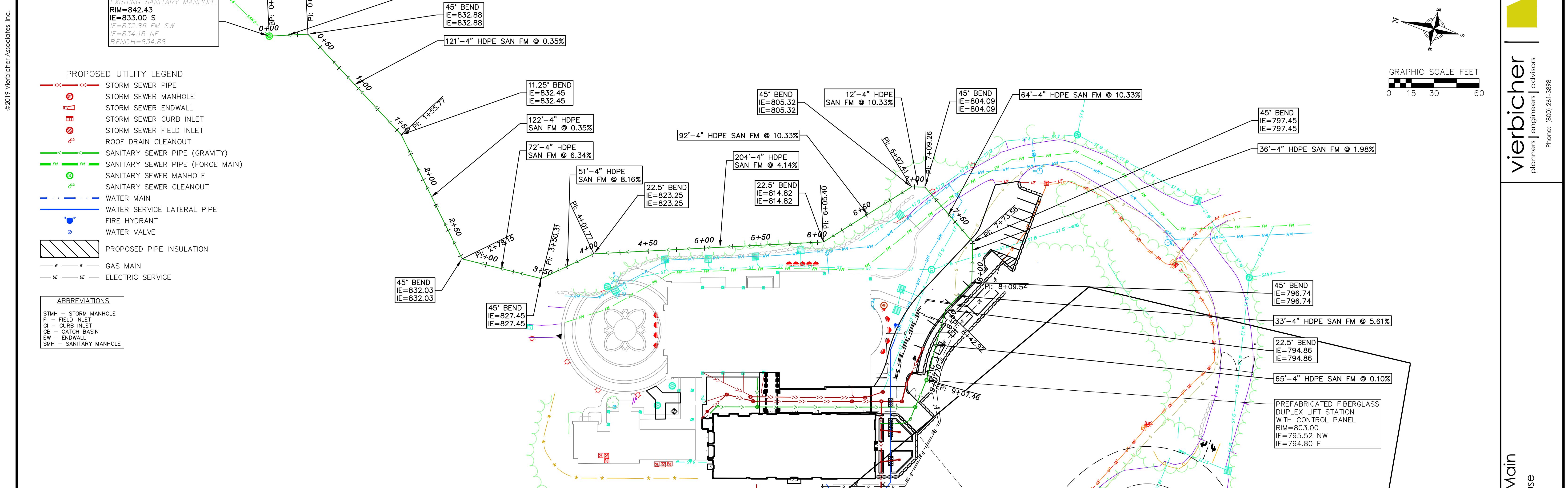
| LAND TYPE | AREA (SQ. FT.) |
|-------------|----------------|
| DISTURBED | 3605 |
| UNDISTURBED | 21228 |
| TOTAL | 24833 |











GENERAL NOTES:

- THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGE CAUSED DURING CONSTRUCTION TO PUBLIC PROPERTY, PRIVATE PROPERTY OR UTILITIES.
- THE CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR REVIEW BY THE ENGINEER, PRIOR TO PLACING AN ORDER OF ANY SUCH ITEM.
- EXISTING TOPOGRAPHIC INFORMATION IS BASED ON FIELD OBSERVATIONS AND/OR PLAN OF RECORD DRAWINGS. CONTRACTOR SHALL VERIFY TOPOGRAPHIC INFORMATION PRIOR TO STARTING CONSTRUCTION.
- PROPERTY LINES ARE APPROXIMATE. CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING EXISTING PROPERTY CORNER MONUMENTATION, ANY MONUMENTS DISTURBED BY CONTRACTOR SHALL BE REPLACED AT THE CONTRACTORS EXPENSE.
- CONTRACTOR SHALL COORDINATE WITH DRY UTILITY COMPANYS REGARDING ANY POTENTIAL CONFLICTS AND COORDINATE RELOCATIONS AS MAY BE REQUIRED. CONTRACTOR SHALL ALSO COORDINATE THE PROPOSED INSTALLATION OF NEW FACILITIES AS REQUIRED.

DEMOLITION NOTES:

- CONTRACTOR SHALL KEEP ALL PUBLIC ROADWAYS FREE AND CLEAR OF CONSTRUCTION RELATED DIRT/DUST/DEBRIS.
- COORDINATE EXISTING UTILITY REMOVAL/ABANDONMENT WITH LOCAL AUTHORITIES AND UTILITY COMPANIES HAVING JURISDICTION.
- ALL SAWCUTTING SHALL BE FULL DEPTH TO PROVIDE A CLEAN EDGE TO MATCH NEW CONSTRUCTION. MATCH EXISTING ELEVATIONS AT POINTS OF CONNECTION FOR NEW AND EXISTING PAVEMENT, CURB, SIDEWALKS, ETC. ALL SAWCUT LOCATIONS SHOWN ARE APPROXIMATE AND MAY BE FIELD ADJUSTED TO ACCOMMODATE CONDITIONS, JOINTS, MATERIAL TYPE, ETC. REMOVE MINIMUM AMOUNT NECESSARY FOR INSTALLATION OF PROPOSED IMPROVEMENTS.
- CONTRACTOR SHALL PROVIDE AND SHALL BE RESPONSIBLE FOR ANY NECESSARY TRAFFIC CONTROL SIGNAGE AND SAFETY MEASURES DURING DEMOLITION AND CONSTRUCTION OPERATIONS WITHIN OR NEAR THE PUBLIC ROADWAY.
- COORDINATE TREE REMOVAL WITH LANDSCAPE ARCHITECT. ALL TREES TO BE REMOVED SHALL BE REMOVED IN THEIR ENTIRETY AND STUMPS SHALL BE GROUND TO 12" BELOW PROPOSED SUBGRADE.
- IF APPLICABLE, PROVIDE TREE PROTECTION FENCING PRIOR TO CONSTRUCTION OPERATIONS. MAINTAIN THROUGHOUT CONSTRUCTION.
- ALL LIGHT POLES TO BE REMOVED FROM PRIVATE PROPERTY SHALL BE REMOVED IN THEIR ENTIRETY, INCLUDING BASE AND ALL APPURTENANCES. COORDINATE ABANDONMENT OF ELECTRICAL LINES WITH ELECTRICAL ENGINEER AND OWNER PRIOR TO DEMOLITION.
- CONTRACTOR SHALL OBTAIN ANY NECESSARY DEMOLITION AND UTILITY PLUGGING PERMITS.
- ANY DAMAGE TO THE CITY PAVEMENT, INCLUDING DAMAGE RESULTING FROM CURB REPLACEMENT, WILL REQUIRE RESTORATION IN ACCORDANCE WITH THE CITY ENGINEERING PATCHING CRITERIA.

SITE PLAN NOTES:

- CONCRETE TO BE 5" THICK, CONSTRUCTED ON A BASE OF 4" COMPAKTED SAND OR CRUSHED STONE.
- CONCRETE FOR DRIVEWAYS AND SIDEWALK AT DRIVEWAY ENTRANCES SHALL BE 7" THICK, CONSTRUCTED ON A BASE OF 5" COMPAKTED SAND OR CRUSHED STONE.
- ALL DIMENSIONS WITH CURB & GUTTER ARE REFERENCED TO THE FACE OF CURB.
- CONTRACTOR SHALL DEEP TILL ANY DISTURBED AREAS AFTER CONSTRUCTION IS COMPLETE AND BEFORE RESTORING.
- CONTRACTOR TO OBTAIN ANY NECESSARY DRIVEWAY CONNECTION, RIGHT OF WAY AND EXCAVATION PERMITS PRIOR TO CONSTRUCTION.
- ALL ABANDONED DRIVEWAYS ADJACENT TO THE SITE SHALL BE REPLACED WITH CURB AND THE TERRACE SHALL BE RESTORED WITH GRASS.
- ANY SIDEWALK AND CURB & GUTTER ABUTTING THE PROPERTY SHALL BE REPLACED IF IT IS DAMAGED DURING CONSTRUCTION OR IF THE CITY OF LA CROSSE ENGINEERING DEPARTMENT DETERMINES THAT IT IS NOT AT A DESIRABLE GRADE, REGARDLESS OF WHETHER THE CONDITION EXISTED PRIOR TO BEGINNING CONSTRUCTION.

GRADING NOTES:

- CONTOURS ARE SHOWN FOR PURPOSES OF INDICATING ROUGH GRADING. FINAL GRADE SHALL BE ESTABLISHED ON PAVED SURFACES BY USING SPOT GRADES ONLY.
- ALL GRADES SHOWN REFERENCE FINISHED ELEVATIONS.
- CROSS SLOPE OF SIDEWALKS SHALL BE 1.5% UNLESS OTHERWISE NOTED.
- ACCESSIBLE ROUTES SHALL BE 5.0% MAX LONGITUDINAL SLOPE AND 1.5% MAX CROSS SLOPE. ACCESSIBLE LOADING AREAS OR LANDINGS SHALL BE 2.0% MAX SLOPE IN ANY DIRECTION. RAMPS SHALL BE 8.33% MAX SLOPE.
- NO LAND DISTURBANCE ACTIVITIES SHALL BEGIN UNTIL ALL EROSION CONTROL BMP'S ARE INSTALLED.
- SEE DETAIL SHEETS FOR EROSION CONTROL NOTES AND CONSTRUCTION SEQUENCE.

UTILITY NOTES:

- CONTRACTOR SHALL OBTAIN ANY NECESSARY WORK IN RIGHT OF WAY, EXCAVATION, UTILITY CONNECTION, PLUGGING AND ABANDONMENT PERMITS PRIOR TO CONSTRUCTION.
- CONTRACTOR TO VERIFY EXISTING UTILITY LOCATIONS AND ELEVATIONS PRIOR TO STARTING WORK.
- SANITARY & STORM SEWER LENGTHS SHOWN ARE FROM CENTER OF STRUCTURE TO CENTER OF STRUCTURE. STORM SEWER END SECTIONS ARE INCLUDED IN THE LENGTH AND SLOPE OF THE PIPE.
- CONTRACTOR SHALL INVESTIGATE ALL UTILITY CROSSINGS PRIOR TO CONSTRUCTION AND NOTIFY ENGINEER OF ANY CONFLICTS.
- CONTRACTOR SHALL BE RESPONSIBLE FOR ADJUSTING ALL UTILITY STRUCTURES TO FINISHED GRADE (MANHOLE RIMS, WATER VALVES, AND CURB STOPS), IF NECESSARY.
- IF DEWATERING OPERATIONS EXCEED 70 GALLONS PER MINUTE OF PUMPING CAPACITY, A DEWATERING WELL PERMIT SHALL BE OBTAINED PRIOR TO STARTING ANY DEWATERING ACTIVITIES.
- A COPY OF THE APPROVED UTILITY PLANS, SPECIFICATIONS AND PLUMBING PERMIT APPROVAL LETTER SHALL BE ON-SITE DURING CONSTRUCTION AND OPEN TO INSPECTION BY AUTHORIZED REPRESENTATIVES OF THE DEPARTMENT OF SAFETY AND PROFESSIONAL SERVICES AND OTHER LOCAL INSPECTORS.
- PROPOSED UTILITY SERVICE LINES SHOWN ARE APPROXIMATE. COORDINATE THE EXACT LOCATIONS WITH THE PLUMBING DRAWINGS. COORDINATE THE LOCATION WITH THE PLUMBING CONTRACTOR AND/OR OWNER'S CONSTRUCTION REPRESENTATIVE PRIOR TO INSTALLATION OF ANY NEW UTILITIES.
- STORM BUILDING SEWER PIPE SHALL CONFORM TO ONE OF THE STANDARDS LISTED IN TABLE 384.30-6 OF SPS 384.30(3)(c).
- UNDERGROUND DRAIN AND VENT PIPE/TUBING SHALL CONFORM TO ONE OF THE STANDARDS LISTED IN TABLE 384.30-2 OF SPS 384.30(2).
- PRIVATE WATER SERVICES AND PRIVATE WATER MAINS SHALL CONFORM TO ONE OF THE STANDARDS LISTED IN TABLE 384.30-7 OF SPS 384.30(4)(d).
- PRIVATE SANITARY SEWER AND LATERALS SHALL BE POLYVINYL CHLORIDE (PVC) ASTM D3034 – SDR 35 OR APPROVED EQUAL MATERIAL THAT CONFORMS TO ONE OF THE STANDARDS LISTED IN TABLE 384.30-3 OF SPS 384.30(2)(c).
- A MEANS TO LOCATE BURIED UNDERGROUND EXTERIOR NON METALLIC SEWERS/MAINS AND WATER SERVICES/MAINS MUST BE PROVIDED WITH TRACER WIRE OR OTHER METHODS IN ORDER TO BE LOCATED PER SPS 382.10(11)(h) AND SPS 382.40(8)(k).
- EXTERIOR WATER SUPPLY PIPING SETBACKS AND CROSSINGS SHALL BE IN ACCORDANCE WITH SPS 382.40(8)(b).
- NO PERSON MAY ENGAGE IN PLUMBING WORK IN THE STATE UNLESS LICENSED TO DO SO BY THE DEPARTMENT OF SAFETY AND PROFESSIONAL SERVICES PER S.145.06.
- SITE CONTRACTOR SHALL LEAVE SANITARY AND WATER LATERALS FIVE (5) FEET SHORT (HORIZONTALLY) FROM THE BUILDING. BUILDING PLUMBER SHALL VERIFY SIZE, LOCATION, AND INVERT ELEVATION OF PROPOSED SANITARY AND WATER LATERALS.
- IT IS THE CONTRACTOR'S RESPONSIBILITY TO VERIFY THAT THE EXISTING VALVES WILL HOLD THE PRESSURE TEST PRIOR TO CONNECTION. THE CITY IS NOT RESPONSIBLE FOR ANY COSTS INCURRED DUE TO THE CONTRACTOR NOT VERIFYING THAT THE EXISTING VALVE WILL HOLD THE PRESSURE TEST PRIOR TO CONNECTION. IF A NEW VALVE IS REQUIRED, THE APPLICANT WILL BE REQUIRED TO INSTALL ONE AT THEIR EXPENSE, AT THE POINT OF CONNECTION.
- CONTRACTOR TO CHLORINATE AND BACTERIA TEST BEFORE DOMESTIC SUPPLY PURPOSES
- CLEAN OUT ALL EXISTING AND PROPOSED STORM INLETS AND CATCH BASINS AT THE COMPLETION OF CONSTRUCTION.
- SANITARY SEWER MAIN AT BURY DEPTHS GREATER THAN 15' SHALL BE SDR 26. ALL OTHER SANITARY SEWER MAIN SHALL BE SDR 35.
- CONTRACTOR SHALL COORDINATE WITH DRY UTILITY COMPANY'S REGARDING ANY POTENTIAL CONFLICTS AND COORDINATE RELOCATIONS AS MAY BE REQUIRED. CONTRACTOR SHALL ALSO COORDINATE THE PROPOSED INSTALLATION OF NEW FACILITIES AS REQUIRED.
- ALL WATER MAIN AND SERVICES SHALL BE INSTALLED AT A MINIMUM DEPTH OF 6.5' FROM TOP OF FINISHED GRADE ELEVATION TO TOP OF MAIN. PROVIDE 1.5' CLEAR SEPARATION IF WATER CROSSES BELOW SEWER AND MINIMUM 0.5' IF WATER CROSSES ABOVE.
- SANITARY MANHOLES WITH SEWER MAIN CONNECTIONS GREATER THAN 2' ABOVE THE LOWEST INVERT SHALL BE CONSTRUCTED WITH AN EXTERNAL DROP. MANHOLES WITH SEWER LATERAL CONNECTIONS GREATER THAN 2' ABOVE THE LOWEST INVERT SHALL BE CONSTRUCTED WITH AN INTERNAL DROP.
- INSTALL 1 SHEET OF 4'x8'x4" HIGH DENSITY STYROFOAM INSULATION AT ALL LOCATIONS WHERE STORM SEWER CROSSES WATER MAIN OR WATER LATERALS.

EROSION CONTROL MEASURES

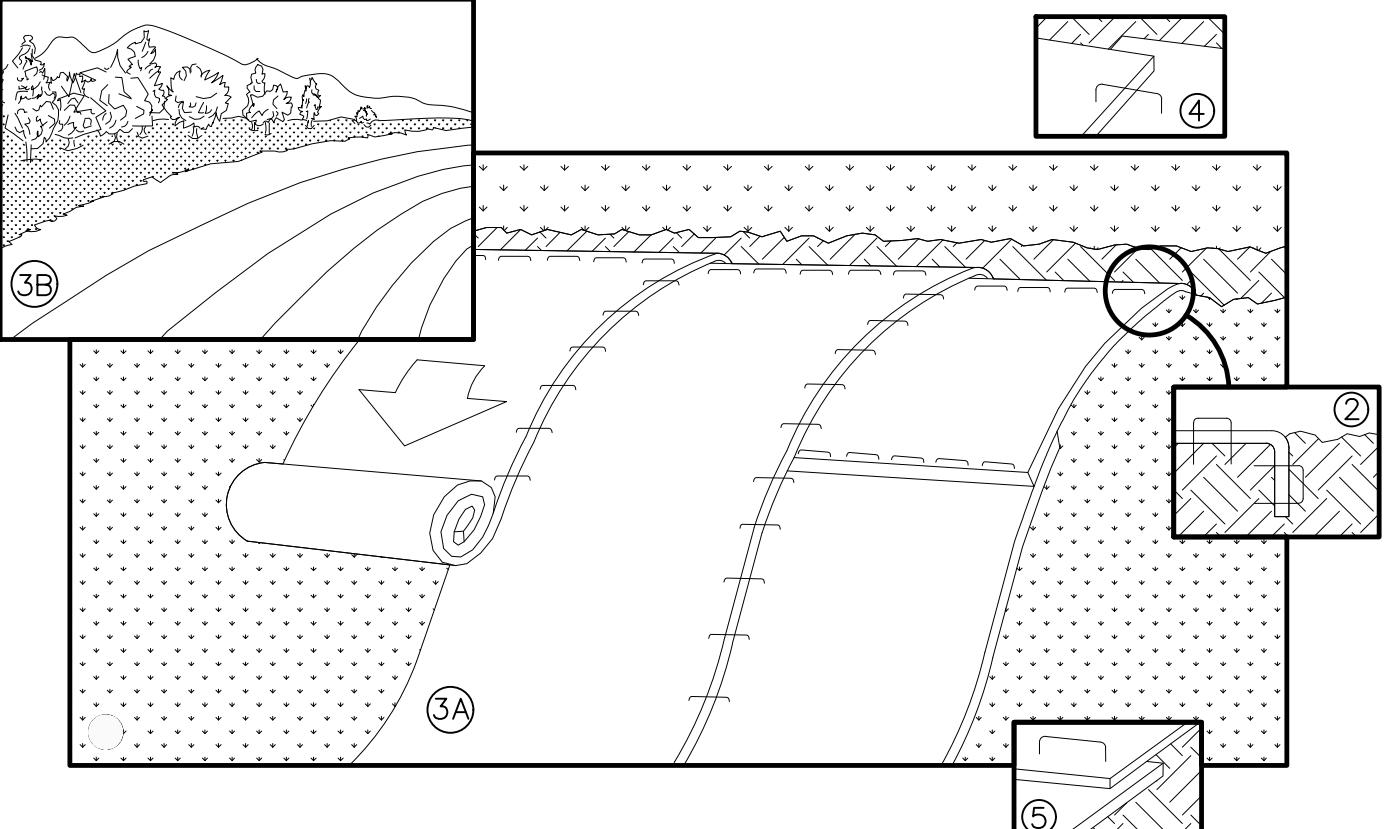
- EROSION CONTROL SHALL BE IN ACCORDANCE WITH THE CITY OF LA CROSSE EROSION CONTROL ORDINANCE AND CHAPTER NR 216 OF THE WISCONSIN ADMINISTRATIVE CODE.
- CONSTRUCT AND MAINTAIN ALL EROSION AND SEDIMENT CONTROL MEASURES IN ACCORDANCE WITH WISCONSIN DNR TECHNICAL STANDARDS AND WISCONSIN CONSTRUCTION SITE BEST MANAGEMENT PRACTICE HANDBOOK.
- INSTALL SEDIMENT CONTROL PRACTICES (TRACKING PAD, PERIMETER SILT FENCE, SEDIMENT BASINS, ETC.) PRIOR TO INITIATING OTHER LAND DISTURBING CONSTRUCTION ACTIVITIES.
- THE CONTRACTOR IS REQUIRED TO MAKE EROSION CONTROL INSPECTIONS AT THE END OF EACH WEEK AND WHEN 0.5 INCHES OF RAIN FALLS WITHIN 24 HOURS. INSPECTION REPORTS SHALL BE PREPARED AND FILED AS REQUIRED BY THE DNR AND/OR CITY. ALL MAINTENANCE WILL FOLLOW AN INSPECTION WITHIN 24 HOURS.
- EROSION CONTROL IS THE RESPONSIBILITY OF THE CONTRACTOR UNTIL ACCEPTANCE OF THIS PROJECT. EROSION CONTROL MEASURES AS SHOWN SHALL BE THE MINIMUM PRECAUTIONS THAT WILL BE ALLOWED. ADDITIONAL EROSION CONTROL MEASURES, AS REQUESTED IN WRITING BY THE STATE OR LOCAL INSPECTORS, OR THE DEVELOPER'S ENGINEER, SHALL BE INSTALLED WITHIN 24 HOURS.
- A 3" CLEAR STONE TRACKING PAD SHALL BE INSTALLED AT THE END OF ROAD CONSTRUCTION LIMITS TO PREVENT SEDIMENT FROM BEING TRACKED ONTO THE ADJACENT PAVED PUBLIC ROADWAY. SEDIMENT TRACKING PAD SHALL CONFORM TO WISDNR TECHNICAL STANDARD 1057. SEDIMENT REACHING THE PUBLIC ROAD SHALL BE REMOVED BY STREET CLEANING (NOT HYDRAULIC FLUSHING) BEFORE THE END OF EACH WORK DAY.
- CHANNELIZED RUNOFF: FROM ADJACENT AREAS PASSING THROUGH THE SITE SHALL BE DIVERTED AROUND DISTURBED AREAS.
- STABILIZED DISTURBED GROUND: ANY SOIL OR DIRT PILES WHICH WILL REMAIN IN EXISTENCE FOR MORE THAN 7 CONSECUTIVE DAYS, WHETHER TO BE WORKED DURING THAT PERIOD OR NOT, SHALL NOT BE LOCATED WITHIN 25 FEET OF ANY ROADWAY, PARKING LOT, PAVED AREA, OR DRAINAGE STRUCTURE OR CHANNEL (UNLESS INTENDED TO BE USED AS PART OF THE EROSION CONTROL MEASURES). TEMPORARY STABILIZATION AND CONTROL MEASURES (SEEDING, MULCHING, TARPING, EROSION MATTING, BARRIER FENCING, ETC.) ARE REQUIRED FOR THE PROTECTION OF DISTURBED AREAS AND SOIL PILES, WHICH WILL REMAIN UN-WORKED FOR A PERIOD OF MORE THAN 7 CONSECUTIVE CALENDAR DAYS. THESE MEASURES SHALL REMAIN IN PLACE UNTIL SITE HAS STABILIZED.
- SITE DE-WATERING: WATER PUMPED FROM THE SITE SHALL BE TREATED BY TEMPORARY SEDIMENTATION BASINS OR OTHER APPROPRIATE CONTROL MEASURES. SEDIMENTATION BASINS SHALL HAVE A DEPTH OF AT LEAST 3 FEET, BE SURROUNDED BY SNOWFENCE OR EQUIVALENT BARRIER AND HAVE SUFFICIENT SURFACE AREA TO PROVIDE A SURFACE SETTLING RATE OF NO MORE THAN 750 GALLONS PER SQUARE FOOT PER DAY AT THE HIGHEST DEWATERING PUMPING RATE. WATER MAY NOT BE DISCHARGED IN A MANNER THAT CAUSES EROSION OF THE SITE, A NEIGHBORING SITE, OR THE BED OR BANKS OF THE RECEIVING WATER. POLYMERS MAY BE USED AS DIRECTED BY DNR TECHNICAL STANDARD 1061 (DE-WATERING).
- SEE DETAIL SHEETS FOR RIP-RAP SIZING. RIP-RAP SHALL NOT BE SMALLER THAN 3" TO 6".
- INLET FILTERS ARE TO BE PLACED IN STORMWATER INLET STRUCTURES AS SOON AS THEY ARE INSTALLED. ALL PROJECT AREA STORM INLETS NEED WISCONSIN D.O.T. TYPE D INLET PROTECTION. THE FILTERS SHALL BE MAINTAINED UNTIL THE CITY HAS ACCEPTED THE BINDER COURSE OF ASPHALT.
- RESTORATION (SEED, FERTILIZE AND MULCH) SHALL BE PER SPECIFICATIONS ON THIS SHEET (NOTE: ADD SEEDING RATE STANDARD OF DETAIL BLOCK TO PLAN) UNLESS SPECIAL RESTORATION IS CALLED FOR ON THE LANDSCAPE PLAN OR THE DETENTION BASIN DETAIL SHEET.
- TERRACES SHALL BE RESTORED WITH 6" TOPSOIL, PERMANENT SEED, FERTILIZER AND MULCH. LOTS SHALL BE RESTORED WITH 6" TOPSOIL, TEMPORARY SEED, FERTILIZER AND MULCH.
- SEED, FERTILIZER AND MULCH SHALL BE APPLIED WITHIN 7 DAYS AFTER FINAL GRADE HAS BEEN ESTABLISHED. IF DISTURBED AREAS WILL NOT BE RESTORED IMMEDIATELY AFTER ROUGH GRADING, TEMPORARY SEED SHALL BE PLACED.
- FOR THE FIRST SIX WEEKS AFTER RESTORATION (E.G. SEED & MULCH, EROSION MAT, SOD) OF A DISTURBED AREA, INCLUDE SUMMER WATERING PROVISIONS OF ALL NEWLY SEDED AND MULCHED AREAS WHENEVER 7 DAYS ELAPSE WITHOUT A RAIN EVENT.
- SOIL STABILIZERS SHALL BE APPLIED TO DISTURBED AREAS WITH SLOPES BETWEEN 10% AND 3:1 (DO NOT USE IN CHANNELS). SOIL STABILIZERS SHALL BE TYPE B, PER WISCONSIN D.O.T. P.A.L. (PRODUCT ACCEPTABILITY LIST), OR EQUAL. APPLY AT RATES AND METHODS SPECIFIED PER MANUFACTURER. SOIL STABILIZERS SHALL BE RE-APPLIED WHENEVER VEHICLES OR OTHER EQUIPMENT TRACK ON THE AREA.
- SILT FENCE OR EROSION MAT SHALL BE INSTALLED ALONG THE CONTOURS AT 100 FOOT INTERVALS DOWN THE SLOPE ON THE DISTURBED SLOPES STEEPER THAN 5% AND MORE THAN 100 FEET LONG THAT SHEET FLOW TO THE ROADWAY UNLESS SOIL STABILIZERS ARE USED.
- SILT FENCE TO BE USED ACROSS AREAS OF THE LOT THAT SLOPE TOWARDS A PUBLIC STREET OR WATERWAY. SEE DETAILS.
- SEDIMENT SHALL BE CLEANED FROM CURB AND GUTTER AFTER EACH RAINFALL AND PRIOR TO PROJECT ACCEPTANCE.
- ACCUMULATED CONSTRUCTION SEDIMENT SHALL BE REMOVED FROM ALL PERMANENT BASINS TO THE ELEVATION SHOWN ON THE GRADING PLAN FOLLOWING THE STABILIZATION OF DRAINAGE AREAS.
- ALL CONSTRUCTION ENTRANCES SHALL HAVE TEMPORARY ROAD CLOSED SIGNS THAT WILL BE IN PLACE WHEN THE ENTRANCE IS NOT IN USE AND AT THE END OF EACH DAY.
- THE CITY, OWNER AND/OR ENGINEER MAY REQUIRE ADDITIONAL EROSION CONTROL MEASURES AT ANY TIME DURING CONSTRUCTION.

| Construction Notes | |
|------------------------------|--|
| St. Juan Diego Pilgrim House | |
| City of La Crosse | |
| La Crosse County, WI | |
| DATE 08/09/2024 | |
| DRAFTER CKNA/CSHE | |
| CHECKED JKAS | |
| PROJECT NO. 200196 | |
| C600 | |

CONSTRUCTION SEQUENCE:

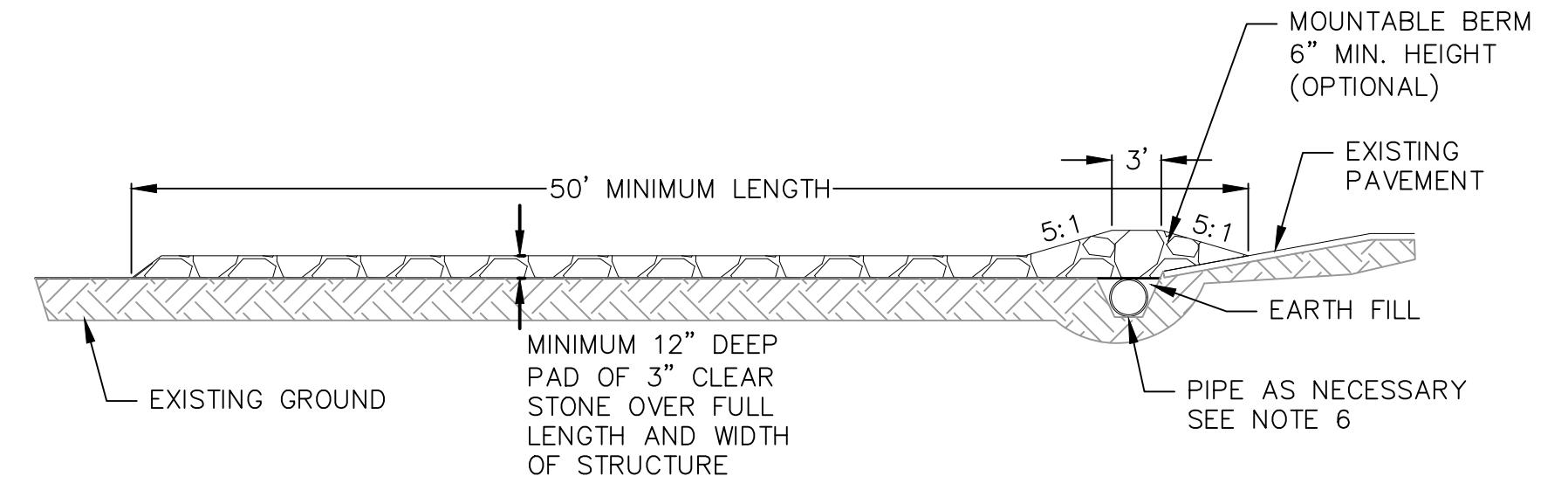
1. INSTALL EROSION CONTROL MEASURES
2. STRIP TOPSOIL
3. ROUGH GRADE
4. CONSTRUCT UNDERGROUND UTILITIES
5. INSTALL INLET PROTECTION
6. CONSTRUCT REMAINING IMPROVEMENTS
7. RESTORE DISTURBED AREAS
8. REMOVE EROSION CONTROL MEASURES
AFTER DISTURBED AREAS ARE RESTORED

SEEDING RATES:
TEMPORARY:
 1. USE ANNUAL OATS AT 3.0 LB./1,000 S.F. FOR SPRING AND SUMMER PLANTINGS.
 2. USE WINTER WHEAT OR RYE AT 3.0 LB./1,000 SF FOR FALL PLANTINGS STARTED AFTER SEPTEMBER 15.
PERMANENT:
 1. USE WISCONSIN D.O.T. SEED MIX #40 AT 2 LB./1,000 S.F.
FERTILIZING RATES:
TEMPORARY AND PERMANENT:
 USE WISCONSIN D.O.T. TYPE A OR B AT 7 LB./1,000 S.F.
MULCHING RATES:
TEMPORARY AND PERMANENT:
 USE $\frac{1}{2}$ " TO 1- $\frac{1}{2}$ " STRAW OR HAY MULCH, CRIMPED PER SECTION 607.3.2.3, OR OTHER RATE AND METHOD PER SECTION 627, WISCONSIN D.O.T. STANDARD SPECIFICATIONS FOR HIGHWAY AND STRUCTURE CONSTRUCTION

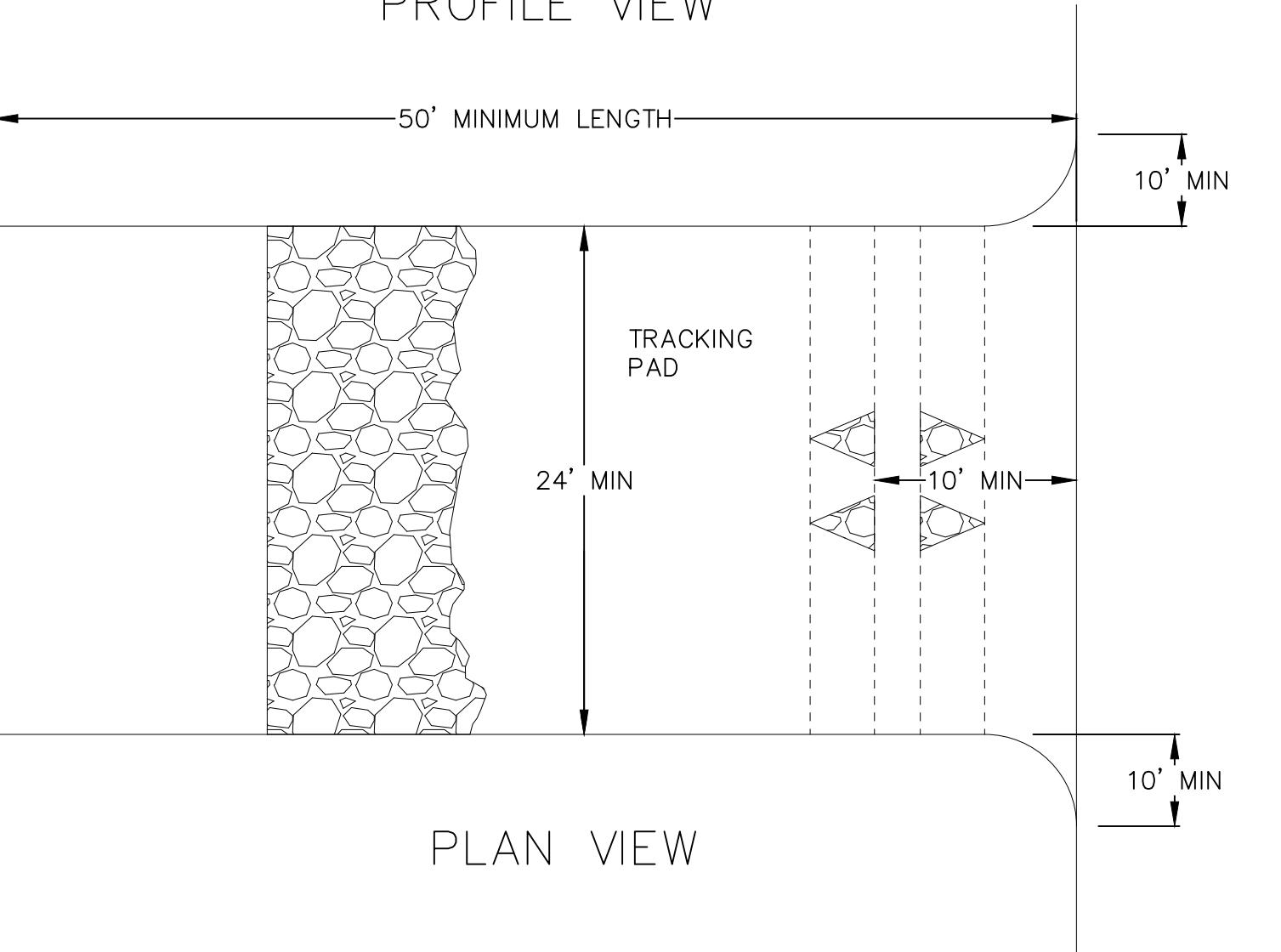


NOTE: REFER TO GENERAL STAPLE PATTERN GUIDE FOR CORRECT STAPLE PATTERN RECOMMENDATIONS FOR SLOPE INSTALLATIONS.

1. PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING APPLICATION OF FERTILIZER AND SEED.
NOTE: WHEN USING CELL-O-SEED, DO NOT SEED PREPARED AREA. CELL-O-SEED MUST BE INSTALLED WITH PAPER SIDE DOWN.
2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN 6" DEEP BY 6" WIDE TRENCH. BACKFILL AND COMPACT THE TRENCH AFTER STAPLING.
3. ROLL THE BLANKETS <A> DOWN, OR HORIZONTALLY ACROSS THE SLOPE.
4. THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2" OVERLAP.
5. WHEN BLANKETS MUST BE SPLICED DOWN THE SLOPE, PLACE BLANKETS END OVER END (SHINGLE STYLE) WITH APPROXIMATELY 4" OVERLAP. STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12" APART.
6. ALL BLANKETS MUST BE SECURELY FASTENED TO THE SLOPE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS RECOMMENDED BY THE MANUFACTURER.



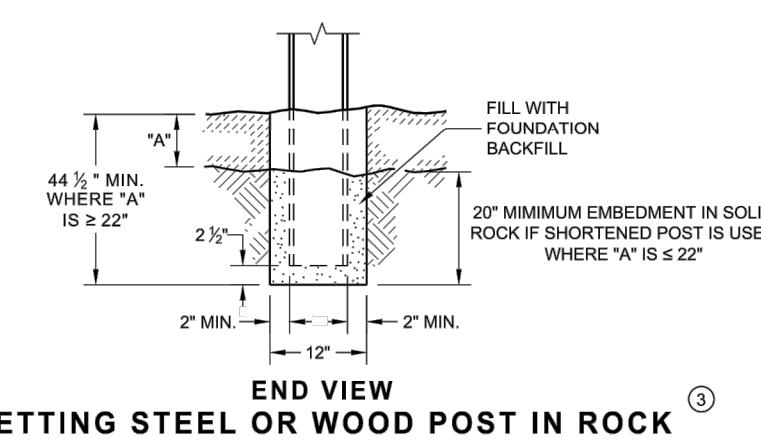
PROFILE VIEW



PLAN VIEW

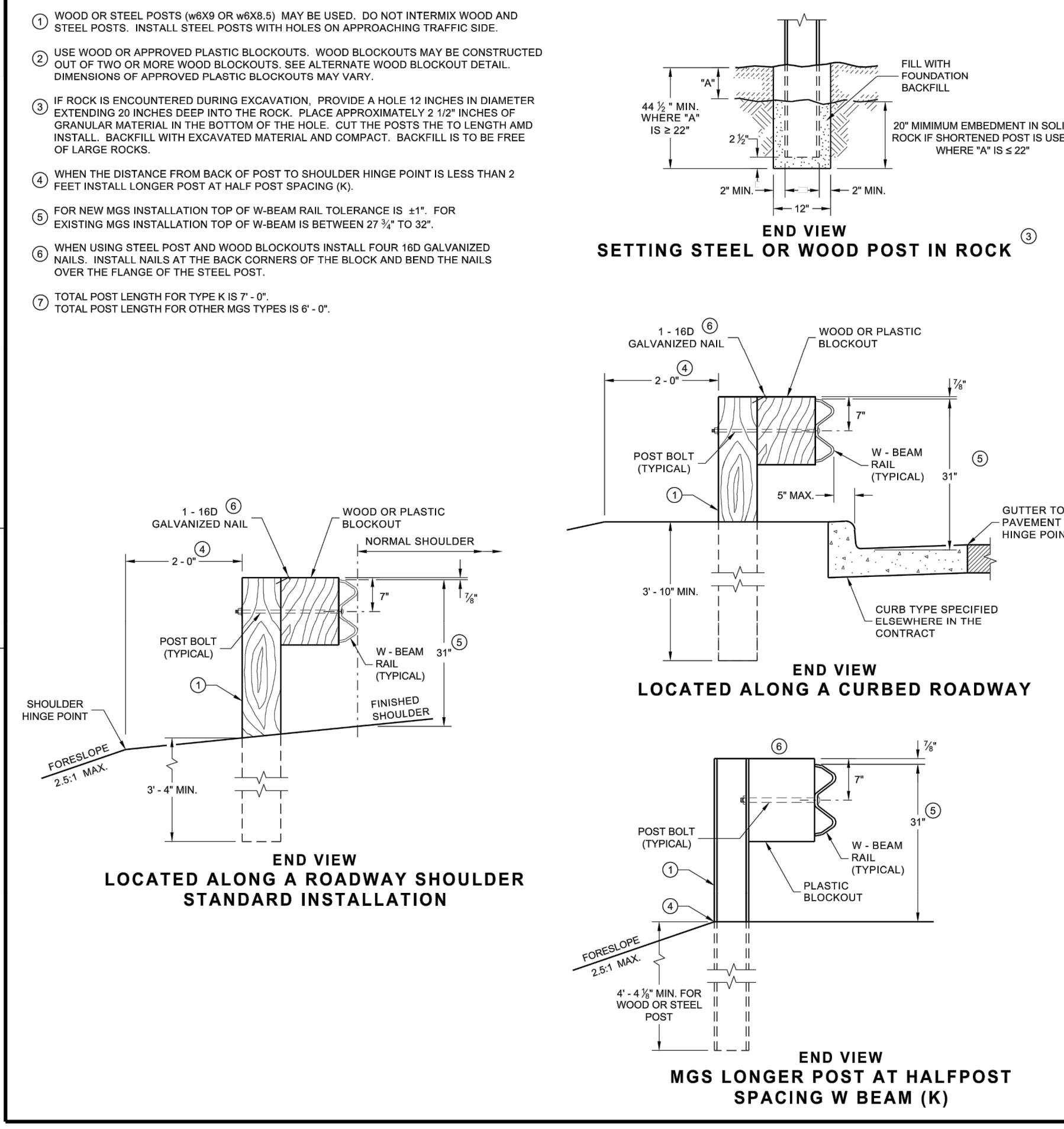
SDD 14B42-a Midwest Guardrail System (MGS) Guardrail

1. WOOD OR STEEL POSTS w6x9 or w8x8.5 MAY BE USED. DO NOT INTERMIX WOOD AND STEEL POSTS. INSTALL STEEL POSTS WITH HOLES ON APPROACHING TRAFFIC SIDE.
2. USE WOOD OR APPROVED PLASTIC BLOCKOUTS. WOOD BLOCKOUTS MAY BE CONSTRUCTED OUT OF TWO OR MORE WOOD BLOCKOUTS. SEE ALTERNATE WOOD BLOCKOUT DETAIL DIMENSIONS OF APPROVED PLASTIC BLOCKOUTS MAY VARY.
3. IF ROCK IS ENCOUNTERED DURING EXCAVATION, POST HOLE IS 12 INCHES IN DIAMETER EXTENDED 12 INCHES DEEP INTO THE ROCK. PLACE APPROXIMATELY 2 1/2 INCHES OF GRANULAR MATERIAL IN THE BOTTOM OF THE HOLE. CUT THE POSTS TO LENGTH AND INSTALL. BACKFILL WITH EXCAVATED MATERIAL AND COMPACT. BACKFILL IS TO BE FREE OF LARGE ROCKS.
4. WHEN THE DISTANCE FROM BACK OF POST TO SHOULDER HINGE POINT IS LESS THAN 2 FEET INSTALL LONGER POST AT HALF POST SPACING (K).
5. FOR NEW MGS INSTALLATION TOP OF W-BEAM RAIL TOLERANCE IS $\pm 1"$. FOR EXISTING MGS INSTALLATION TOP OF W-BEAM IS BETWEEN 27 1/2" TO 32".
6. WHEN USING A POST AND PLASTIC BLOCKOUTS INSTALL FOUR 16D GALVANIZED NAILS. INSTALL NAILS AT THE BACK CORNERS OF THE BLOCK AND BEND THE NAILS OVER THE FLANGE OF THE STEEL POST.
7. TOTAL POST LENGTH FOR TYPE K IS 7'-0".
TOTAL POST LENGTH FOR OTHER MGS TYPES IS 6'-0".

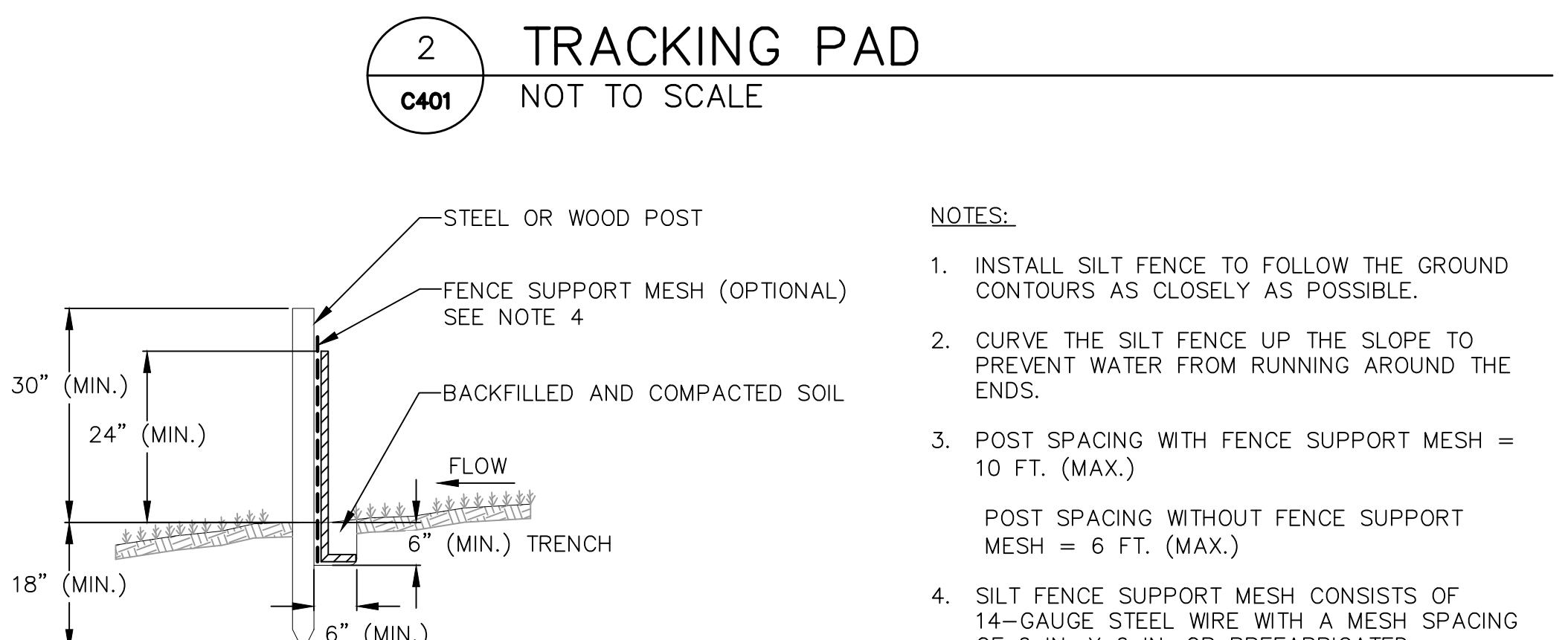


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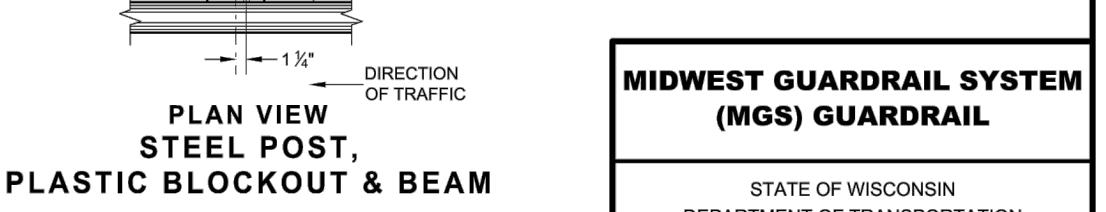
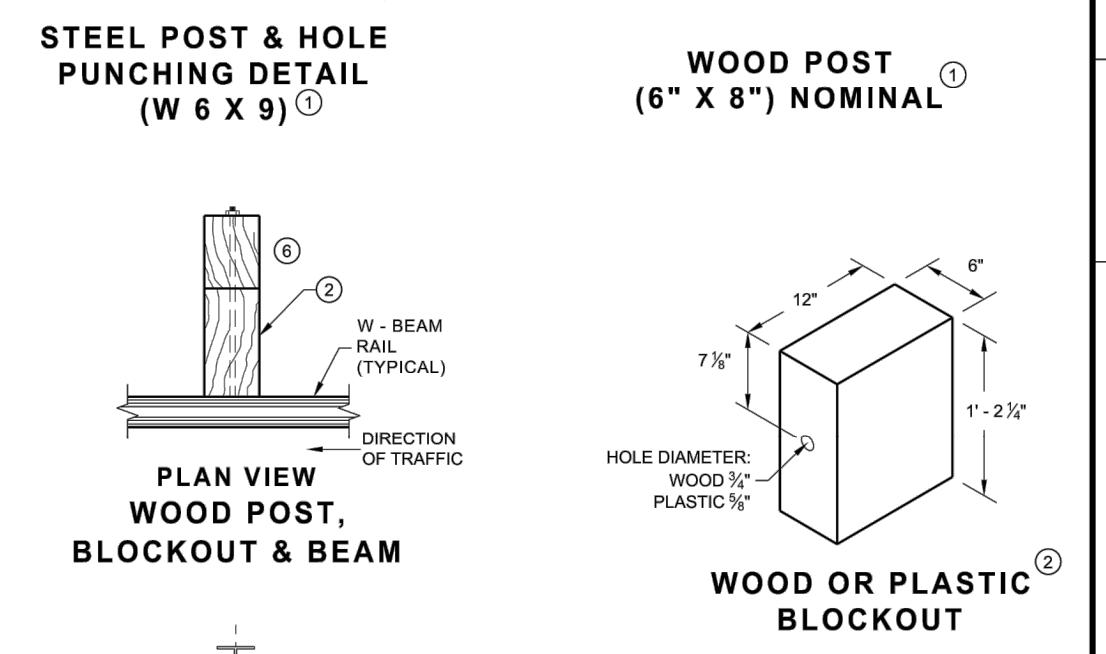
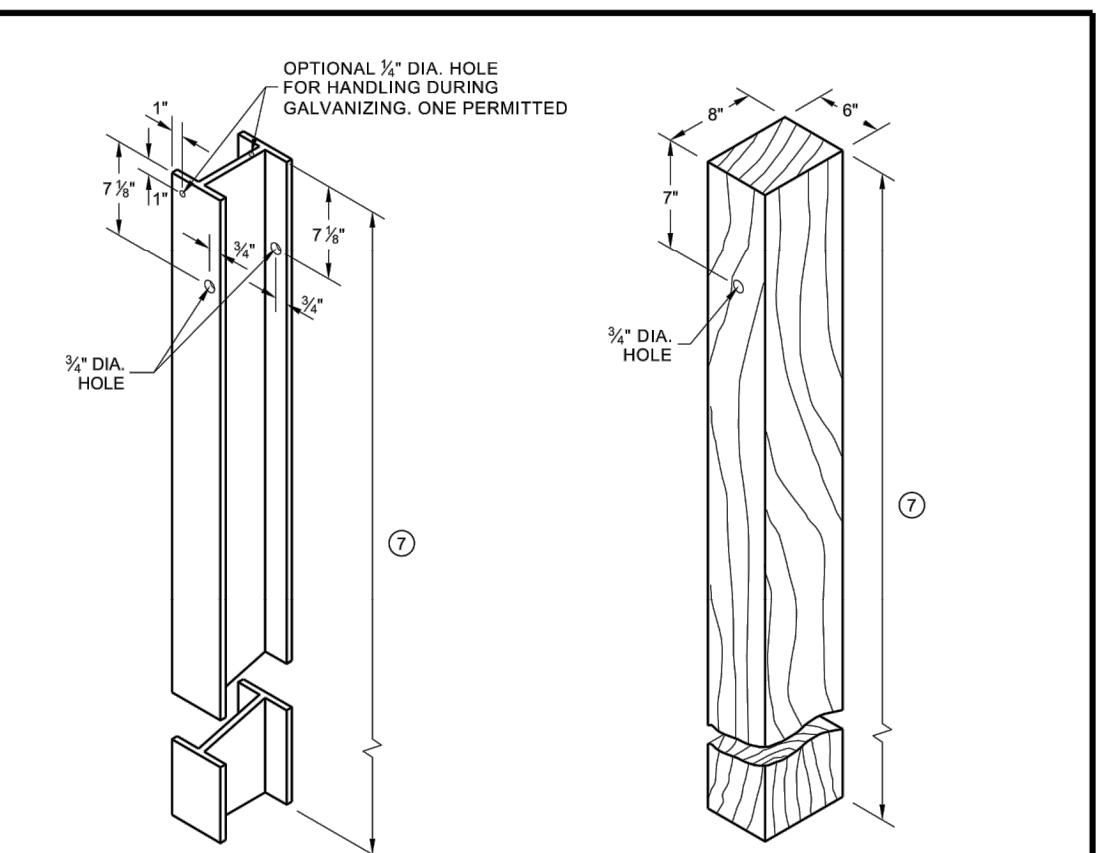
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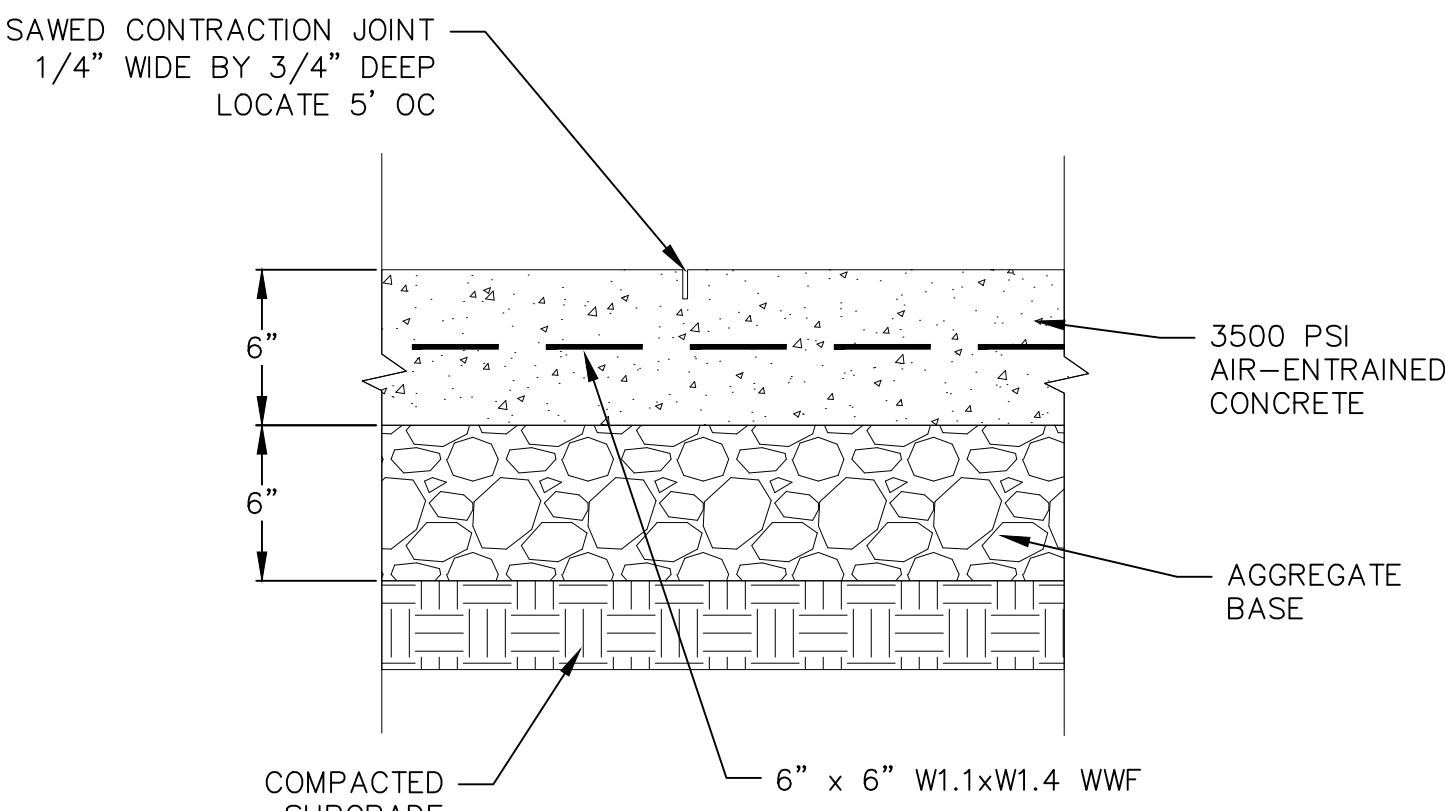
Construction Details
 St. Juan Diego Pilgrim House
 City of La Crosse
 La Crosse County, WI



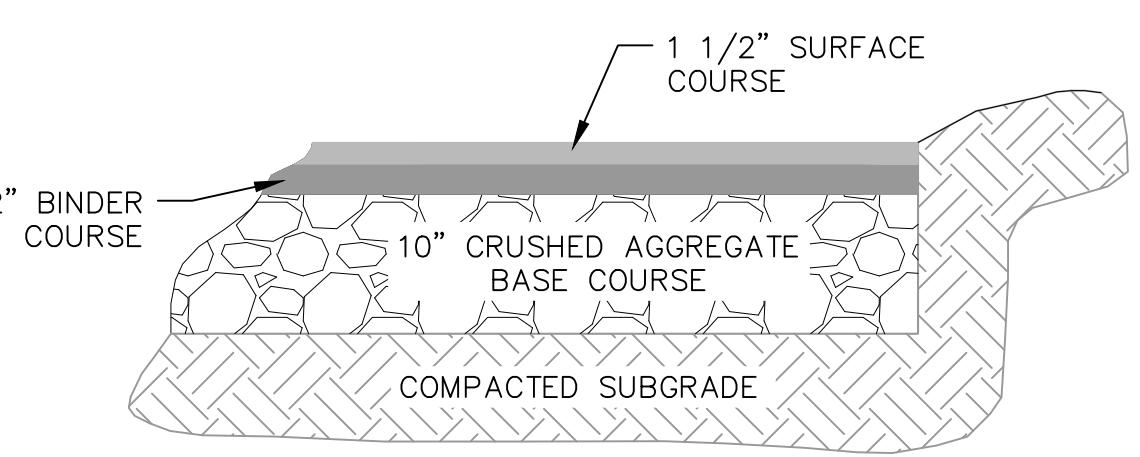
- NOTES:**
1. INSTALL SILT FENCE TO FOLLOW THE GROUND CONTOURS AS CLOSELY AS POSSIBLE.
 2. CURVE THE SILT FENCE UP THE SLOPE TO PREVENT WATER FROM RUNNING AROUND THE ENDS.
 3. POST SPACING WITH FENCE SUPPORT MESH = 10 FT. (MAX.)
POST SPACING WITHOUT FENCE SUPPORT MESH = 6 FT. (MAX.)
 4. SILT FENCE SUPPORT MESH CONSISTS OF 14-GAUGE STEEL WIRE WITH A MESH SPACING OF 6 IN. X 6 IN. OR PREFABRICATED POLYMERIC MESH OF EQUIVALENT STRENGTH



REVISIONS
 DATE 08/09/2024
 NO. DATE
 DRAFTER CKNA/CSHE
 CHECKED JKAS
 PROJECT NO. 200196



CONCRETE PAD

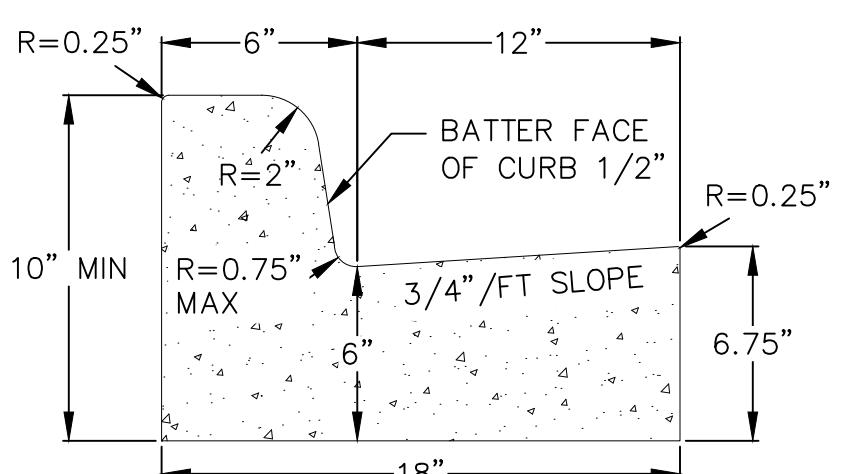


BITUMINOUS PAVEMENT



SITE PAVEMENT

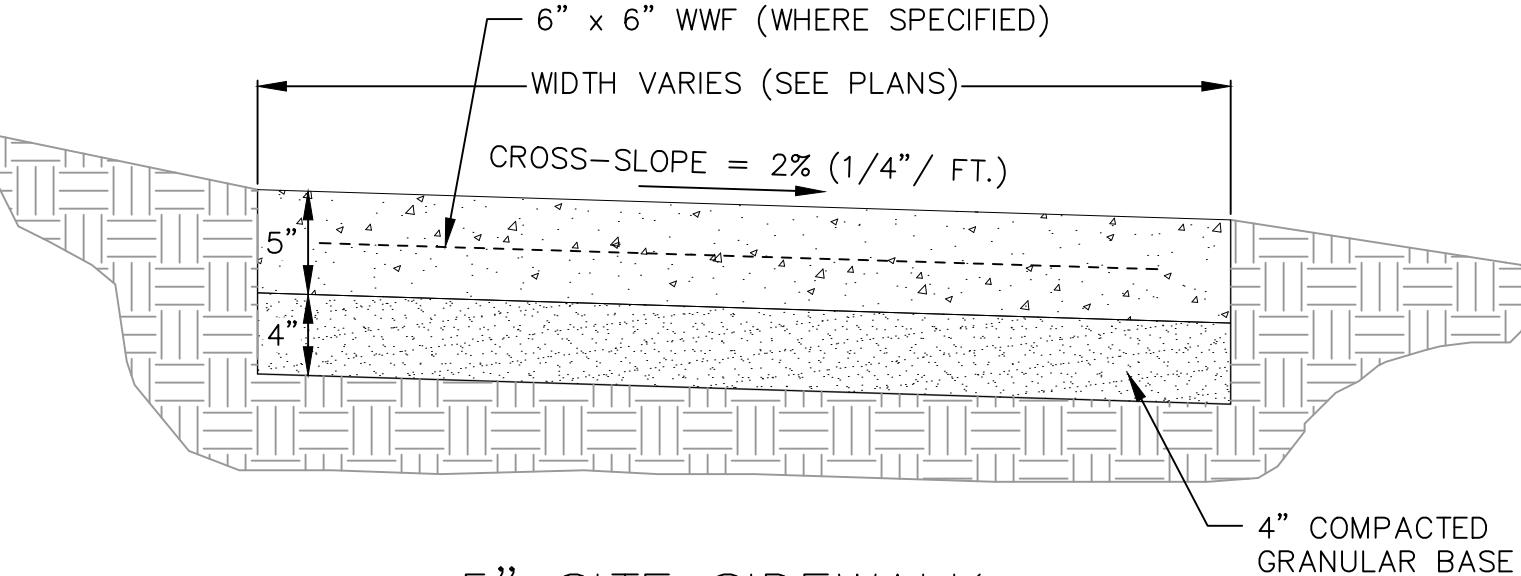
NOT TO SCALE



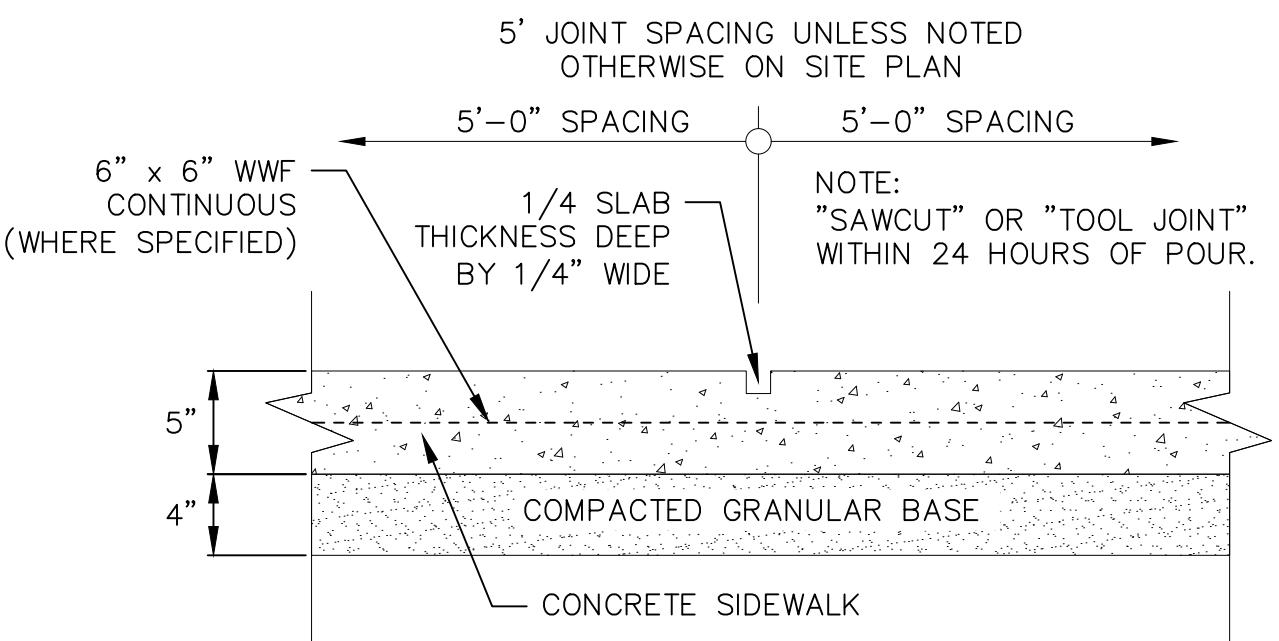
CURB AND GUTTER CROSS SECTION



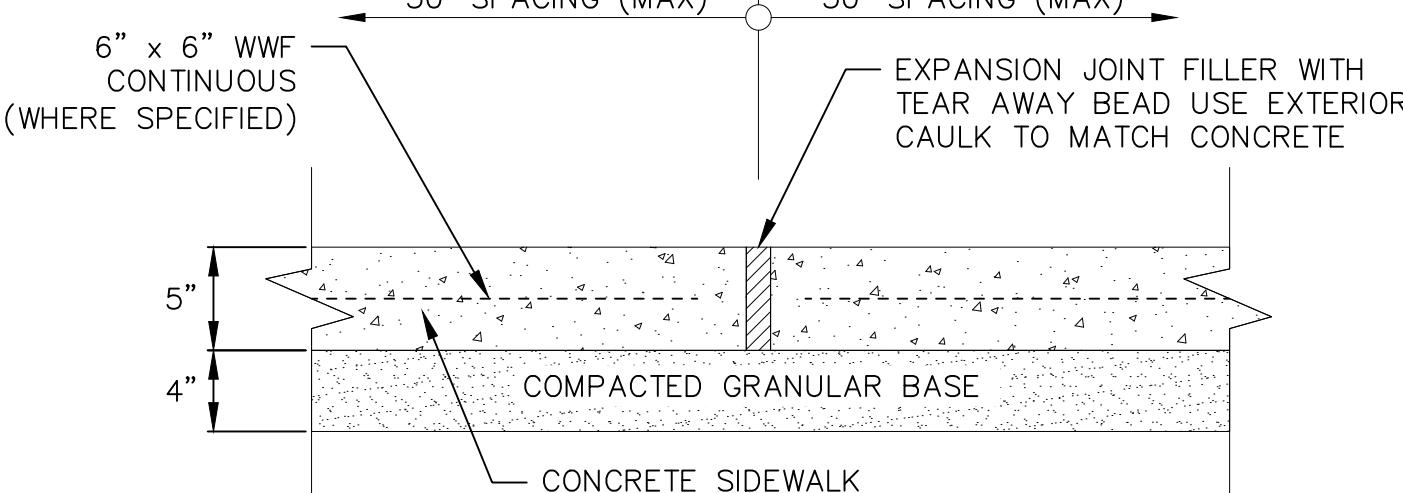
18" CONCRETE CURB AND GUTTER



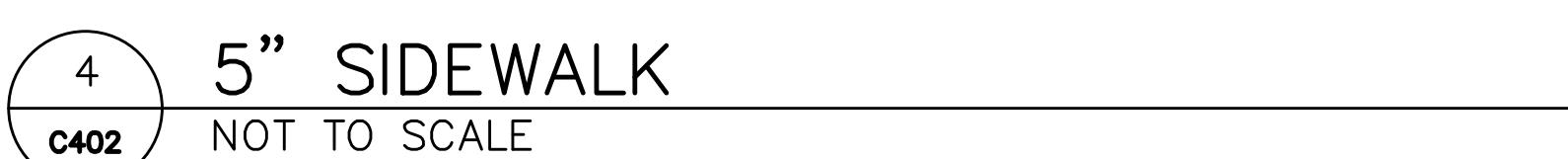
5" SITE SIDEWALK



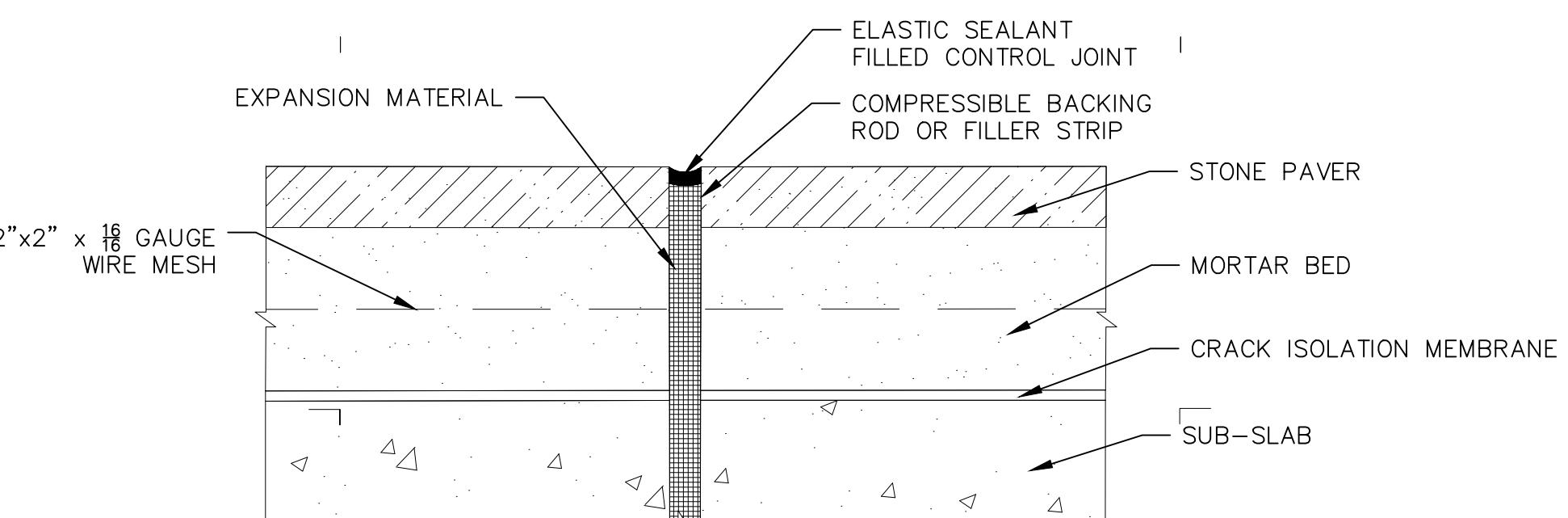
SIDEWALK CONTROL JOINT



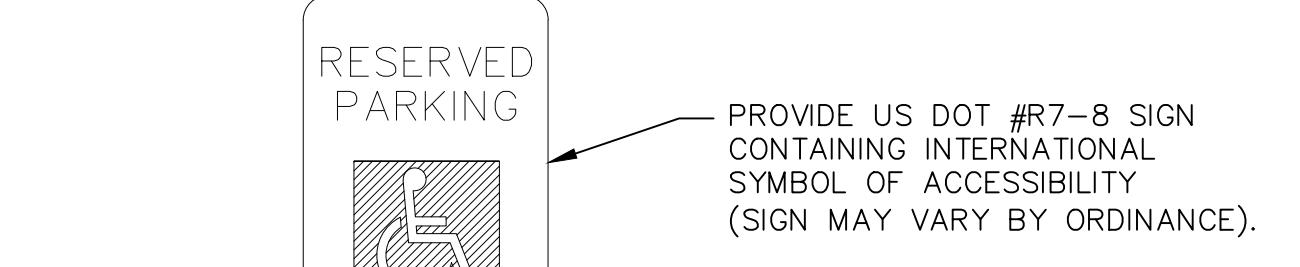
SIDEWALK EXPANSION JOINT



” SIDEWALK

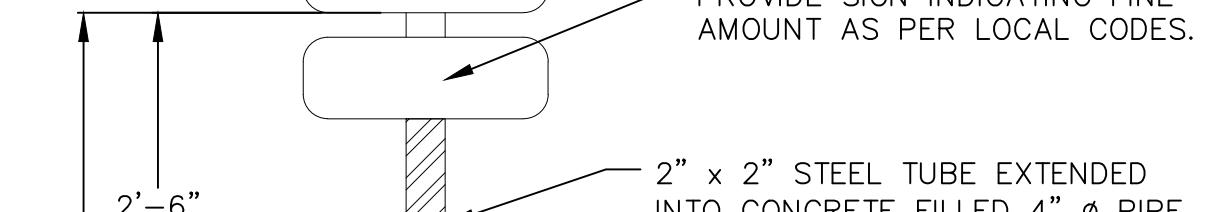


5 FULL MORTAR BED WITH MEMBRANE AND EXPANSION JOINT
C402 NOT TO SCALE



RESERVED
PARKING

PROVIDE US DOT #R7-8 SIGN
CONTAINING INTERNATIONAL
SYMBOL OF ACCESSIBILITY
(SIGN MAY VARY BY ORDINANCE).



INTO CONCRETE FIELD 4' x 10'

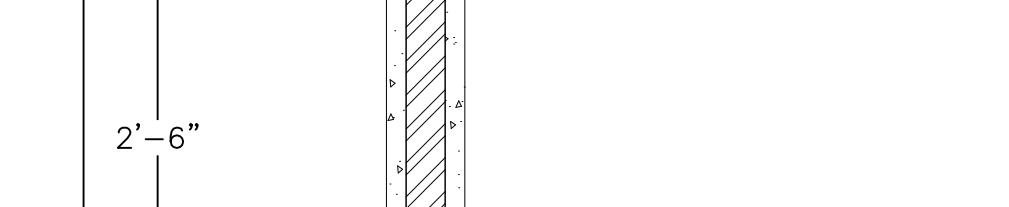
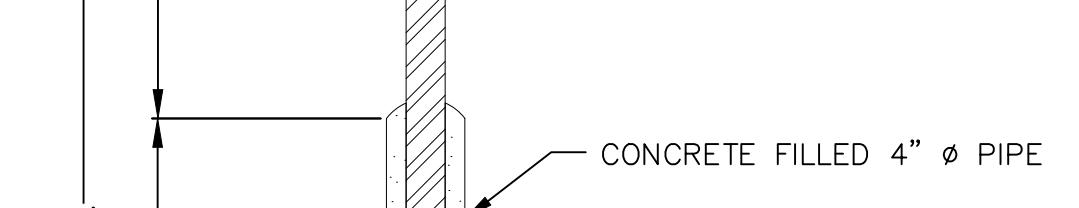
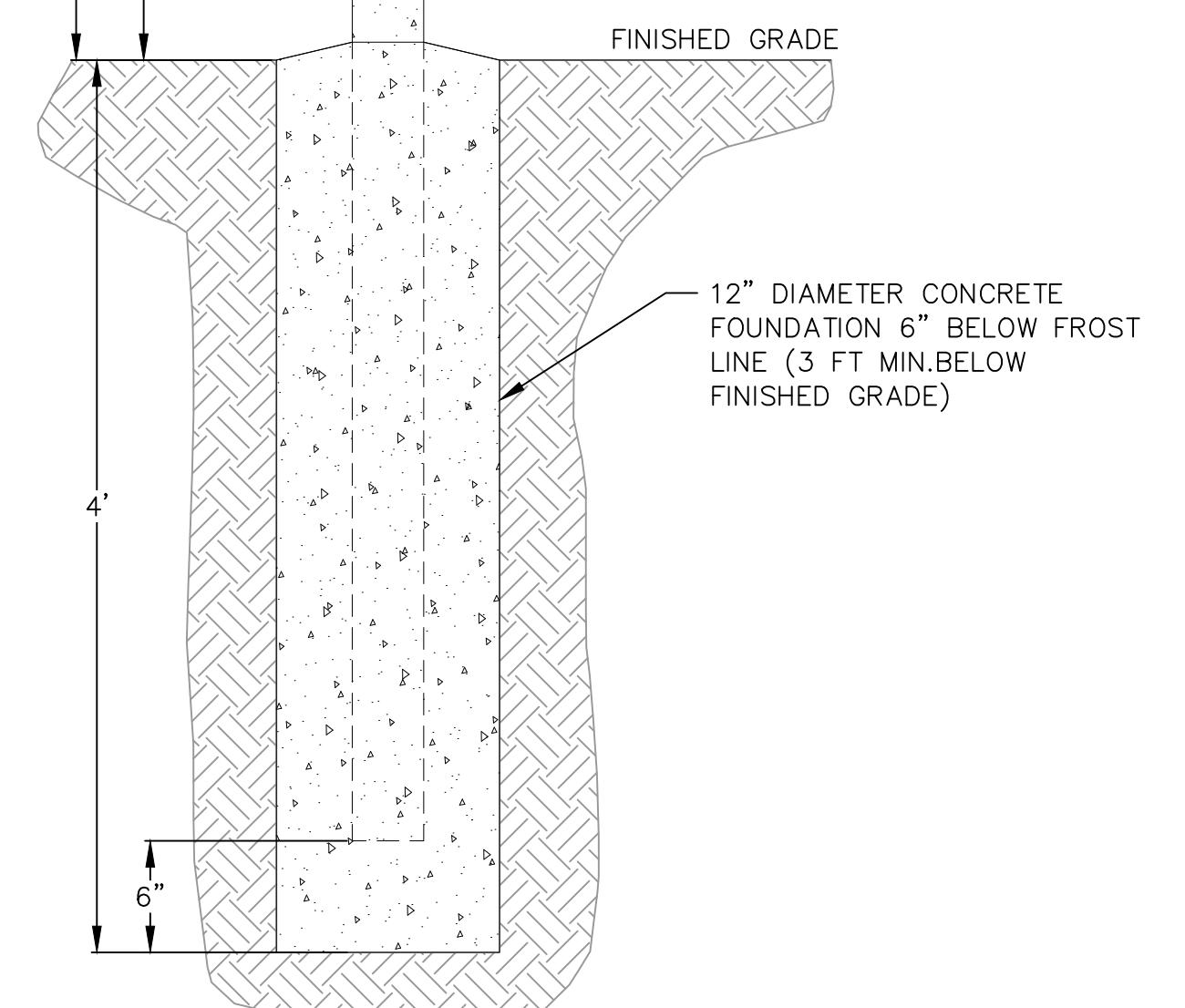
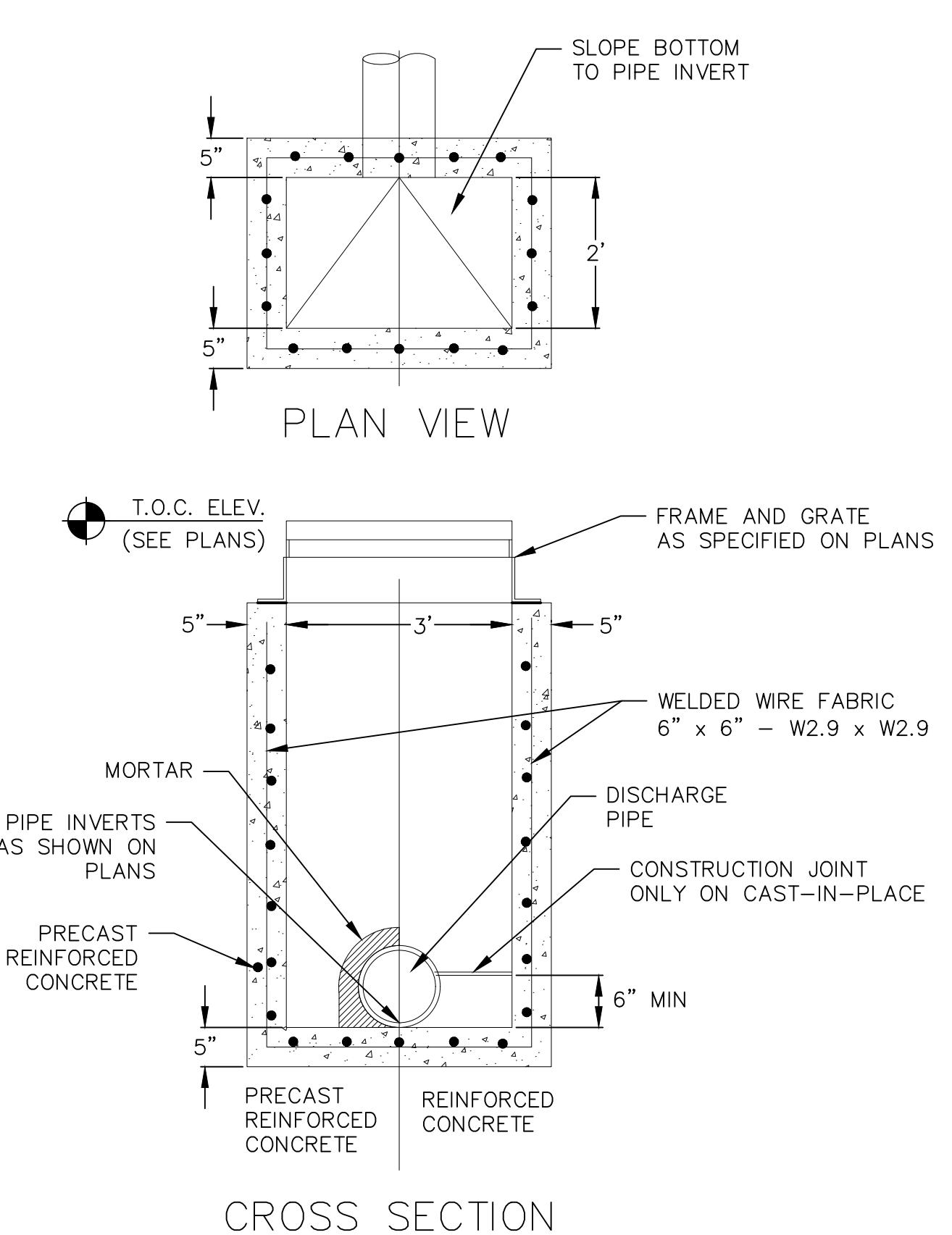
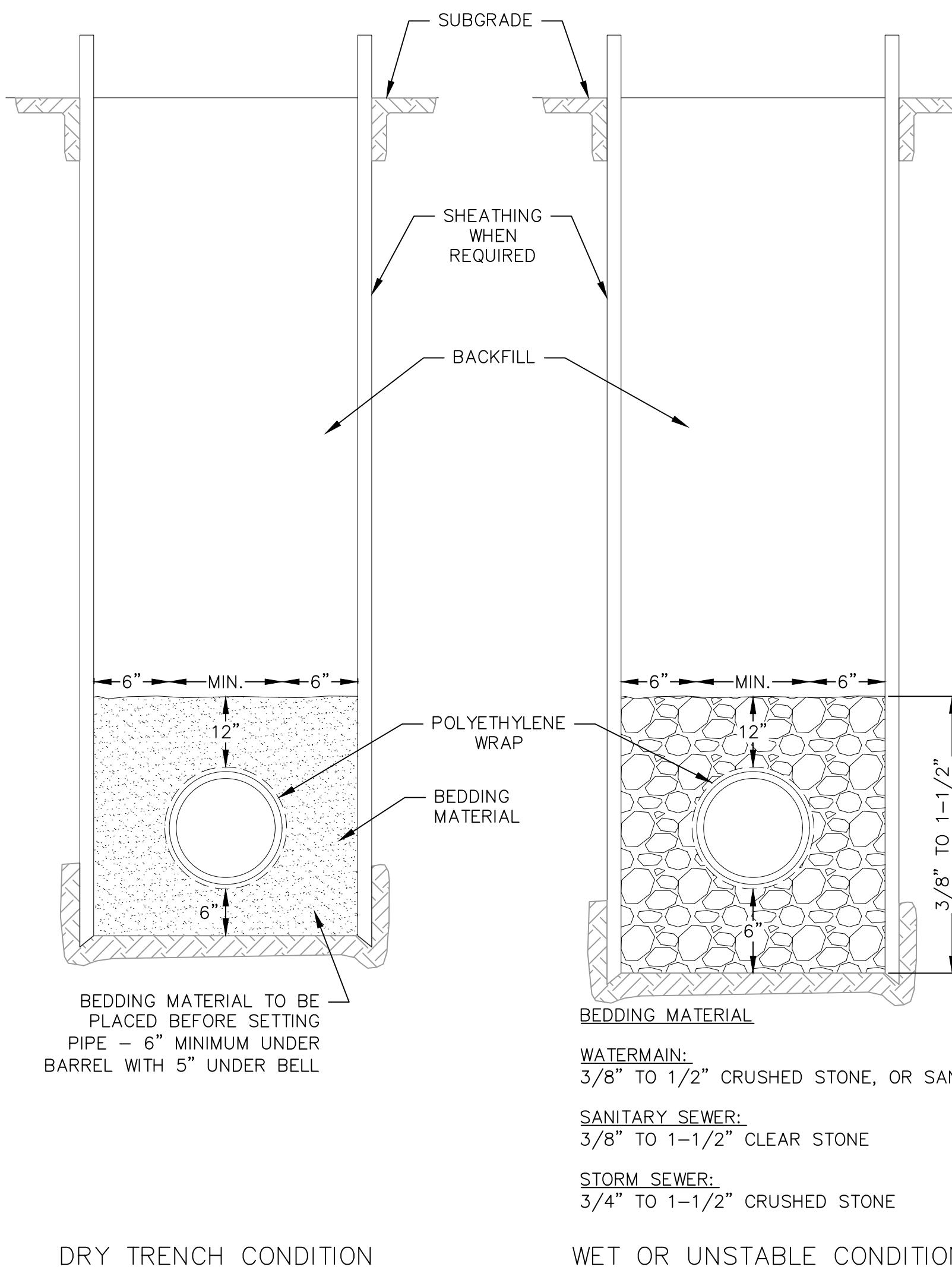
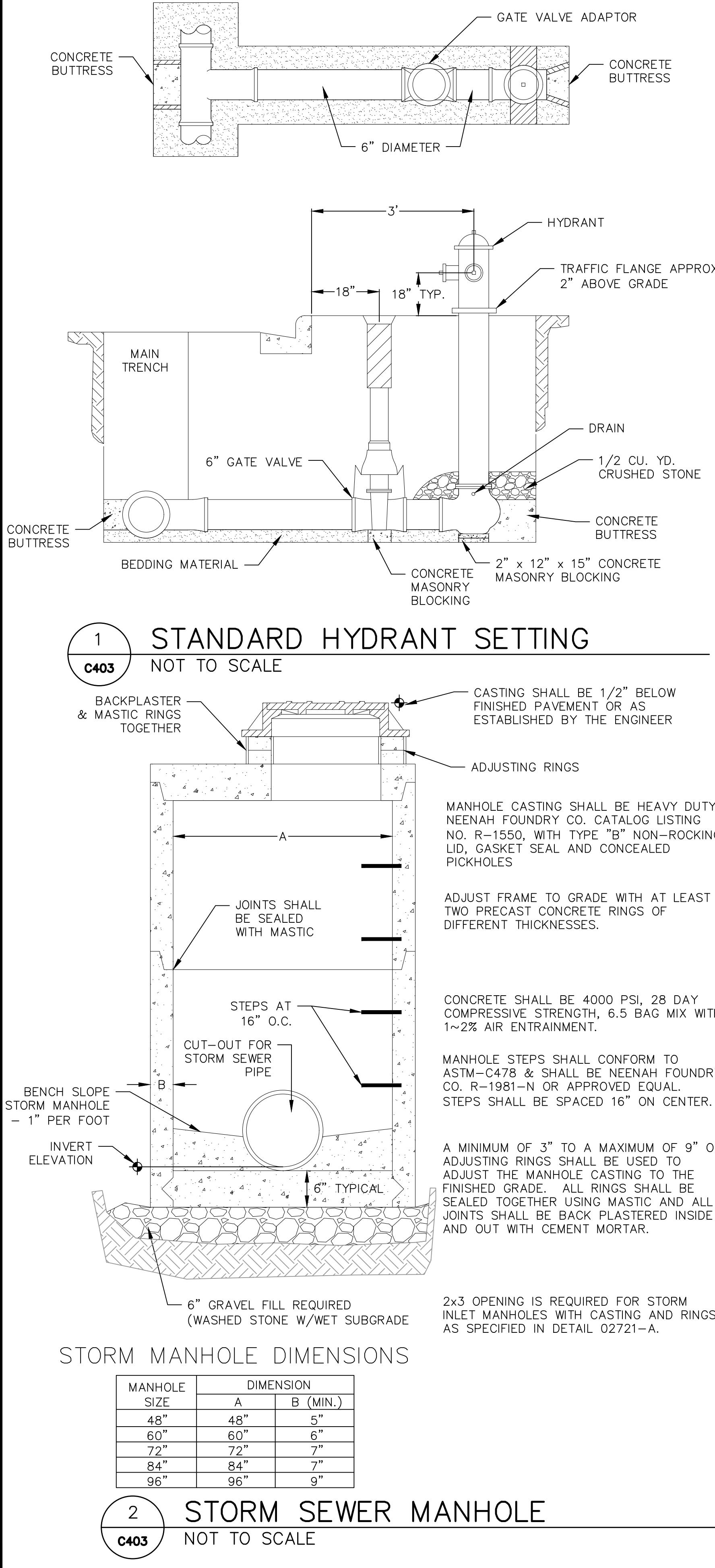


Figure 1. A schematic diagram of the experimental setup. The sample is a rectangular block of size $L_x \times L_y \times L_z$. The top surface is divided into two regions: a central region of size $L_x \times L_y$ and two side regions of size $(L_x - \Delta x) \times L_y$. The bottom surface is divided into two regions: a central region of size $L_x \times L_y$ and two side regions of size $(L_x - \Delta x) \times L_y$. The left boundary is a fixed boundary, while the right boundary is a free boundary. The top and bottom boundaries are periodic boundaries.



HANDICAP PARKING SIGN

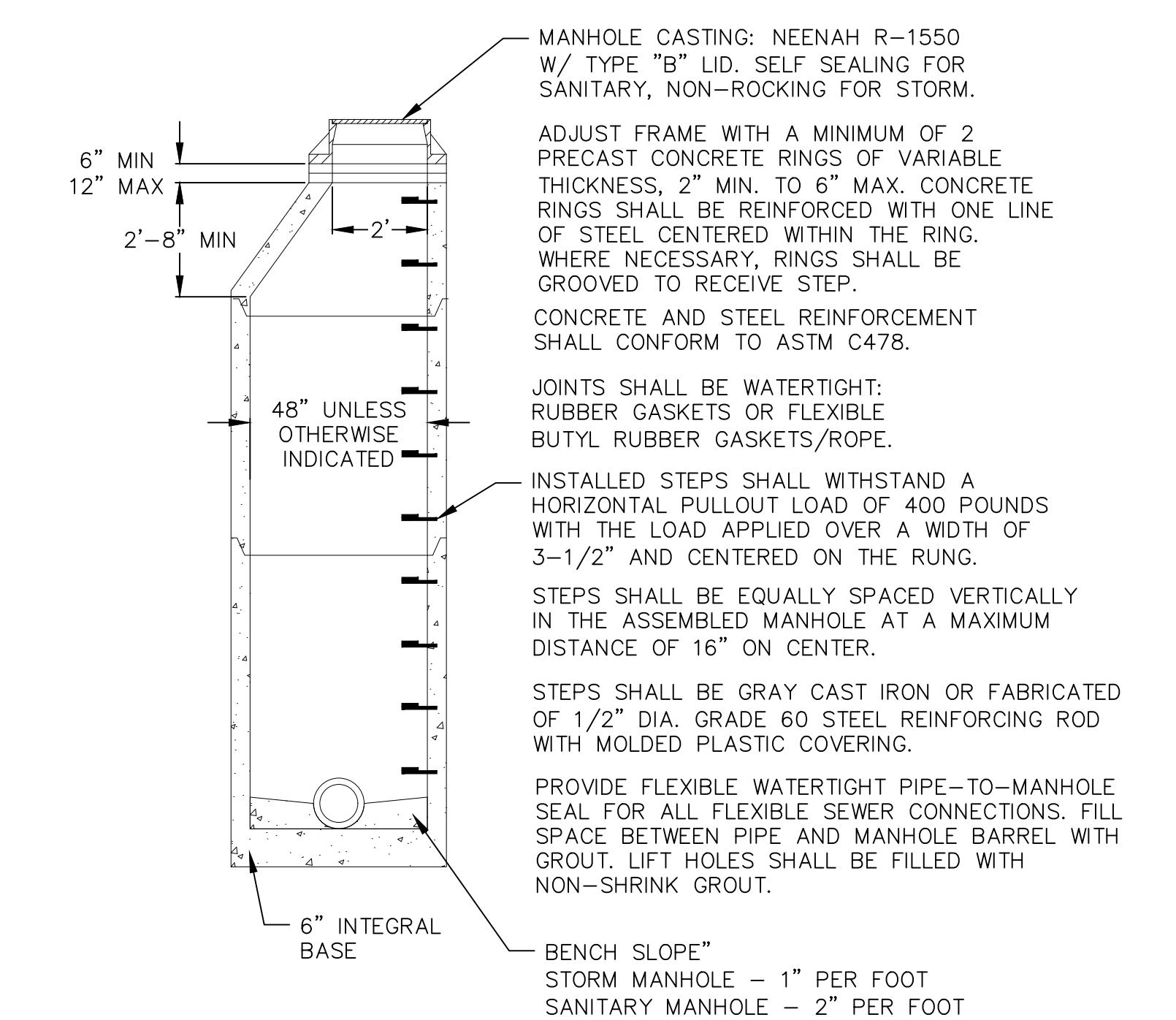
NOT TO SCALE



5 CURB INLET - TYPE 3, 2' x 3' BASIN

C403

NOT TO SCALE



| Construction Details | |
|----------------------|-------------|
| REVISIONS | REVISIONS |
| NO. DATE | NO. DATE |
| REMARKS | REMARKS |
| DATE 08/09/2024 | DATE |
| DRAFTER CKNA/CSHE | DRAFTER |
| CHECKED JKAS | CHECKED |
| PROJECT NO. 200196 | PROJECT NO. |

PROJECT SUMMARY

CALCULATION DETAILS

- LOADING = H20+H2S
- APPROX. LINEAR FOOTAGE = 254 LF

STORAGE SUMMARY

- STORAGE VOLUME REQUIRED = N/A
- PIPE STORAGE VOLUME = 11,221 CF
- BACKFILL STORAGE VOLUME = 0 CF
- TOTAL STORAGE PROVIDED = 11,221 CF

PIPE DETAILS

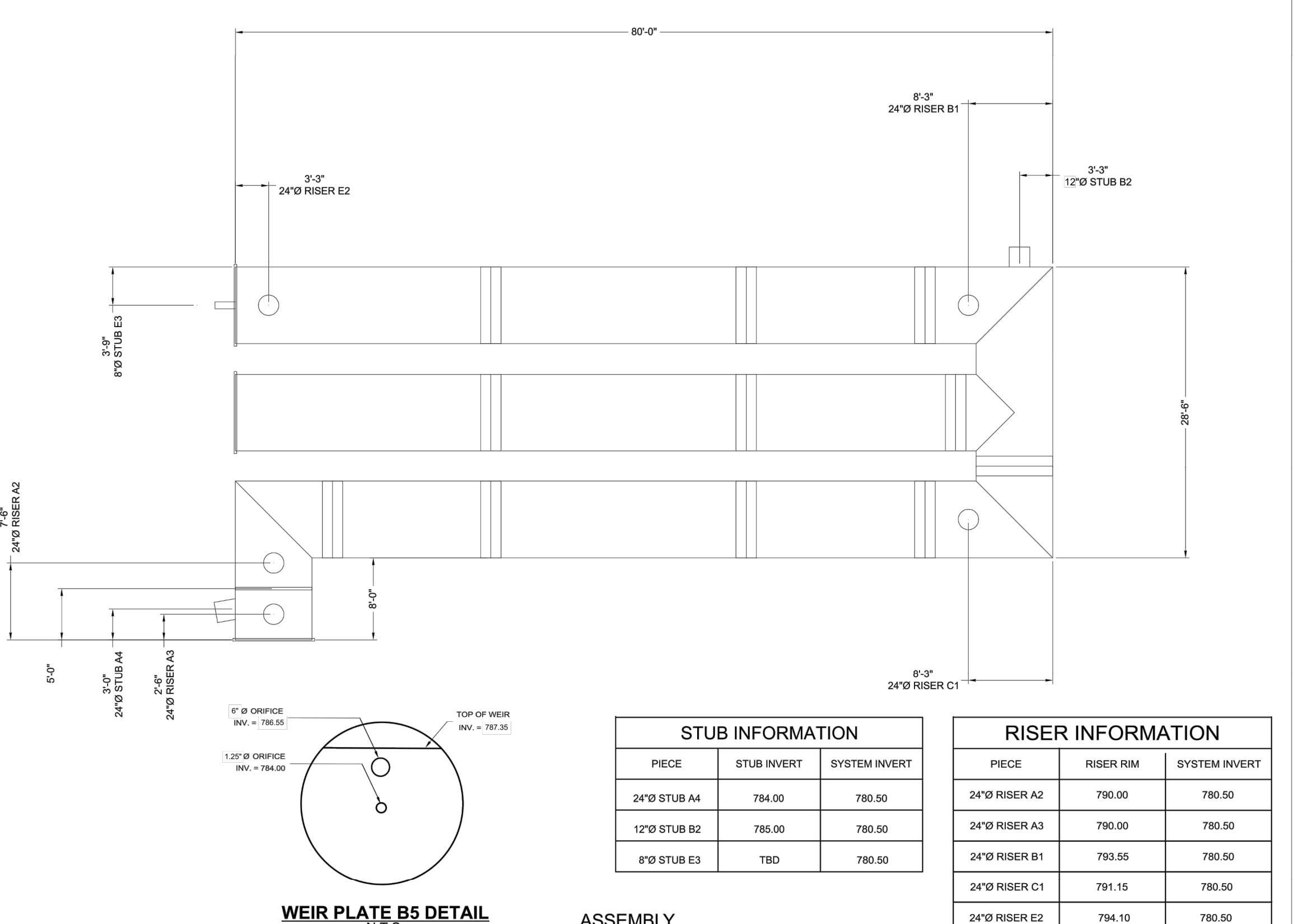
- DIAMETER = 9"
- CORRUGATION = 5x1
- GAGE = 14
- COATING = ALTAZ
- WALL TYPE = SOLID
- BARREL SPACING = 36"

BACKFILL DETAILS

- WIDTH AT ENDS = 12"
- ABOVE PIPE = 0"
- WIDTH AT SIDES = 12"
- BELOW PIPE = 0"

NOTES

- ALL RISER AND STUB DIMENSIONS ARE TO CENTERLINE. ALL ELEVATIONS, SPACINGS, AND LOCATIONS OF INLETS AND INLETS SHALL BE VERIFIED BY THE ENGINEER OF RECORD PRIOR TO RELEASING FOR FABRICATION.
- ALL RISERS AND STUBS ARE 2 $\frac{1}{2}$ " x 1 $\frac{1}{2}$ " CORRUGATION AND 16 GAGE UNLESS OTHERWISE NOTED.
- REINFORCING IS NOT PROVIDED.
- QUANTITY OF PIPE SHOWN DOES NOT PROVIDE EXTRA PIPE FOR CONNECTING THE SYSTEM TO EXISTING DRAINAGE FACILITIES. YOUR SYSTEM AS DETAILED PROVIDES NOMINAL INLET AND OUTLET PIPE STUB FOR CONNECTION TO EXISTING DRAINAGE FACILITIES. IF ADDITIONAL PIPE IS NEEDED IT IS THE RESPONSIBILITY OF THE CONTRACTOR.
- BACKFILL TYPE TO BE DETERMINED UPON FINAL DESIGN.
- BACKFILL SUMMARY IS REFLECTIVE OF THE DYODS DESIGN. QUANTITIES ARE APPROX. AND SHOULD BE VERIFIED UPON FINAL DESIGN AND APPROVAL. THE CONTRACTOR IS ADVISED THAT THIS DOES NOT CONSIDER ALL VARIABLES SUCH AS SIZING AND ONLY ACCOUNTS FOR MATERIAL WITHIN THE ESTABLISHED SPACING.
- THESE DRAWINGS ARE FOR CONCEPTUAL PURPOSES AND DO NOT REFLECT ANY LOCAL PREFERENCES OR REQUIREMENTS. PLEASE CONTACT YOUR LOCAL CONTECH REP FOR MODIFICATIONS.



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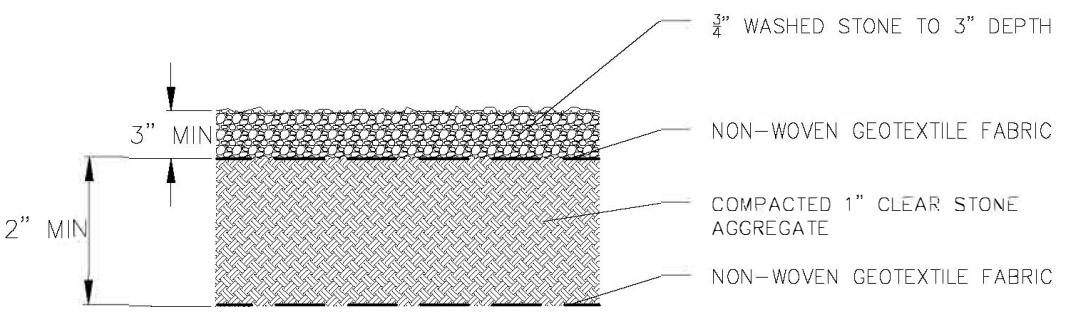
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LANDSCAPE MATERIAL NOTES:

1. CONTRACTOR SHALL PROVIDE A SUITABLE AMENDED TOPSOIL BLEND FOR ALL PLANTING AREAS WHERE SOIL CONDITIONS ARE UNSUITABLE FOR PLANT GROWTH. TOPSOIL SHALL CONFORM TO QUALITY REQUIREMENTS AS PER SECTION 625.2(1) OF THE "STANDARD SPECIFICATIONS FOR HIGHWAY CONSTRUCTION". PROVIDE A MINIMUM OF 18" OF TOPSOIL IN ALL PLANTING AREAS AND 6" OF TOPSOIL IN AREAS TO BE SEEDED/SODDED.
2. SUBSOIL UNDER TURF AND PLANTING BEDS MUST BE FREE DRAINING AND LOOSE TO ALLOW ROOT PENETRATION AND DRAINAGE. LANDSCAPE CONTRACTOR SHOULD NOTIFY GENERATOR CONTRACTOR. SUBSURFACE COMPACTION IS UNDESIRABLE. PLANTING LANDSCAPE CONTRACTOR IS NOT RESPONSIBLE FOR SUBSURFACE SOIL PREPARATION.
3. LANDSCAPE BEDS TO BE MULCHED WITH UNDYED SHREDDED HARDWOOD BARK MULCH TO 3" DEPTH MIN. DO NOT ALLOW MULCH TO TOUCH STEMS OR TRUNKS OF INSTALLED PLANTS. NO LANDSCAPE FABRIC TO BE INSTALLED WITHIN PLANTED AREAS.
4. AREAS IDENTIFIED AS WASHED STONE ARE TO BE INSTALLED USING 1"-2" WASHED STONE TO A DEPTH OF 3" MINIMUM. INSTALL 1" OF COMPACTED 1" CLEAR AGGREGATE STONE BELOW WASHED STONE. WASHED STONE AND CLEAR AGGREGATE STONE SEPARATED BY COMMERCIAL GRADE NON-WOVEN GEOTEXTILE FABRIC LAY COMMERCIAL GRADE NON-WOVEN GEOTEXTILE FABRIC BETWEEN GRADE AND STONE. APPROVE STONE PRODUCT WITH CLIENT PRIOR TO INSTALLATION.
5. AREAS IDENTIFIED AS 3" RAVEN BLACK STONE ARE TO BE INSTALLED USING 3" "RAVEN BACK" AS SUPPLIED BY HALQUIST STONE OR EQUAL APPROVED PRODUCT. TO A DEPTH OF 3" MINIMUM. LAY COMMERCIAL GRADE LANDSCAPE FABRIC BETWEEN GRADE AND STONE. APPROVE STONE PRODUCTS WITH CLIENT PRIOR TO INSTALLATION.



1
WASHED STONE
NOT TO SCALE

SEEDING AND PLUG PLANTING NOTES:

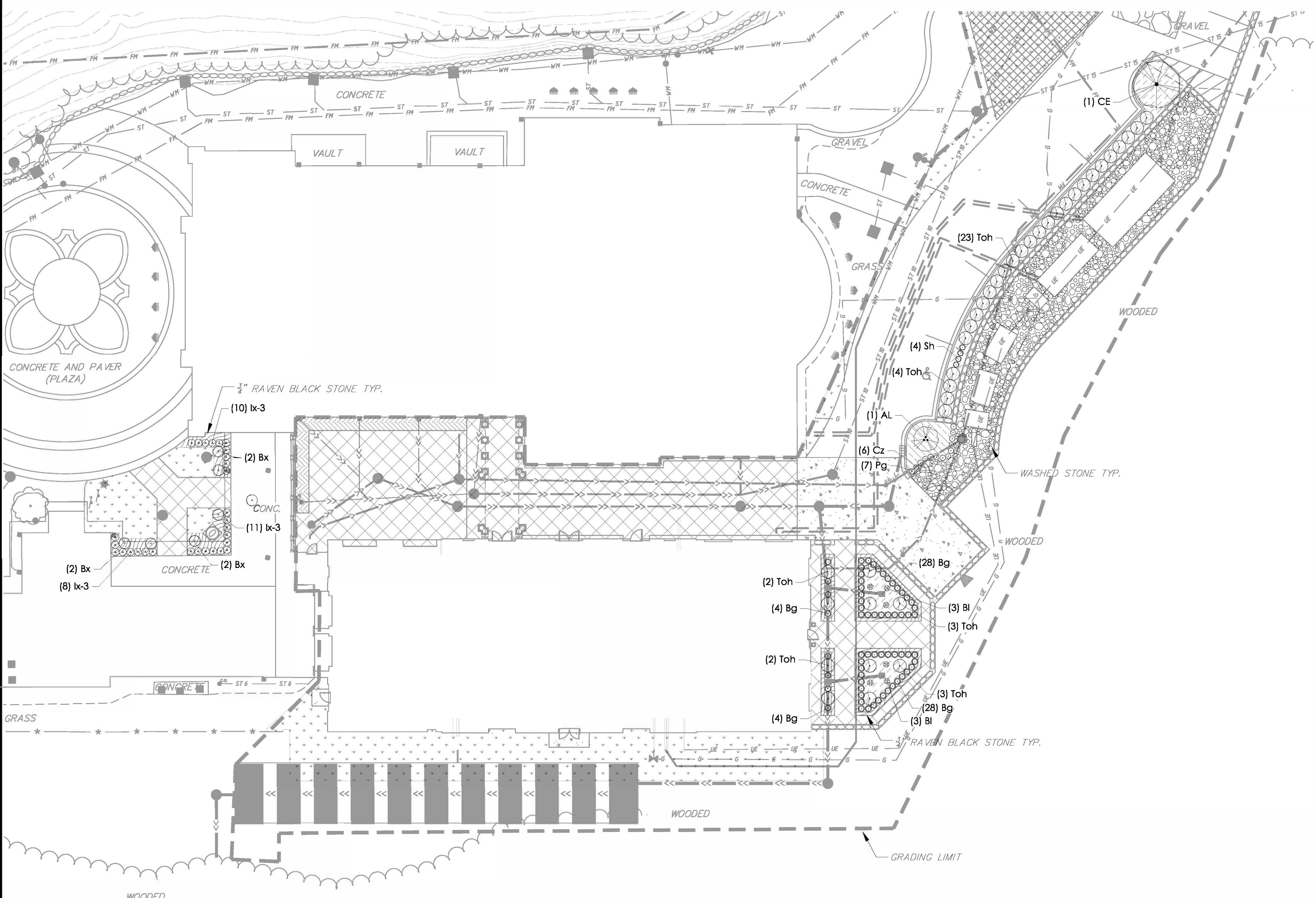
1. ALL AREAS SHOWN AS TURF GRASS TO BE SEDED WITH "MADISON PARKS" SEED MIX BY LA GROSSE SEED OR EQUIVALENT. ALL SEDED AREAS ARE TO BE WATERED DAILY TO MAINTAIN ADEQUATE SOIL MOISTURE FOR PROPER GERMINATION. AFTER VIGOROUS GROWTH IS ESTABLISHED, APPLY 3" WATER TWICE WEEKLY UNTIL FINAL ACCEPTANCE. (PRIOR TO ROUTINE MAINTENANCE SCHEDULE ESTABLISHMENT, MOWING SHOULD OCCUR TO MAINTAIN A TURF HEIGHT OF 3"-6") PRIOR TO SEEDING, APPLY A MINIMUM OF 4" TOPSOIL TO ENTIRE AREA. FOLLOWING SEEDING, APPLY A MULCH LAYER OF STRAW OR STRAW MAT.
2. INSTALL GROUNDCOVERS (GC) AS 2" X 2" X 4", 2.25" X 2.25" X 5" OR 2.5" X 2.5" X 3.5" ROOT MASS PLUGS OR EQUAL PLUGS TO BE INSTALLED 10" ON CENTER IN A TRIANGULAR GRID PATTERN. PLANT SPECIES RANDOMLY THROUGHOUT SPECIFIED AREA, MAINTAINING A REPRESENTATIVE RATIO OF SPECIES AS SHOWN IN THE CONCEPT PLANT SCHEDULE. THROUGHOUT PLANTING, PLUG NUMBERS ARE APPROXIMATE BASED ON AREA. CONTRACTOR TO CONFIRM QUANTITIES. QUANTITIES IN SCHEDULE REPRESENT TOTAL PLUGS PER SPECIES FOR THE GROUNDCOVER AREA. SHOW EACH PLUG TO RECEIVE ITS RESPECTIVE FRACTIONAL PLUG BASED ON THE SQUARE FOOTAGE OF EACH RESPECTIVE PLANTING LOCATION SPECIFIED, WHERE SHRUBS/TREES ARE SHOWN WITHIN GROUNDCOVER AREAS, SUBSTITUTE SHRUB/TREE FOR PLUG AND SPACE SURROUNDING PLUGS 10" FROM SHRUB/TREE ROOT MASS PATTERN ACCORDING. APPLY 1/2" WATER DAILY FOR 4 WEEKS FOLLOWING INSTALLATION. APPLY AN INITIAL APPLICATION OF PRE-EMERGENT HERBICIDE PER MANUFACTURER'S INSTRUCTIONS AND STATE REGULATIONS. APPLY 2" OF CEDAR MULCH AT TIME OF PLANTING.
3. ALL UNLABELED DISTURBED AREAS ADJACENT TO EXISTING WOODED VEGETATION TO BE SEDED WITH "SHADE SEED MIX" BY AGRECOL OR EQUIVALENT, PER MANUFACTURER'S SPECIFICATIONS.

GENERAL LANDSCAPE NOTES:

1. CONTRACTOR SHALL OBTAIN ALL NECESSARY PERMITS FOR ANY RIGHT OF WAY WORK.
2. CONTRACTOR SHALL VERIFY ALL UTILITIES WITHIN SCOPE OF CONTRACT.
3. CONTRACTOR SHALL COORDINATE ALL WORK WITH OTHER CONTRACTORS AT SITE AND COMPLETE WORK PER SCHEDULE.
4. CONTRACTOR SHALL CLEAN ALL PAVEMENT AREAS WITHIN SITE AFTER COMPLETION. CONTRACTOR SHALL CLEAN ANY Affected PAVED AREAS OUTSIDE OF DISTURBANCE DELINEATION DAILY.
5. ALL MATERIAL QUANTITIES AND AREA MEASUREMENTS SHOWN ON LANDSCAPE PLAN ARE TO BE CONFIRMED BY LANDSCAPE CONTRACTOR. LANDSCAPE CONTRACTOR IS RESPONSIBLE FOR VERIFYING AND ADJUSTING FOR ANY QUANTITATIVE DISCREPANCIES BETWEEN PLAN, SCHEDULES, AND PREPARED CONDITIONS PRIOR TO INSTALLATION.
6. PLANTS SHALL BE INSTALLED WHEN ALL GRAADING AND CONSTRUCTION HAS BEEN COMPLETED WITHIN THE IMMEDIATE VIGINTY.
7. ANY PREPARED SITE CONDITIONS THAT CONTRADICT THE LANDSCAPE PLAN AND NEGATIVELY AFFECT THE SUCCESS OF PLANTINGS SHALL BE BROUGHT TO THE ATTENTION OF THE LANDSCAPE ARCHITECT.
8. LANDSCAPE CONTRACTOR TO PROVIDE 60 DAYS OF INITIAL MAINTENANCE PERIOD FOLLOWING LANDSCAPE INSTALLATION. CONTRACTOR IS RESPONSIBLE FOR WATERING ALL SEEDINGS AND PLANTINGS, AS WELL AS MOWING, WEEDING AND MATERIAL CLEAN UP.

PLANT MATERIAL NOTES:

1. ALL PLANTINGS SHALL CONFORM TO QUALITY REQUIREMENTS AS PER ANSI Z60.1.
2. ALL PLANT MATERIAL SHALL BE TRUE TO SPECIES, VARIETY AND SIZE SPECIFIED, NURSERY GROWN IN ACCORDANCE WITH GOOD HORTICULTURAL PRACTICES, AND UNDER CLIMATIC CONDITIONS SIMILAR TO THOSE OF THE PROJECT SITE.
3. CONTACT LANDSCAPE ARCHITECT, IN WRITING, TO REQUEST ANY PLANT MATERIAL SUBSTITUTIONS DUE TO AVAILABILITY ISSUES.
4. ALL PLANTS SHALL BE GUARANTEED TO BE IN HEALTHY AND FLOURISHING CONDITION DURING THE GROWING SEASON FOLLOWING INSTALLATION. ALL PLANT MATERIAL SHALL BE GUARANTEED FOR ONE YEAR FROM THE TIME OF INSTALLATION.
5. EXACT LOCATIONS OF EACH PLANT ARE GIVEN IN PLAN. WHILE SLIGHT DEVIATIONS ARE ACCEPTABLE, OVERALL SCHEMATIC/ORIENTATION TO BE ADHERED TO AS ACCURATELY AS POSSIBLE. NOTIFY LANDSCAPE ARCHITECT OF ANY CONFLICTS.



PLANT SCHEDULE

| CODE | BOTANICAL / COMMON NAME | ROOT COND. | SIZE | QTY |
|-------------------------|---|------------|--------|-----|
| UNDERSTORY TREES | | | | |
| AL | Amelanchier laevis / Allegheny Serviceberry | B & B | 5' ht. | 1 |
| CE | Cercis canadensis / Eastern Redbud Multi-trunk | B & B | 6' ht. | 1 |
| EVERGREEN SHRUBS | | | | |
| Bg | Buxus x 'Green Gem' / Green Gem Boxwood | Cont. | 5 Gal. | 64 |
| Bx | Buxus x 'Green Mountain' / Green Mountain Boxwood | Cont. | 5 Gal. | 7 |
| Ix-3 | Ilex glabra 'SMNGA#17' / Gem Box# Inkberry Holly | Cont. | 3 Gal. | 29 |
| Toh | Thuya occidentalis 'Holmstrup' / Holmstrup Cedar | B & B | 5' ht. | 37 |
| PERENNIALS | | | | |
| Bl | Baptisia alba / White Wild Indigo | Cont. | 1 Gal. | 6 |
| Cz | Coreopsis tripteris / Tall Coreopsis | Cont. | 1 Gal. | 6 |
| Pg | Parthenocissus virginiana / Switch Grass | Cont. | 1 Gal. | 7 |
| Sh | Sporobolus heterolepis / Prairie Dropseed | Cont. | 1 Gal. | 4 |

CONCEPT PLANT SCHEDULE

| | |
|--|-------------------------------------|
| 3/4" RAVEN BLACK STONE | 522 sf |
| GC #1 Antennaria plantaginifolia / Pussytoes Sedum ternatum / Wild Stonecrop | 759 sf 397 737 |
| GC #2 Carex brevior / Oval Sedge Liatris aspera / Rough Blazing Star Lupinus perennis / Wild Lupine Pycnanthemum virginianum / Mountain Mint Sporobolus heterolepis / Prairie Dropseed | 135 sf 57 16 8 6 115 |
| GC #3 Carex albicans / White-tinged Sedge Sedum ternatum / Wild Stonecrop | 302 sf 226 226 |
| TURF | 4,057 sf |
| WASHED STONE | 1,574 sf |

DATE
3/22/2024
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