

STRUCTURAL CALCULATIONS

Project Name: Kellogg Garage
Jay Street
La Crosse, WI

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Prepared for: Zettler Design Studio

Date Issued: March 2026

Design per ASCE 7-16 and IBC 2021



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3400 Losey Boulevard South
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Project KELLOGG GARAGE

Subject _____

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Signed [Signature]

LOADS PER ASCE 7-16 + IBC 2021

SNOW LOAD PER ASCE 7-16 CH 7

$P_g = 40$ PSF

$I_s = 1.0$

$C_e = 1.0$

$C_t = 1.2$

$$P_f = 0.7 P_g I_s C_e C_t = .7(40)(1.2) = 33.6 \text{ PSF}$$

DRIFT LOAD PARAPET LOADS

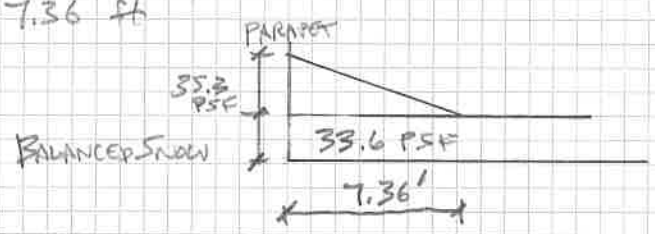
$L_d < 25'$

$$h_d = .43 \sqrt[3]{L_d} \sqrt[4]{P_g + 10} - 1.5 = .43 \sqrt[3]{25} \sqrt[4]{50} - 1.5 = 1.84 \text{ ft}$$

$$\rho = 0.13 P_g + 14 = 19.2 \text{ PCF}$$

$$\text{Snow Load Intensity} = h_d \rho = 1.84(19.2) = 35.3 \text{ PSF}$$

$$\text{DRIFT LENGTH} = 4 h_d = 7.36 \text{ ft}$$



WIND LOADS PER ASCE 7-16 CH 28 Simplified Procedure

FIGURE 28.5-1

MWERS LOADS

$V = 115$ mph

$h = 15'$

Roof Angle 5°

HORIZ PRESSURES

ZONE A	21 PSF
B	-10.9 PSF
C	13.9 PSF
D	-6.5 PSF

VERT PRESSURES

ZONE E	-25.2 PSF
F	-14.3 PSF
G	-17.5 PSF
H	-11.1 PSF

COMPONENTS + CLADDING LOADS PER ASCE 7-16

FIGURE 30.4-1



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ROOF FRAMING $l = 15'$

MAX LOAD = 33.6 PSF SNOW + 30 PSF DRIFT + 12 PSF DL

$$65.6(2) = 131.2 \text{ PLF}$$

$$M = \frac{WL^2}{8} = \frac{131.2(15)^2}{8} = 3690 \text{ lb-ft}$$

$$2 \times 10 \quad S_x = \frac{bd^2}{6} = 21.39 \text{ in}^3$$

$$F'_b \text{ REQD} = \frac{M}{S_x} = \frac{3690(12)}{21.39} = 2070 \text{ PSI}$$

2x10 DFL Select Structural

$$F'_b = 1500 \underset{C_D}{(1.15)} \underset{C_F}{(1.1)} = 2182 \text{ PSI} > 2070 \text{ PSI} \quad \underline{\text{OK}}$$

USE 2x10 DFL SELECT STRUCTURAL ROOF JOISTS @ 24" O.C. PROVIDE BRACING @ BEARING WALL & @ MID SPAN

HEADERS @ ON DOORS

$$\text{MAX SPAN} = 12' \quad l = 12.5$$

$$\text{LOAD} = 6(10) + 1(66) = 126 \text{ PLF}$$

WALL ABOVE ROOF

$$M = \frac{WL^2}{8} = \frac{126(12.5)^2}{8} = 2461 \text{ lb-ft}$$

$$\text{Find } S_x \text{ REQD \& } F'_b = 2450 \underset{C_D}{(1.15)} = 3393 \text{ PSI}$$

$$S_x = \frac{2461(12)}{3393} = 8.7 \text{ in}^3$$

DIMENSIONAL LUMBER OPTION DFL #2

$$F'_b = 900 \underset{C_D}{(1.15)} \underset{C_F}{(1.1)} = 1138.5 \text{ PSI}$$

$$\text{Find } S_x \text{ REQD \& } F'_b = 1138.5 \text{ PSI}$$

$$S_x = \frac{2461(12)}{1138.5} = 26 \text{ in}^3$$



USE 3PLY 2x10 DFL #2 W/ 2x TOP + BOTTOM W/ 2 JACK STUDS & 2 KING STUDS



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HEADERS & MAN DOORS

$$L = 4'$$

$$\text{LOAD} = 15/2 (33.6 + 15) = 365 \text{ PLF}$$

$$\frac{WELD^2}{8} = \frac{365(4)^2}{8} = 730 \text{ lb-ft}$$

$$\text{Find } S_x \text{ REQ'D } C_{Fb} = 900(1.15)(1.1) = 1139 \text{ PSI}$$

$$S_x = \frac{730(12)}{1139} = 7.7 \text{ IN}^3$$

USE 2 Ply 2x8 DFL#2 OR SPF#2 W/12 JACK + 1 King

STUD WALLS 14' WALL w/ROOF LOAD + Wind Load

Wind Load from Components + Cladding

$$V = 11.5 \text{ mph WALLS ZONE 4 } 20 \text{ SF} = -24.7 \text{ PSF}$$

$$\text{LOADS: DL ROOF} = 15(6.5) = 98 \text{ PLF}$$

$$\text{DL WALL} = 14(10) = 140 \text{ PLF}$$

$$\text{SNOW} = 6.5(33.6) = 218 \text{ PLF}$$

USE LOAD COMBINATION $DL + .75 \text{ SNOW} + (.75)(.6) \text{ Wind}$

$$F_{max} = (98 + 140) \underset{16" \text{ O.C.}}{1.33} + 218 \underset{16" \text{ O.C.}}{(.75)} (1.33) = 535 \#$$

$$M_{max} = .6(.75) \frac{WELD^2}{8} = \frac{.6(.75)(24.7)(14)^2(1.33)}{8} = 362 \text{ lb-ft}$$

TRY 2x6 SPF#2 STUDS @ 16" O.C.

$$F_b = 875 \text{ PSI}$$

$$F_{c11} = 1150 \text{ PSI}$$

$$A = 8.25 \text{ IN}^2$$

$$S_x = 7.56 \text{ IN}^3$$

$$E = 1.4 \times 10^6$$

ADJUSTMENT FACTORS: $C_F = 1.15$ $C_F = 1.3$ $C_F = 1.1$ $C_D = 1.6$
 F_b F_c



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STUD WALLS CONT.

$$F_c^* = 1150 (1.15) (1.1) (1.6) = 2328 \text{ PSI}$$

$K_{CE} = 0.3$ VISUALLY GRADED LUMBER

$$\frac{le}{d} = \frac{14(12)}{5.5} = 30.5$$

$$F_{CE} = \frac{K_{CE} E}{\left(\frac{le}{d}\right)^2} = \frac{.3 (1.4 \times 10^6)}{(30.5)^2} = 451.5 \text{ PSI}$$

$$C_p = \frac{1 + \frac{F_{CE}/F_c^*}{2c}}{1 + \frac{F_{CE}/F_c^*}{2c} + \frac{F_{CE}/F_c^*}{c}} = \frac{1 + \frac{.19}{2(.74)}}{1 + \frac{.19}{2(.74)} + \frac{.19}{.55 - .24}} = \frac{1 + .127}{1 + .127 + .41} = \frac{1.127}{1.537} = .74$$

$C_c = 0.8$

$$F_{CE}/F_c^* = \frac{451.5}{2328} = .19$$

$C_p = 0.18$

$$F_c' = F_c^* C_p = 2328 (.18) = 419 \text{ PSI}$$

$$f_c = \frac{P}{A} = \frac{535}{8.25} = 64.8 \text{ PSI}$$

$$F_b' = F_b C_r C_f C_p = 875 (1.15) (1.3) (1.6) = 2093 \text{ PSI}$$

$$f_b = \frac{M}{S_x} = \frac{362(12)}{7.56} = 574 \text{ PSI}$$

Check Combined AXIAL + BENDING

$$\left(\frac{f_c}{F_c'}\right)^2 + \frac{f_b}{F_b' \left(1 - \frac{f_c}{F_c'}\right)} \leq 1.0$$

$$\left(\frac{64.8}{419}\right)^2 + \frac{574}{2093 \left(1 - \frac{64.8}{419}\right)} = 0.34 < 1.0 \quad \checkmark$$

.02 + .32

USE 2x6 SFR #2 STUDS @ 16" O.C.



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SHEAR WALLS

NAIL Plywood to studs w/ 8d NAILS @ 6" O.C. & USE SIMPSON DITZ3
@ CORNER BAYS

@ WALL w/ ON DOORS INSTALL PORTAL FRAMES PER UDC PG 30

HOLD DOWNS - USE H1 @ LOW STUD JOISTS

@ Center wall USE H10A-2



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FOUNDATIONS:

MAX LOAD = $14(10) = 140 \text{ PLF}$

$15/2(33.6 + 30 + 15) = 510 \text{ PLF}$

$.5(150)(1.5) = 113 \text{ PLF}$

TOTAL = 843 PLF

WALL DL

Reef Loads

Concrete Curb

$$F_b \text{ STR} = \frac{843 \text{ PLF}}{1850 \text{ PSF}} = .46 \text{ FT}$$

$$\text{SOIL BRC PRESSURE} = 2000 \text{ PSF} - 150 \text{ PSF}$$

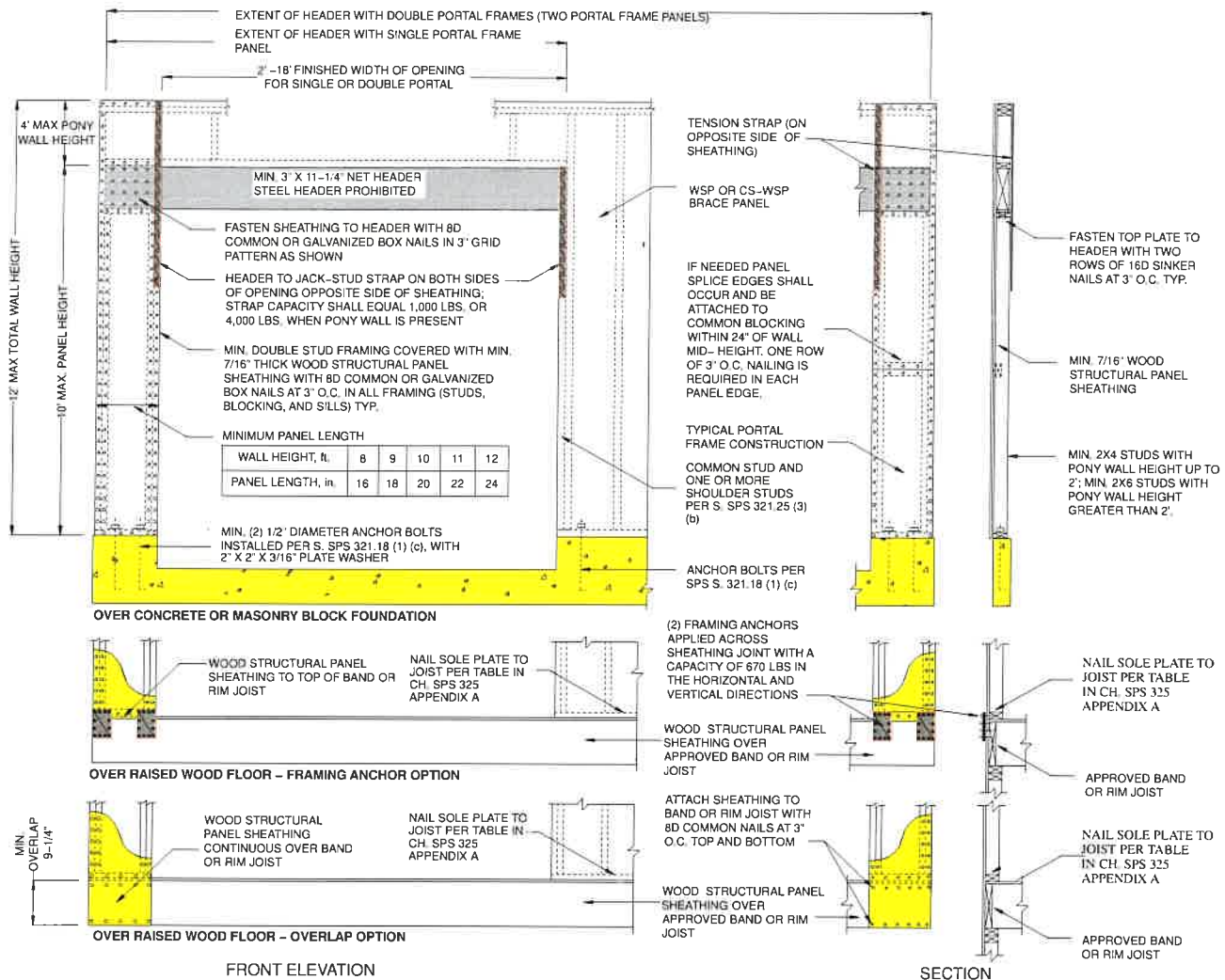
Fog wt.

USE 8" WIDEX 12" DEEP THICKENED SLAB FOOTING W/ (2) #4 BARS CONT.

STEM WALL 6" X 16" W/ #4 VERT + (2) #4 BARS CONT (1 LOW, 1 HIGH)

Figure 321.25-A

METHOD PF – PORTAL FRAME BRACE CONSTRUCTION



Note: Steel headers are permitted if designed by structural analysis.

Note: As shown in the above cross-section, 1/2-inch gypsum wallboard is not required on the interior side of the wall.

(c) *Bracing amount.* Bracing methods and materials complying with Table 321.25-G shall be applied to walls in accordance with all of the following requirements:

1. For the purpose of determining bracing amounts, the outermost extents of the building plan at each floor level shall be circumscribed with a rectangle to define the overall length of each building side as shown in Figure 321.25-B.
2. In no case may the amount of bracing be less than two braced wall panels on walls parallel to each rectangle side for each floor level of the building.
3. Where used, the number of intermittent brace panels applied to walls parallel to each rectangle side shall comply with Table 321.25-I.
4. Where used, the total length of continuous sheathed brace panels applied to walls parallel to each building side shall comply with Table 321.25-J.
5. The location of brace panels applied to walls parallel to

each building side shall comply with Figure 321.25-C.

6. Balloon-frame walls may be no longer than 21 feet and shall have a maximum height of two floors unless constructed in accordance with an approved design. Wall framing shall be continuous from the lowest floor to the wall top plate at the roof. All edges of sheathing shall be supported on and fastened to blocking or framing. Braced wall panels may not be required on the balloon-frame wall portion provided the bracing amount and brace spacing requirement are satisfied for the building side. Where brace panels are located on the balloon-frame wall portion, they shall have a height-to-width ratio of not more than 2.5:1.

7. For a gable end wall, if the brace-panel height does not exceed 12 feet at the highest portion and if the 12½-foot and 21-foot spacing requirements in Figure 321.25-C are met, the wall is adequately braced. Where a brace panel exceeds 12 feet in height, it shall have a height-to-width ratio of not more than 2.5:1, and comply with Figure 21.25-C.

H/TSP

Seismic and Hurricane Ties

Simpson Strong-Tie hurricane ties provide a positive connection between truss/rafter and the wall of the structure to resist wind and seismic forces.

Material: See table

Finish: Galvanized. H1, H1Z, H7Z and H11Z — ZMAX® coating. Some models available in stainless steel or ZMAX; H1A, H2.5A also available (in Spring 2026) in black powder coat (H1APC, H2.5APC)

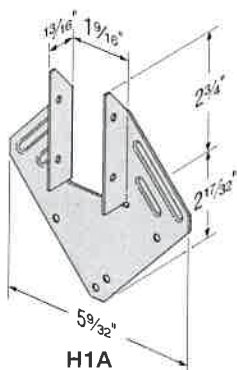
Installation:

- Use all specified fasteners; see General Notes.
- Hurricane ties can be installed with flanges facing inward or outward.
- H2.5T, H3 and H6 ties are shipped in equal quantities of right and left versions (right versions shown).

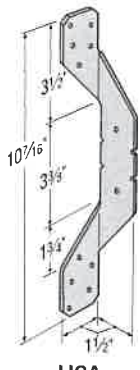
- Hurricane ties do not replace solid blocking.
- When installing ties on plated trusses (on the side opposite the truss plate) do not fasten through the truss plate from behind. This can force the truss plate off of the truss and compromise truss performance.
- H10A optional nailing to connect shear blocking, use 0.131" x 2 1/2" nails. Slots allow maximum field bending up to a pitch of 6:12; use H10A sloped loads for field-bent installation.

Codes: See p. 12 or Code Reference Key Chart

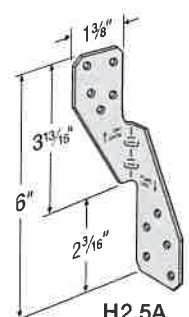
Web Applications: Visit app.strongtie.com/rws to access our Roof-to-Wall Selector web application.



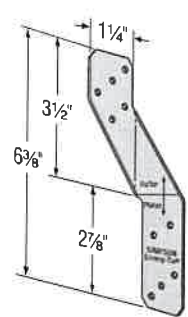
H1A
(H1.81Z similar)



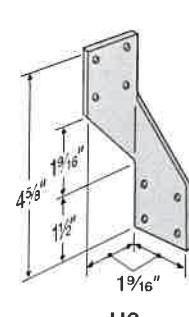
H2A
(H2ASS similar)



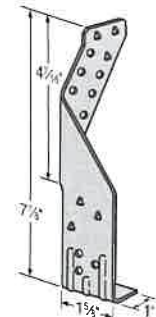
H2.5A
(H2.5ASS similar)



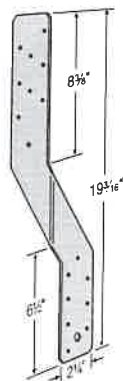
H2.5T



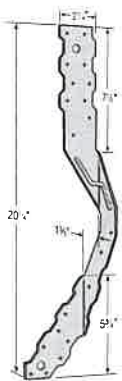
H3
(H3SS similar)



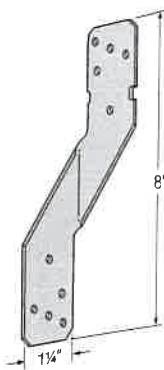
TSP



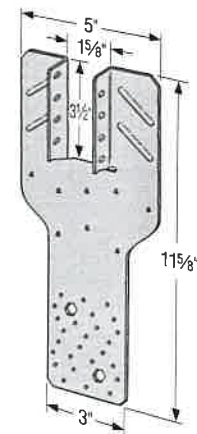
H6



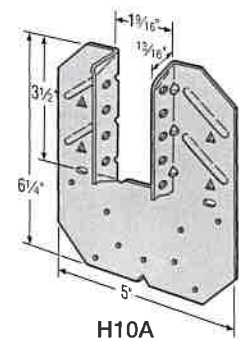
H7Z



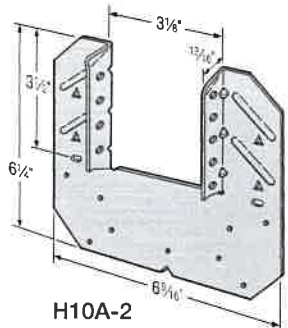
H8
(H8SS similar)



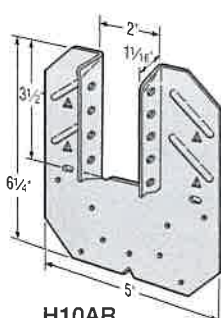
H10S



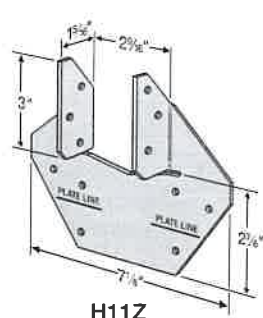
H10A
(H10ASS similar)



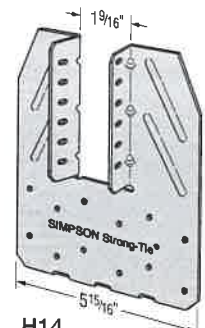
H10A-2



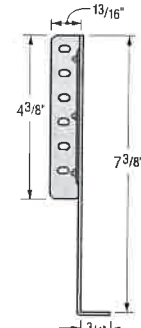
H10AR



H11Z



H14



H14 Profile

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Straps and Ties

H/TSP

Seismic and Hurricane Ties (cont.)

These products are available with additional corrosion protection. For more information, see pp. 13–19.

SS For stainless-steel fasteners, see p. 25.

SD Many of these products are approved for installation with Strong-Drive® SD Connector screws. See pp. 380–382 for more information.

Model No.	Ga.	Fasteners (in.)			DF/SP Allowable Loads			Uplift with 0.131" x 1 1/2" Nails (160)	SPF/HF Allowable Loads			Uplift with 0.131" x 1 1/2" Nails (160)	Code Ref.
		To Rafters/Truss	To Plates	To Studs	Uplift (160)	Lateral (160)			Uplift (160)	Lateral (160)			
						F ₁	F ₂			F ₁	F ₂		
H1A	18	(4) 0.131 x 1 1/2	(4) 0.131 x 1 1/2	—	545	420	265	—	470	360	205	—	IBC, FL, LA
H1.81Z	18	(6) 0.131 x 1 1/2	(4) 0.131 x 2 1/2	—	540	440	170	460	465	380	130	395	—
H2A	18	(5) 0.131 x 1 1/2	(2) 0.131 x 1 1/2	(5) 0.131 x 1 1/2	525	130	55	—	495	130	55	—	IBC, FL, LA
SS H2ASS	18	(5) 0.131 x 1 1/2	(2) 0.131 x 1 1/2	(5) 0.131 x 1 1/2	400	130	55	400	345	130	55	345	—
H2.5A	18	(5) 0.131 x 2 1/2	(5) 0.131 x 2 1/2	—	700	110	110	625	615	110	110	540	IBC, FL, LA
SS H2.5ASS	18	(5) 0.131 x 2 1/2	(5) 0.131 x 2 1/2	—	440	75	70	365	380	75	70	310	—
H2.5T	18	(5) 0.131 x 2 1/2	(5) 0.131 x 2 1/2	—	590	135	145	480	565	135	145	475	IBC, FL, LA
H3	18	(4) 0.131 x 2 1/2	(4) 0.131 x 2 1/2	—	400	210	170	400	365	180	145	290	—
SS H3SS	18	(4) 0.131 x 2 1/2	(4) 0.131 x 2 1/2	—	280	145	120	275	225	100	85	210	—
H6 (to Plates)	16	—	(8) 0.131 x 2 1/2	(8) 0.131 x 2 1/2	930	—	—	—	800	—	—	—	—
H6 (to Rim)	16	(8) 0.131 x 2 1/2	—	(8) 0.131 x 2 1/2	1,230	—	—	—	1,065	—	—	—	IBC, FL, LA
H7Z	16	(4) 0.131 x 2 1/2	(2) 0.131 x 1 1/2	(8) 0.131 x 2 1/2	830	410	—	—	715	355	—	—	—
H8	18	(5) 0.148 x 1 1/2	(5) 0.148 x 1 1/2	—	780	95	90	630	710	95	90	510	—
SS H8SS	18	(5) 0.148 x 1 1/2	(5) 0.148 x 1 1/2	—	610	90	120	440	370	90	55	335	—
H10A Field Bent	18	(9) 0.148 x 1 1/2	(9) 0.148 x 1 1/2	—	780	565	285	—	760	485	285	—	IBC, FL, LA
H10A	18	(9) 0.148 x 1 1/2	(9) 0.148 x 1 1/2	—	1,040	565	285	—	1,015	485	285	—	—
SS H10ASS	18	(9) 0.148 x 1 1/2	(9) 0.148 x 1 1/2	—	970	565	170	—	835	485	170	—	—
H10AR	18	(9) 0.148 x 1 1/2	(9) 0.148 x 1 1/2	—	1,050	490	285	—	905	420	285	—	—
H10S	18	(8) 0.131 x 1 1/2	(8) 0.131 x 1 1/2	(8) 0.131 x 2 1/2	910	660	215	550	785	570	185	475	IBC, FL, LA
H10A-2	18	(9) 0.148 x 1 1/2	(9) 0.148 x 1 1/2	—	1,080	680	260	—	930	585	225	—	—
H11Z	18	(6) 0.162 x 2 1/2	(6) 0.162 x 2 1/2	—	830	525	760	—	715	450	655	—	—
H14	18	(12) 0.131 x 1 1/2	(13) 0.131 x 2 1/2	—	1,275	725	285	—	1,050	480	245	—	IBC, FL, LA
		(12) 0.131 x 1 1/2	(15) 0.131 x 2 1/2	—	1,340	670	230	—	1,050	480	245	—	
TSP	16	(9) 0.148 x 1 1/2	(6) 0.148 x 1 1/2	—	755	310	190	—	650	265	160	—	IBC, FL, LA
		(9) 0.148 x 1 1/2	(6) 0.148 x 3	—	1,015	310	190	—	875	265	160	—	

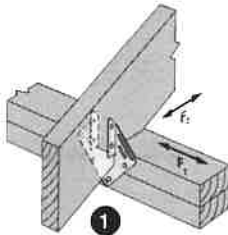
- See pp. 288–289 for Straps and Ties General Notes.
- Allowable loads are for one anchor. A minimum rafter thickness of 2 1/2" must be used when framing anchors are used on each side of the joist and on the same side of the plate (exception: connectors installed such that nails on opposite side don't interfere).
- Allowable DF/SP uplift load for stud-to-bottom plate installation (see detail 12) is 390 lb. (H2.5A); 265 lb. (H2.5ASS); and 310 lb. (H8). For SPF/HF values, multiply these values by 0.86.
- Allowable loads in the F₁ direction are not intended to replace diaphragm boundary members and do not account for possible cross-grain bending of the truss or rafter members.
- When cross-grain bending or cross-grain tension cannot be avoided in the members, mechanical reinforcement to resist such forces shall be considered by the designer.
- Southern pine allowable uplift loads for H10A = 1,105 lb. (160), H2.5A with 0.131" x 1 1/2" nails = 635 lb. (160) and H2.5A with 0.131" x 2 1/2" nails = 730 lb. (160).
- H10S can have the stud offset a maximum of 1" from the rafter (center to center) for a reduced uplift of 890 lb. (DF/SP) and 765 lb. (SPF).
- H10S nails to plates are optional for uplift but required for lateral loads.
- Some load values for the stainless-steel connectors shown here are lower than those for the carbon-steel versions. Ongoing test programs have shown this also to be the case with other stainless-steel connectors in the product line that are installed with nails. Visit strongtie.com/corrosion for updated information.
- The allowable loads of stainless-steel connectors match carbon-steel connectors when installed with stainless-steel Strong-Drive SCNR™ Ring-Shank Connector nails. For more information, refer to engineering letter L-F-SSNAILS at strongtie.com.
- Simpson Strong-Tie offers stainless-steel Strong-Drive SCNR Ring-Shank Connector nails. For bulk SCNR nails, see p. 375; for collated SCNR nails, see p. 376. For general fastener information, see pp. 25–26.
- Allowable DF/SP/SPF uplift load for the H2.5A fastened to a 2x4 truss bottom chord and double top plates using five 0.131" x 1 1/2" nails in the top plates and three 0.131" x 1 1/2" nails in the lowest three flange holes into the truss bottom chord is 260 lb. (160).
- For TSP installed stud to single plate see pp. 303–305.
- Fasteners:** Nail dimensions are listed diameter by length. See pp. 25–26 for fastener information.
- Using Strong-Drive SD Connector (SD9112) for 0.131" x 1 1/2" and 0.148" x 1 1/2", Strong-Drive SD Connector (SD9212) for 0.131" x 2 1/2" (and longer) and 0.148" x 2 1/2" (and longer), Strong-Drive SD Connector (SD10212) for 0.162" x 2 1/2" (and longer) will get the same load as nails.

Straps and Ties

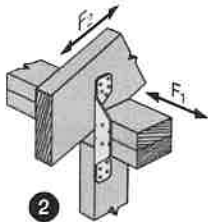
C-C-2026 © 2026 SIMPSON STRONG-TIE COMPANY INC.

H/TSP

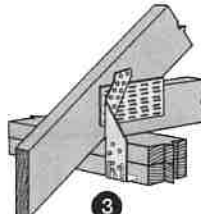
Seismic and Hurricane Ties (cont.)



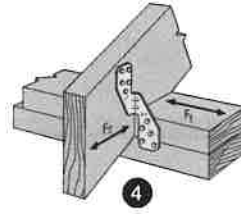
1 H1A Installation
(H1.81Z similar)



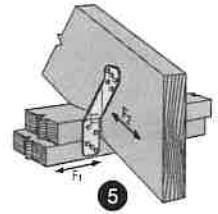
2 H2A Installation



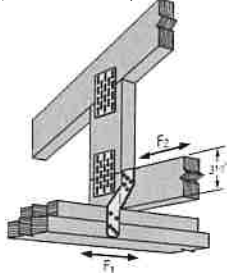
3 TSP Installation



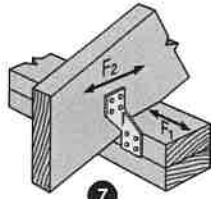
4 H2.5A Installation
(nails into both top plates)



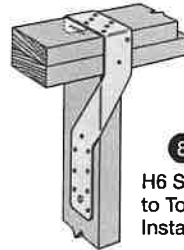
5 H2.5T Installation
(nails into both top plates)



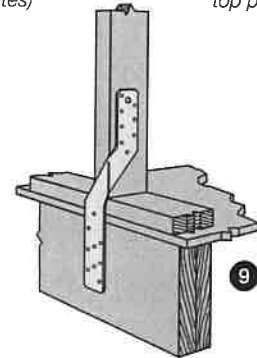
6 H2.5T Installation



7 H3 Installation
(nails into upper top plate)

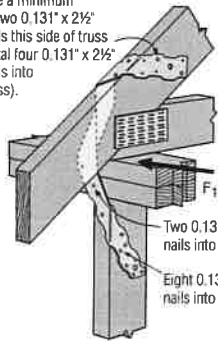


8 H6 Stud to Top Plate Installation



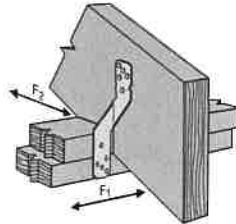
9 H6 Stud to Rim Board Installation

Use a minimum of two 0.131" x 2½" nails this side of truss (total four 0.131" x 2½" nails into truss).

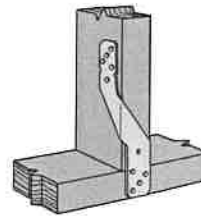


10 H7Z Installation

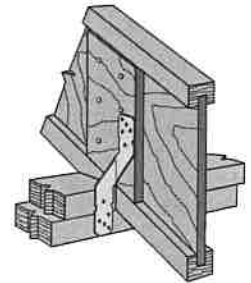
Two 0.131" x 2½" nails into plates.
Eight 0.131" x 2½" nails into studs.



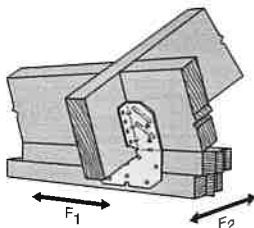
11 H8 Attaching Rafter to Double Top Plates



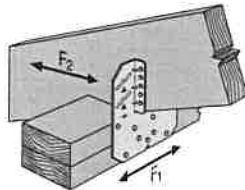
12 H8 attaching Stud to Sill
(4) 0.131" x 2½" nails into plate, (5) 0.131" x 2½" nails into stud, refer to footnote 3 for loads)



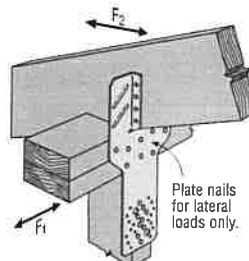
13 H8 attaching I-Joist to Double Top Plates



14 H10A Field-Bent Installation

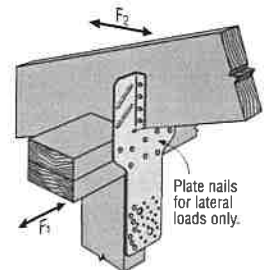


15 H10A Installation



16 H10S Installation

Plate nails for lateral loads only.



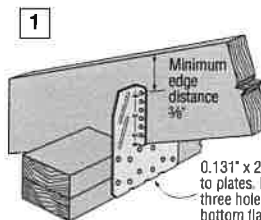
17 H10S Installation with Stud Offset

Plate nails for lateral loads only.

H10A optional nailing connects shear blocking to rafter. Use 0.131" x 2½" nails. Slot allows maximum field-bending up to a pitch of 6:12, bend one time only.

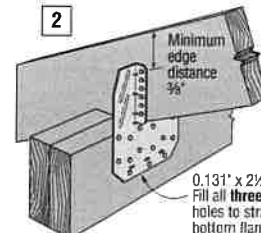


Visit app.strongtie.com/rws to access our Roof-to-Wall Selector web application.



18 H14 Installation to Double Top Plates

0.131" x 2½" nails to plates. Fill one of three holes to H14 bottom flange.



19 H14 Installation to Double 2x Header

Minimum edge distance 3/8".
0.131" x 2½" nails to header. Fill all three triangle holes to straightened bottom flange.

HDUE™/DTT™

Holdowns

Holdowns and
Tension Ties



This product is preferable to similar connectors because of (a) easier installation, (b) higher loads, (c) lower installed cost, or a combination of these features.

Engineered for higher load capacity, the new patent-pending HDUE holdown is ideal for meeting the higher design demands of today's residential wood structures. The HDUE provides exceptional overturning resistance for shearwalls, braced wall panels and other lateral force-resisting applications in wood construction. The HDUE is available in six sizes to meet a wide range of load requirements.

Tested per ICC-ES AC155, higher capacity models uniquely combine fasteners in both shear and tension, while reducing the number of screws required. The HDUE is fast and easy to install using Strong Drive[®] SDS Heavy Duty Connector screws, which reduce fastener slip and allow wood posts to maintain a greater net section than bolts.

The DTT tension ties are designed for lighter-duty holdown applications on single 2x posts. The DTT1Z[®] is installed with nails or Strong-Drive SD Connector screws and the DTT2 installs easily with the Strong-Drive SDS Heavy-Duty Connector screws (included). The DTT1Z holdowns have been tested for use in designed shearwalls and prescriptive braced wall panels as well as prescriptive wood-deck applications (see pp. 326–327 for deck applications).

HDUE Features:

- Pr deflect seat reduces deflection under load
- Angled fastening in the four larger sizes engages the screws in tension for higher load capacity, reducing the number of screws required
- Angled fastening tabs help drive fastener at a 45° angle and offset holes on the second back plate block the fastener from being driven straight
- Overlapping back plate increases fastener strength and shear values, helping prevent post splitting
- Optimized screw patterns reduce splitting at the end of the post and maximize individual fastener capacity
- Installs with Strong-Drive SDS Heavy Duty Connector screws (included)

Material: See table

Finish: HDUE — G90 and HDG;

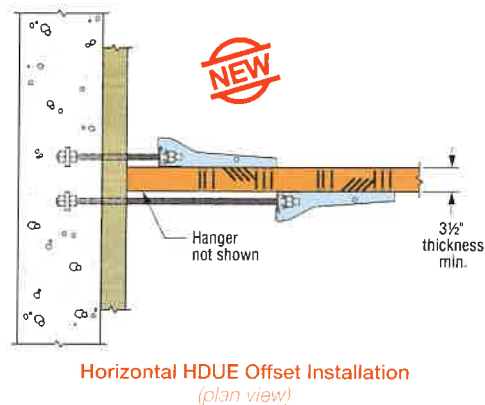
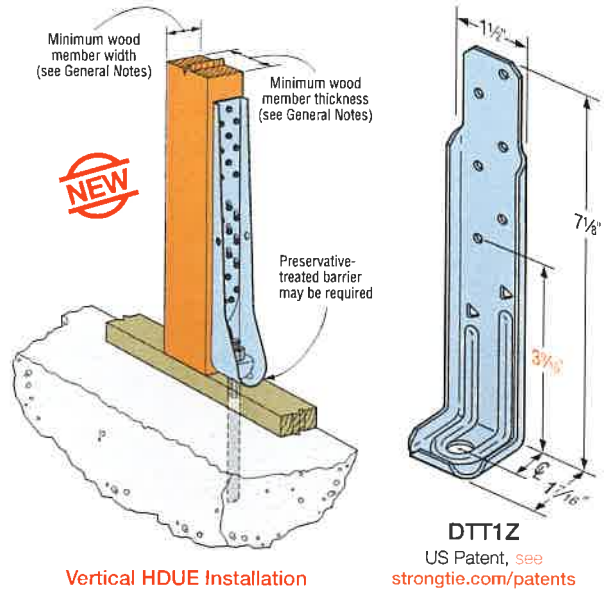
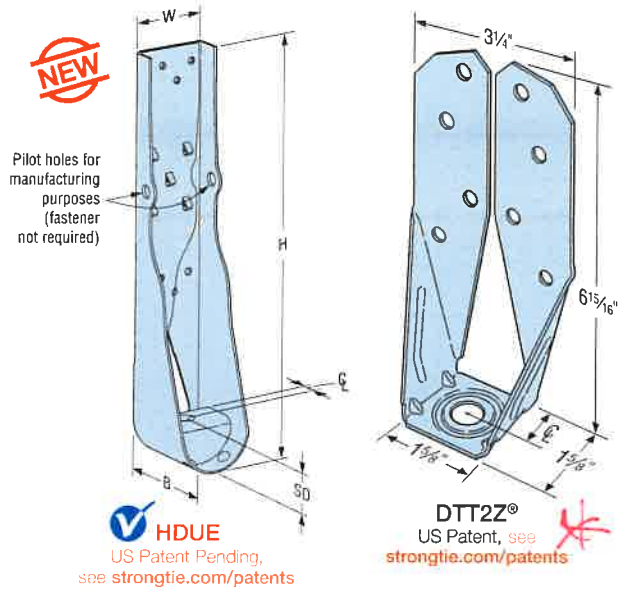
DTT1 and DTT2 — ZMAX[®] coating and stainless steel

Installation:

- See Holdown and Tension Tie General Notes on pp. 57–58.
- The HDUE requires no additional washer; the DTT requires a standard-cut washer (included) be installed between the nut and the seat.
- HDUE13 requires heavy hex nut (provided).
- Strong-Drive SDS Heavy-Duty Connector screws install best with a low-speed high-torque drill with a 3/8" hex-head driver.
- Angled fasteners should be driven at 45° angle.
- Fasteners and crescent washer are included with the holdowns. To order replacements, please contact Simpson Strong-Tie.

Codes: See p. 12 for Code Reference Key Chart

Web Applications: Visit app.strongtie.com/pfd to access our Post-to-Foundation Designer web application.



See Holdown and Tension Tie General Notes on pp 57–58.

Holdowns (cont.)

These products are available with additional corrosion protection. For more information, see pp. 13–19.

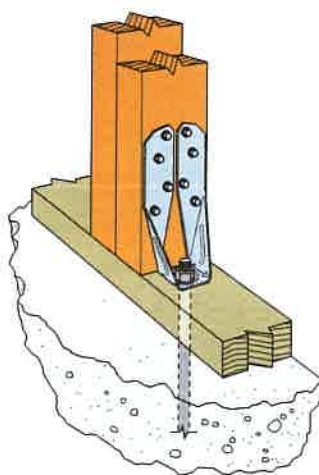
SS For stainless-steel fasteners, see p. 25.

SD Many of these products are approved for installation with Strong-Drive® SD Connector screws. See pp. 380–382 for more information.

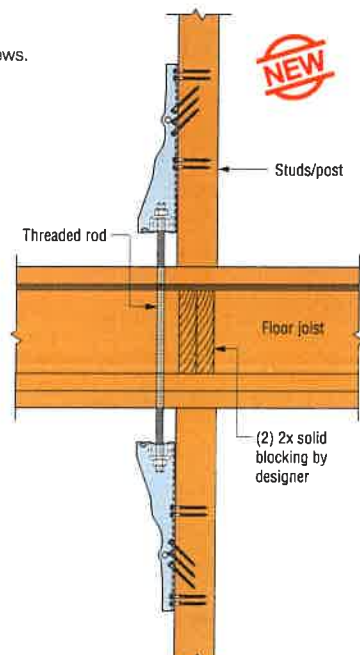
Model No.	Ga.	Dimensions (in.)					Fasteners (in.)			Minimum Wood Member Size Thickness x Width (in.)	Allowable Tension Loads (160)			Code Ref.
		W	H	B	CL	SO	Anchor Bolt Dia.	Wood Fasteners	DF/SP		SPF/HF	Deflection at Allowable Load (in.)		
SS DTT1Z®	14	1½	7½	1⅞	¾	¾	¾	¾	(6) #9 x 1½ SD	1½ x 3½	840	840	0.170	IBC, FL, LA
									(6) 0.148 x 1½		910	640	0.167	
									(8) 0.148 x 1½		910	850	0.167	
SS DTT2Z®	14	3¼	6⅞	1⅞	1⅞	¾	½	(8) ¼ x 1½ SDS	1½ x 3½	1,825	1,800	0.105		
								(8) ¼ x 1½ SDS		2,145	1,835	0.128		
SS DTT2Z-SDS2.5								(8) ¼ x 2½ SDS	3 x 3½	2,145	2,105	0.128		
HDUE3-SDS3	14	2⅞	8⅞	3⅞	1⅞	1½	¾	(7) ¼ x 3 SDS	3 x 3½	3,790	3,340	0.127		
HDUE5-SDS3	14	2⅞	11⅞	3⅞	1⅞	1½	¾	(10) ¼ x 3 SDS	3 x 3½	5,375	4,700	0.146		
HDUE7-SDS3	14	2⅞	14⅞	3⅞	1⅞	1½	¾	(13) ¼ x 3 SDS	3 x 3½	7,015 ¹	6,030	0.154		
HDUE9-SDS3.5	12	3	17⅞	4⅞	1⅞	1½	¾	(16) ¼ x 3½ SDS	3½ x 3½	8,425	7,305	0.159		
										4½ x 3½	9,390	7,995	0.134	
HDUE13-SDS3.5	12	3	23⅞	4⅞	1⅞	1½	1	(23) ¼ x 3½ SDS	5½ x 3½	11,900	10,215	0.164		
										7¼ x 3½	12,950	11,030	0.145	
										5½ x 5½	13,110	10,980	0.135	
HDUE17-SDS4.5	10	3	27⅞	5⅞	1⅞	1½	1	(28) ¼ x 4½ SDS	5½ x 3½	16,040	13,545	0.094		
										5½ x 5½	17,685 ²	14,775	0.111	



1. Allowable loads have been increased for wind or earthquake loading with no further increase allowed. Reduce where other loads govern.
2. To obtain LRFD values for holdowns, multiply allowable loads by 1.4. See evaluation report for LRFD deflections.
3. The designer must specify anchor bolt type, length and embedment. Some of the tabulated holddown tension loads exceed the tensile strength for of ASTM F1554 Grade 36 anchor bolts.
4. HDUE13 requires heavy-hex anchor nut to achieve tabulated loads (supplied with holddown).
5. Allowable loads for alternate HDUE installations using shorter screws are provided in engineering letter L-C-HDUESDS at strongtie.com.
6. Refer to p. 327 for DTT1SS loads and required fasteners.
7. **Fasteners:** Nail dimensions are listed diameter by length. SD and SDS screws are Simpson Strong-Tie Strong-Drive SD Connector and SDS Heavy-Duty Connector screws. See pp. 25–26 for fastener information.



Typical DTT2Z Installation



Typical HDUE Tie Between Floors

Holdowns and Tension Ties