

SITE PLAN NOTES

LOCATION OF UTILITIES, PAVED SURFACES, STORM DRAINAGE, ETC., ARE APPROXIMATE BASED ON PREVIOUS PLANS FOR CONSTRUCTION IN THIS AREA.

DISCREPANCIES TO ENGINEER AND/OR OWNER IMMEDIATELY UPON DISCOVERY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR DETERMINING THE

EXACT LOCATION OF ALL EXISTING UTILITIES, WHETHER SHOWN ON THESE PLANS OR NOT,

BEFORE COMMENCING WORK, AND SHALL BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CAUSED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UTILITIES. CALL DIGGERS HOTLINE (800) 242-8511

UNDERGROUND UTILITIES HAVE BEEN VERIFIED WITH

3. IT SHALL BE THE CONTRACTORS RESPONSIBILITY TO ARRANGE FOR ANY NECESSARY INSPECTIONS BY LOCAL GOVERNMENT THAT MAY BE REQUIRED.

4. PROVIDE A MINIMUM SLOPE AWAY FROM BUILDING OF 1/2" PER FOOT UNLESS NOTED OTHERWISE.

REPORT ANY AND ALL DISCREPANCIES TO SUCH ASSUMPTIONS AS DISCOVERED DURING EXCAVATION

THE OWNER SHALL PROVIDE DESIGNATED SPACE ADJACENT TO THE BUILDING FOR THE COLLECTION

OWNER TO PROVIDE AT LEAST 1 VAN ACCESSIBLE PARKING SPACE (132" MIN. WIDTH) AS PER I ICC/ANSI 117.1, CHAPTER 5. INCLUDE VEHICLE SPACE AND AISLE MARKING AS PER ICC/ANSI

HANDICAPPED PARKING STALLS AS PER ICC/ANSI 117.1, SECTION 703.6.3.1 WITH INTERNATIONAL SYMBOL OF ACCESSIBILITY. INCLUDE "VAN

ACCESSIBLE" SIGN AT VAN PARKING SPACE. BOTTOM OF SIGNS TO BE 60" ABOVE PAVING AT PARKING

OF RECYCLABLE WASTE MATERIALS AS PER

117.1, FIG. 502.2. PROVIDE SIGNAGE AT

5. SOIL BEARING CAPACITY HAS BEEN ASSUMED.

TO ENGINEER AND/OR OWNER.

SPS 362.0400(2)

STALLS.

FIELD VERIFY ALL ITEMS AND REPORT

NO WORK SHALL PROCEED UNTIL ALL

THE UTILITY COMPANIES.

DRAWING INDEX MAIN BUILDING: PROPOSED SITE PLAN AND CODE INFO. A2 | MAIN BUILDING: PROPOSED 1ST FLOOR PLAN A3 | MAIN BUILDING: PROPOSED MEZZANINE PLAN A4 | MAIN BUILDING: BUILDING SECTIONS A5 | MAIN BUILDING: WALL SECTIONS MAIN BUILDING: EXTERIOR ELEVATIONS AND STRUCTURAL NOTES MAIN BUILDING: FOUNDATION PLAN AND DETAILS S2 | MAIN BUILDING: FLOOR FRAMING PLAN S3 | MAIN BUILDING: ROOF FRAMING PLAN S4 | WIND LOAD DETAILS & REPORTS C1 | EXISTING SITE PLAN & PROJECT NOTES C2 GRADING PLAN & NOTES PROPOSED SITE PLAN WITH STORM WATER RETENTION C4 | PROFILES & CROSS SECTIONS

CODE INFORMATION

1714 S. 16TH/ STREET

LA CROSSE COUNTY TAX PARCEL #17-50266-30

CITY OF LA CROSSE MUNICIPAL CODE CHAPTER 115 (ZONING) & CHAPTER 103 (BUILDINGS & BUILDING REGULATIONS)

ZONING DISTRICT

SCOPE OF WORK

CONSTRUCT 5,175 SF LUMBER YARD HEADQUARTERS BUILDING WITH MEZZANINE

OCCUPANCY - TOTAL OCCUPANCY LOAD = 75

MAIN BUILDING

MERCANTILE GROUP, M STORAGE GROUP, S-1 MODERATE HAZARD STORAGE

 $\overline{\text{MAIN}}$ BUILDING 1ST/ FLOOR = 5,175 SF COVERED EXTERIOR STORAGE= 240 SF

TOTAL = 7,095 SF

ADDRESS & LEGAL DESCRIPTION

CITY OF LA CROSSE

APPLICABLE CODES

WISCONSIN COMMERCIAL BUILDING CODE (2015 IBC W/AMENDMENTS)

LIGHT INDUSTRIAL DISTRICT

MAIN BUILDING

UNSEPARATED, UNPROTECTED MULTIPLE OCCUPANCIES BUSINESS GROUP, B

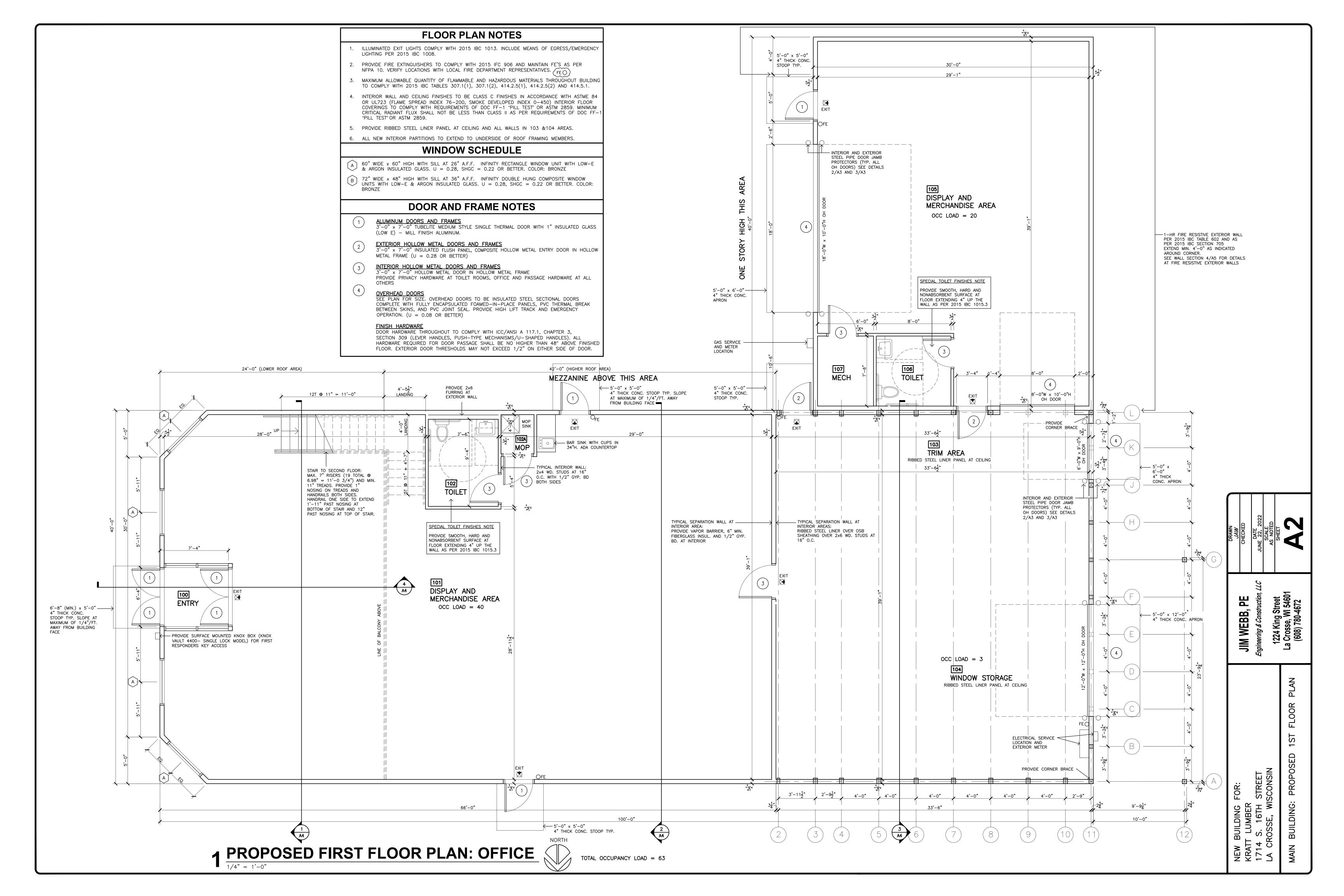
MAIN BUILDING MEZZANINE = 1,680 SF

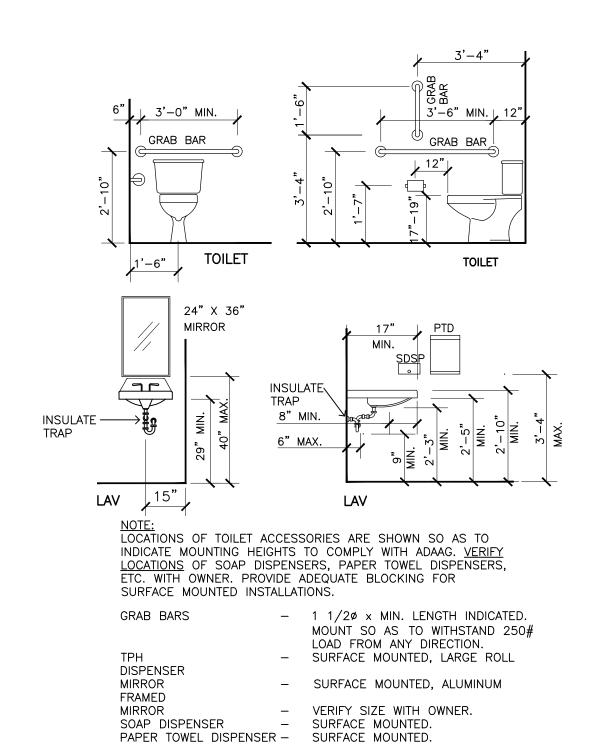
TYPE OF CONSTRUCTION TYPE VB, UNPROTECTED WOOD FRAME

NO AUTOMATIC FIRE SPRINKLER SYSTEM

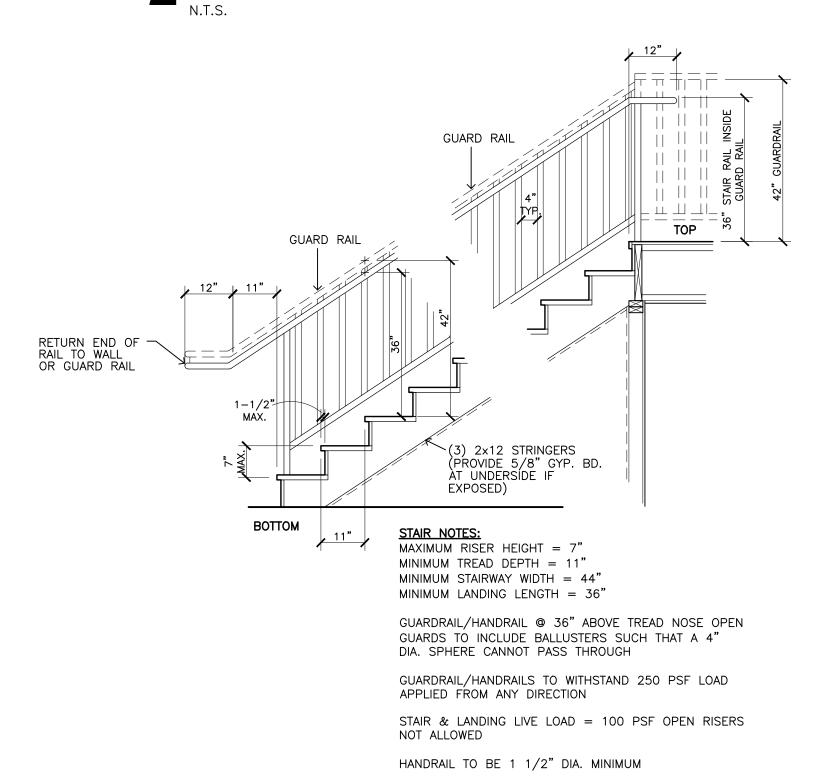
SEISMIC CATEGORY

JIM WEBB, PE

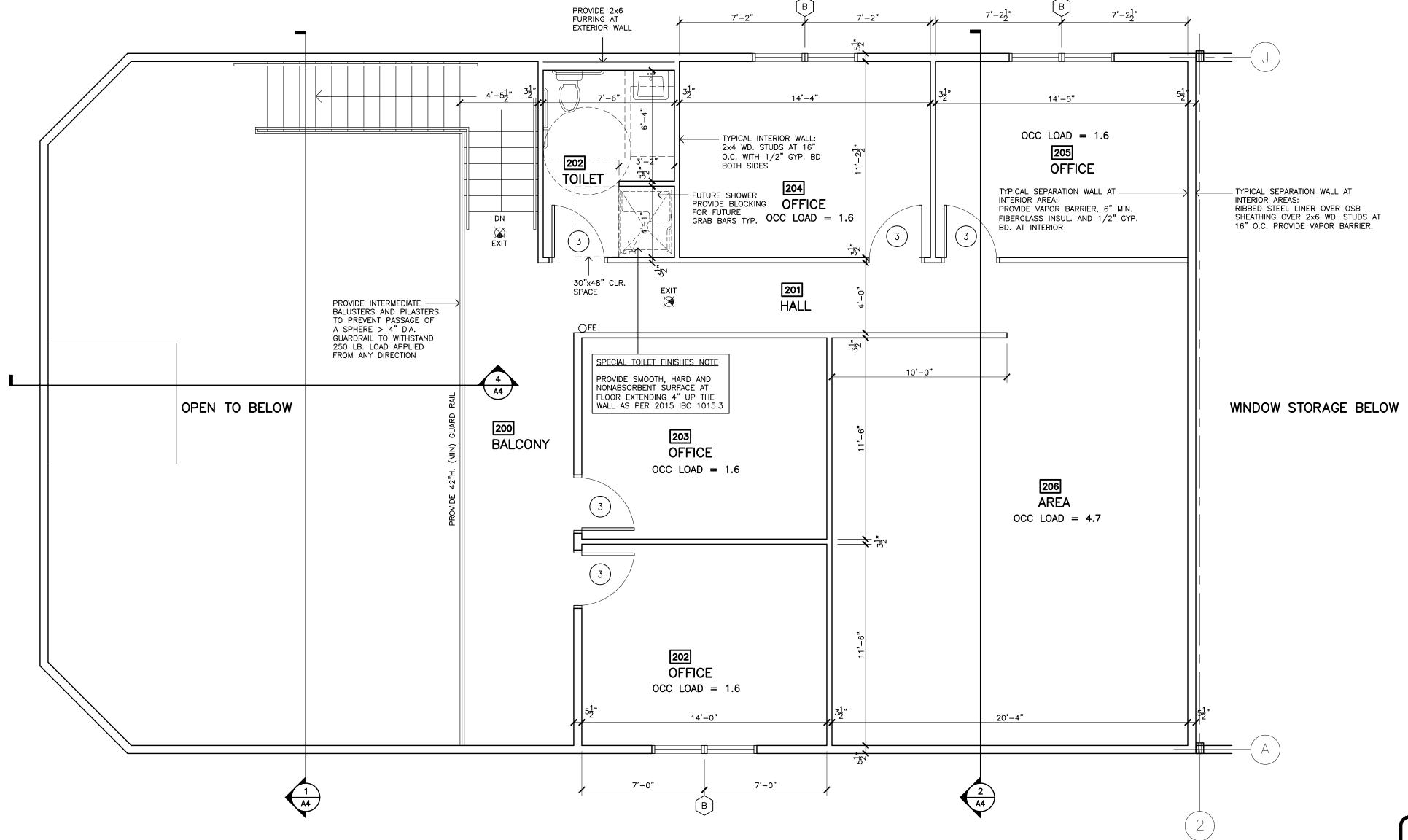




2 TYP. MOUNTING HGT. DET. N.T.S.



3 TYP. STAIR AND RAIL DETAILS



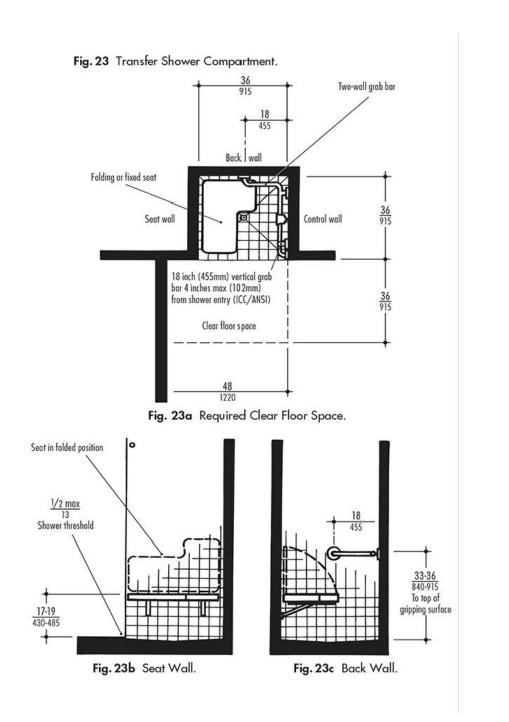
1 PROPOSED MEZZANINE PLAN

NORTH TOTAL OCCUPA

TOTAL OCCUPANCY LOAD = 12

FLOOR PLAN NOTES

- 1. ILLUMINATED EXIT LIGHTS COMPLY WITH 2015 IBC 1013. INCLUDE MEANS OF EGRESS/EMERGENCY LIGHTING PER 2015 IBC 1008.
- 2. PROVIDE FIRE EXTINGUISHERS TO COMPLY WITH 2015 IFC 906 AND MAINTAIN FE'S AS PER NFPA 10. VERIFY LOCATIONS WITH LOCAL FIRE DEPARTMENT REPRESENTATIVES. (FEO)
- 3. MAXIMUM ALLOWABLE QUANTITY OF FLAMMABLE AND HAZARDOUS MATERIALS THROUGHOUT BUILDING TO COMPLY WITH 2015 IBC TABLES 307.1(1), 307.1(2), 414.2.5(1), 414.2.5(2) AND 414.5.1.
- 4. INTERIOR WALL AND CEILING FINISHES TO BE CLASS C FINISHES IN ACCORDANCE WITH ASTME 84 OR UL723 (FLAME SPREAD INDEX 76-200, SMOKE DEVELOPED INDEX 0-450) INTERIOR FLOOR COVERINGS TO COMPLY WITH REQUIREMENTS OF DOC FF-1 "PILL TEST" OR ASTM 2859. MINIMUM CRITICAL RADIANT FLUX SHALL NOT BE LESS THAN CLASS II AS PER REQUIREMENTS OF DOC FF-1 "PILL TEST" OR ASTM 2859.
- 5. SEE SHEET A2 FOR DOOR AND WINDOW NOTES.
- 6. ALL NEW INTERIOR PARTITIONS TO EXTEND TO UNDERSIDE OF ROOF FRAMING MEMBERS.



4 TYP. SHWR. GRAB BAR DETAILS
N.T.S.

JAW	СНЕСКЕD	DATE JUNE 22, 2022	SCALE AS NOTED	SHEET	A 3

JIM WEBB, PE

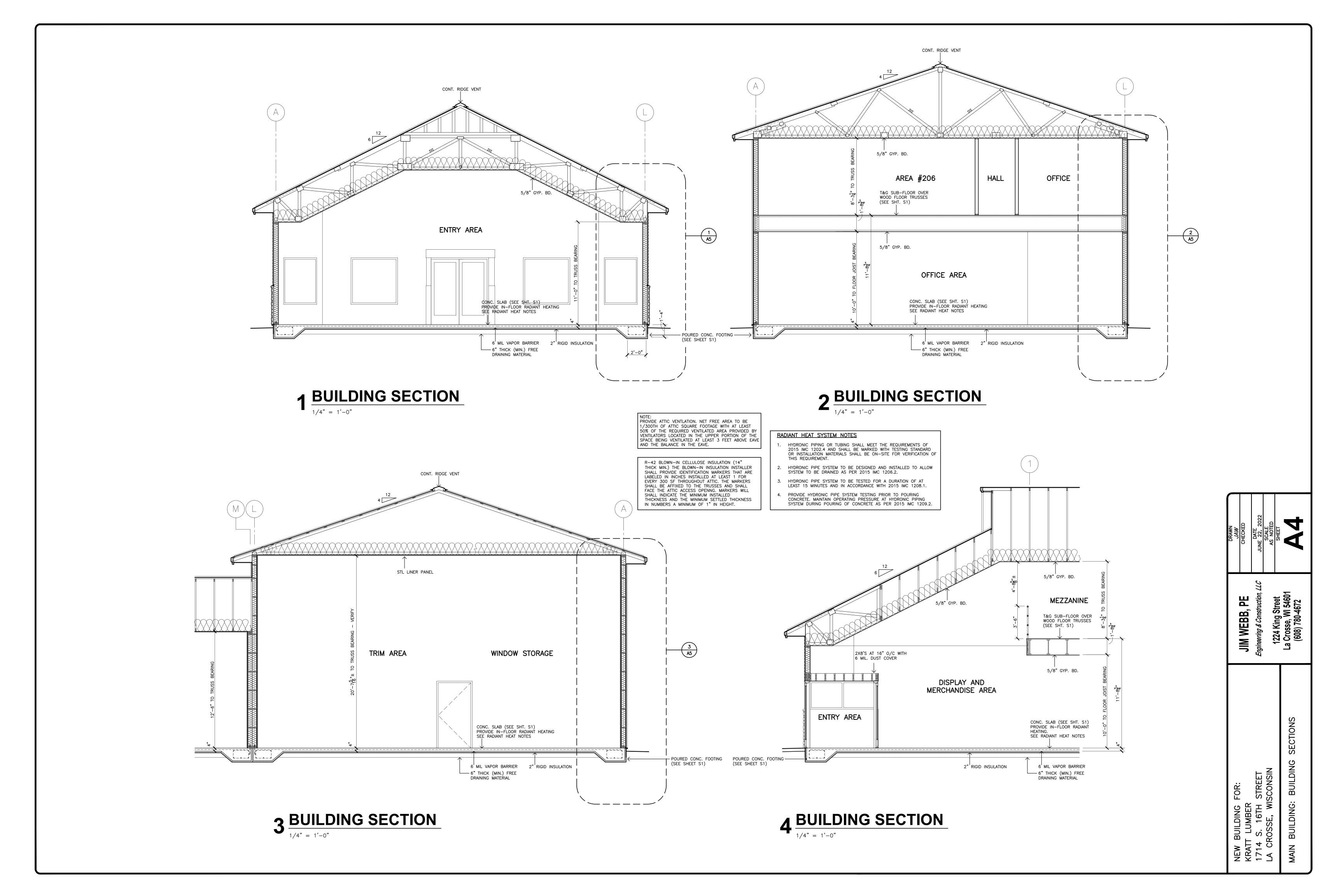
Engineering & Construction, LLC

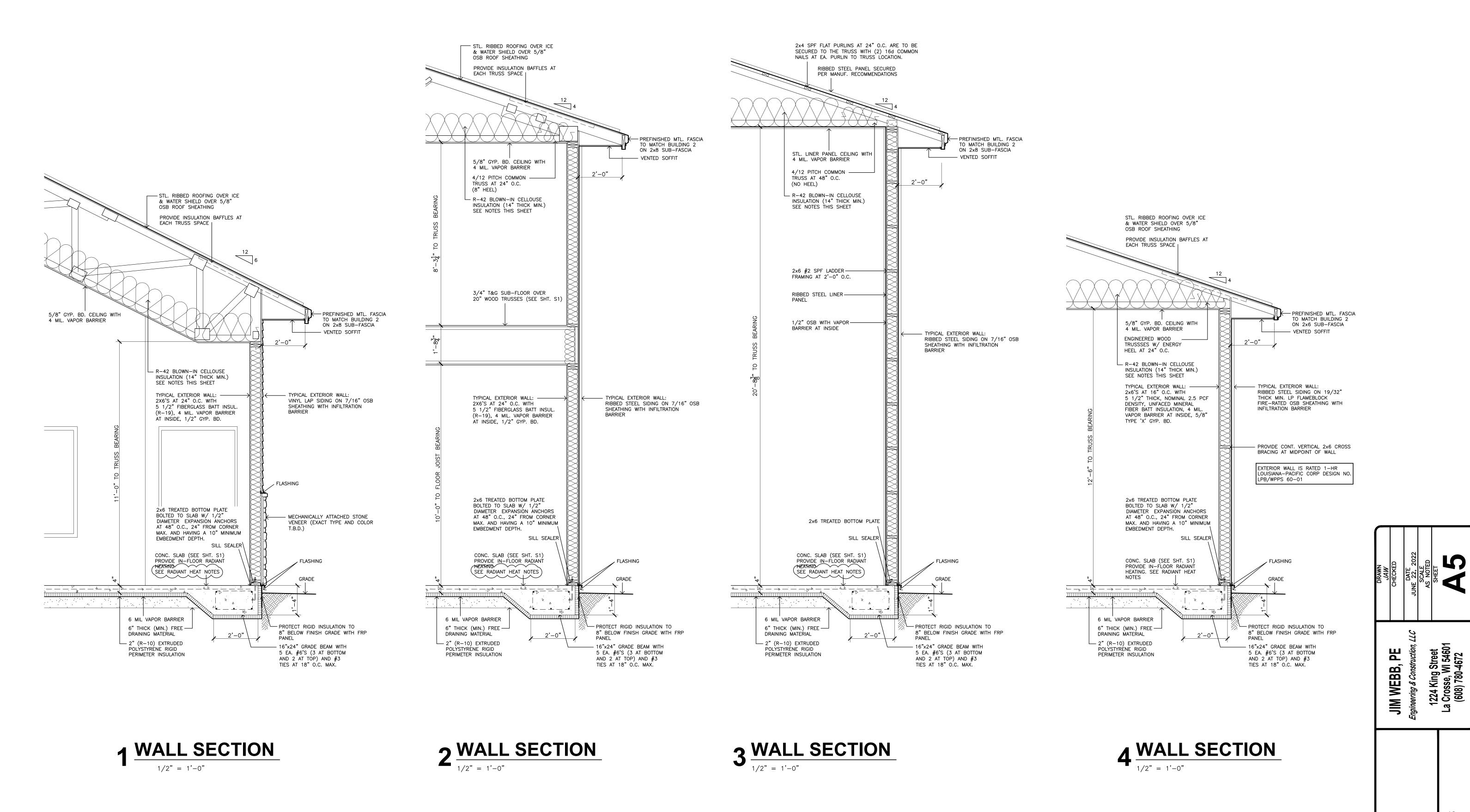
1224 King Street

La Crosse, WI 54601

NG: PROPOSED MEZZANINE PL

KRATT LUMBER 1714 S. 16TH STREET LA CROSSE, WISCONSIN





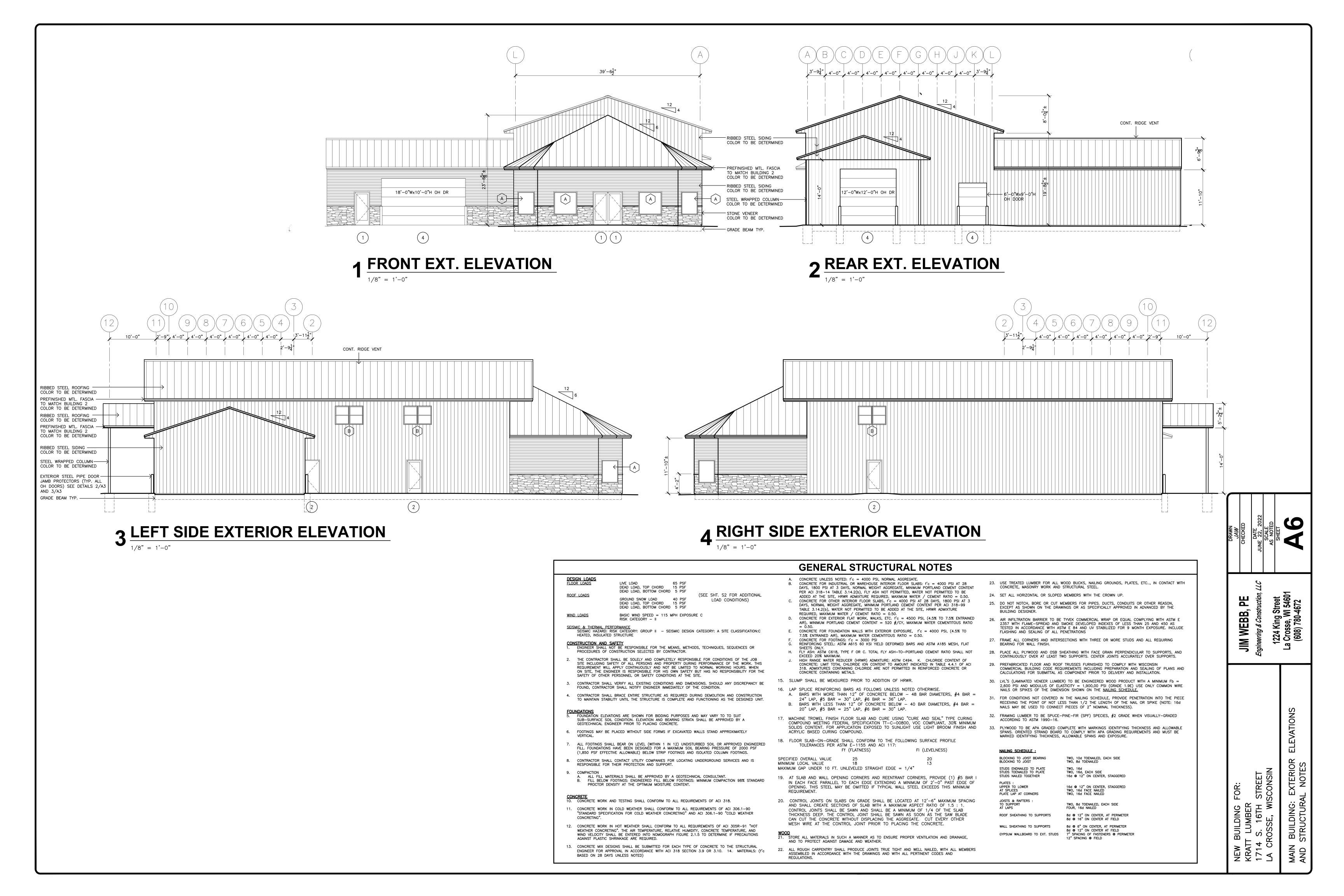
NOTE: PROVIDE ATTIC VENTLATION. NET FREE AREA TO BE 1/300TH OF ATTIC SQUARE FOOTAGE WITH AT LEAST 50% OF THE REQUIRED VENTILATED AREA PROVIDED BY VENTILATORS LOCATED IN THE UPPER PORTION OF THE SPACE BEING VENTILATED AT LEAST 3 FEET ABOVE EAVE AND THE BALANCE IN THE EAVE.

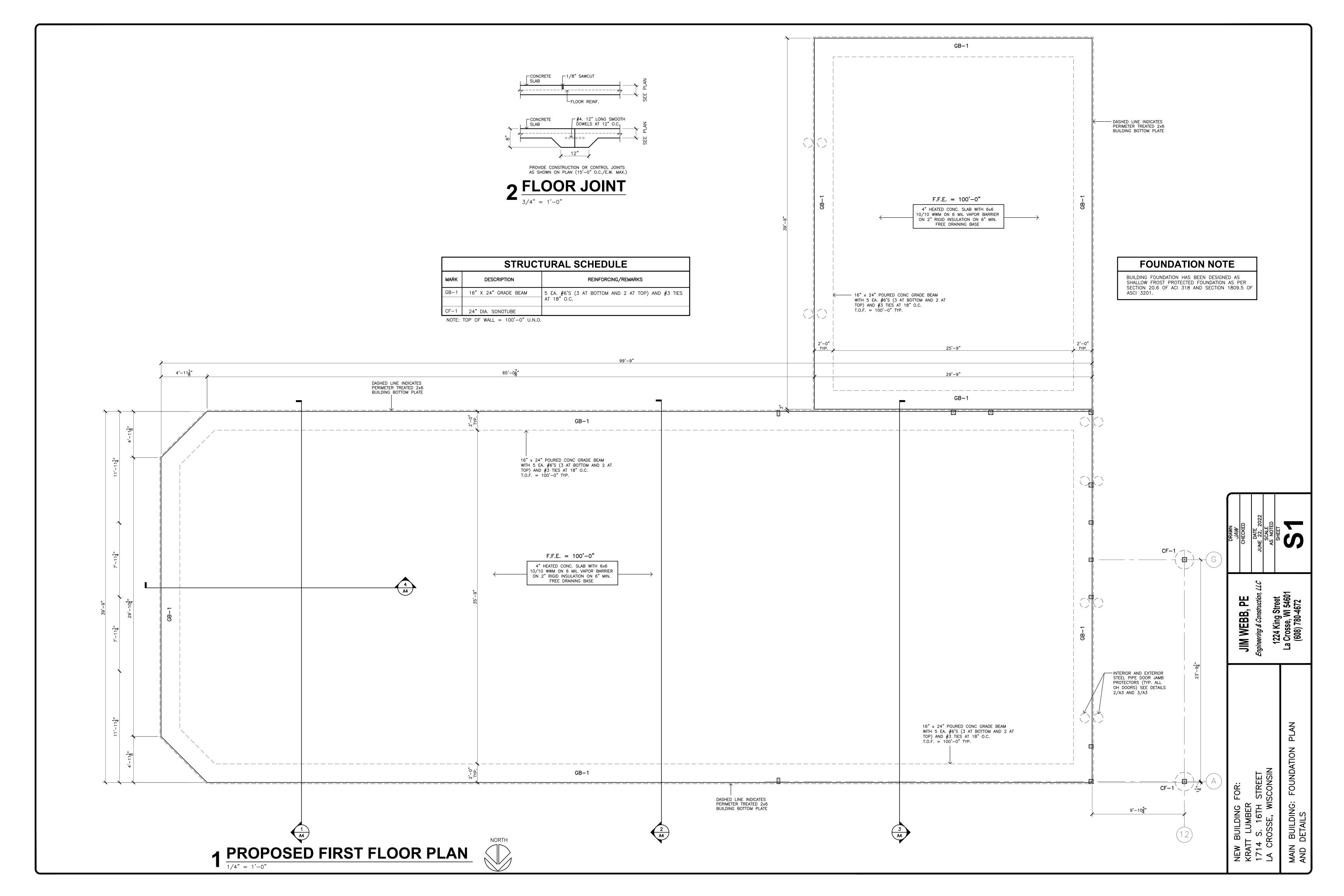
R-42 BLOWN-IN CELLULOSE INSULATION (14" THICK MIN.) THE BLOWN-IN INSULATION INSTALLER SHALL PROVIDE IDENTIFICATION MARKERS THAT ARE LABELED IN INCHES INSTALLED AT LEAST 1 FOR EVERY 300 SF THROUGHOUT ATTIC. THE MARKERS SHALL BE AFFIXED TO THE TRUSSES AND SHALL FACE THE ATTIC ACCESS OPENNG. MARKERS WILL SHALL INDICATE THE MINIMUM INSTALLED THICKNESS AND THE MINIMUM SETTLED THICKNESS IN NUMBERS A MINIMUM OF 1" IN HEIGHT.

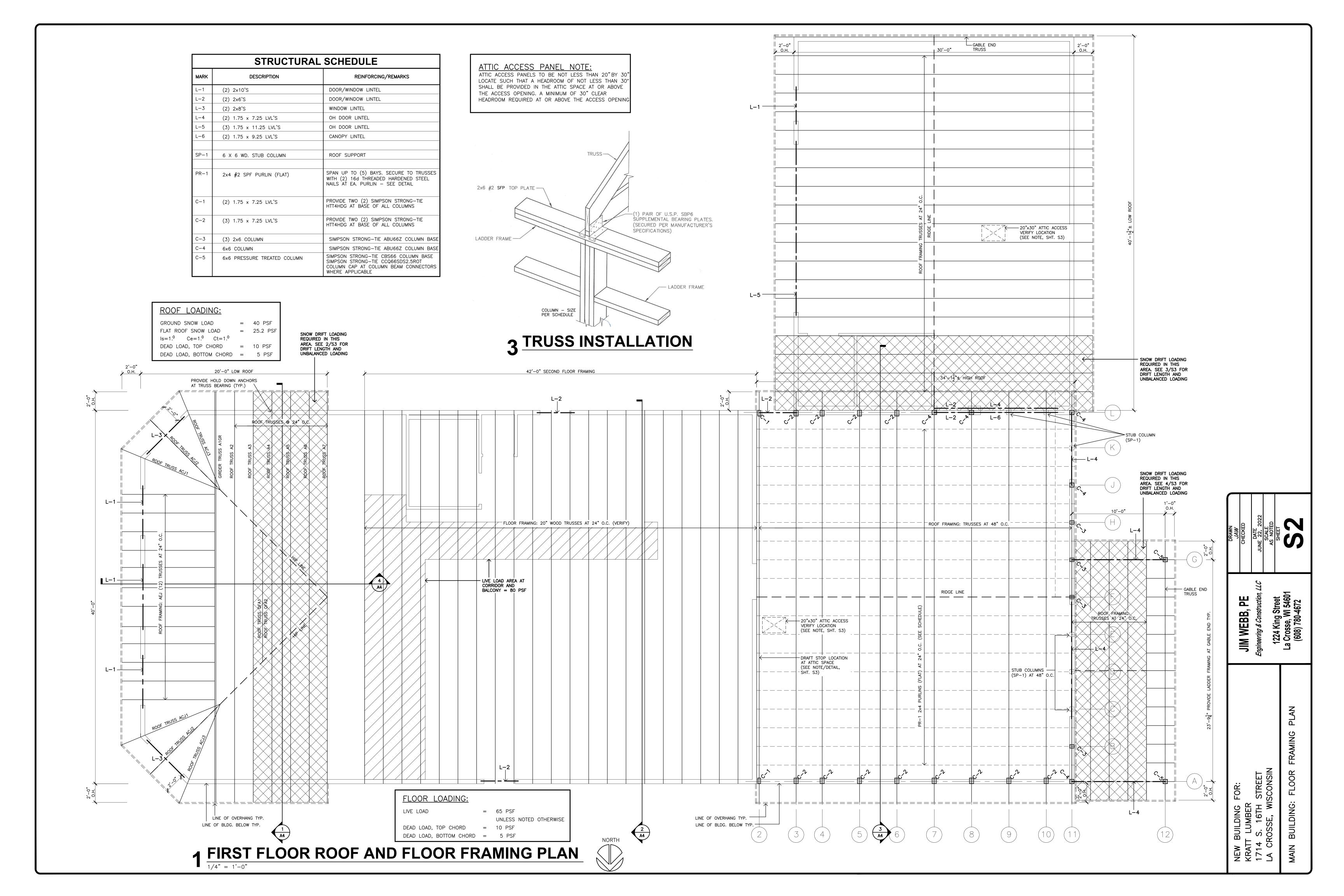
RADIANT HEAT SYSTEM NOTES

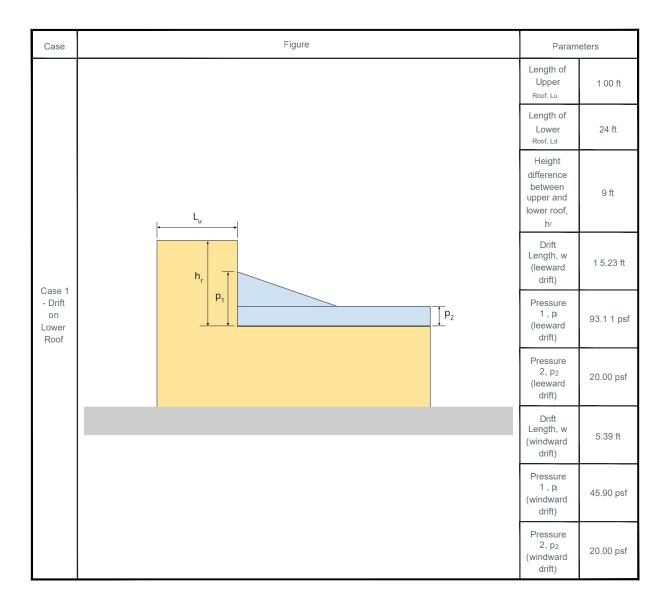
- HYDRONIC PIPING OR TUBING SHALL MEET THE REQUIREMENTS OF 2015 IMC 1202.4 AND SHALL BE MARKED WITH TESTING STANDARD OR INSTALLATION MATERIALS SHALL BE ON-SITE FOR VERIFICATION OF THIS REQUIREMENT.
- HYDRONIC PIPE SYSTEM TO BE DESIGNED AND INSTALLED TO ALLOW
- SYSTEM TO BE DRAINED AS PER 2015 IMC 1206.2. HYDRONIC PIPE SYSTEM TO BE TESTED FOR A DURATION OF AT LEAST 15 MINUTES AND IN ACCORDANCE WITH 2015 IMC 1208.1.
- PROVIDE HYDRONIC PIPE SYSTEM TESTING PRIOR TO POURING CONCRETE. MAINTAIN OPERATING PRESSURE AT HYDRONIC PIPING SYSTEM DURING POURING OF CONCRETE AS PER 2015 IMC 1209.2.

STREET NEW BUILDING F KRATT LUMBER 1714 S. 16TH S LA CROSSE, WIS

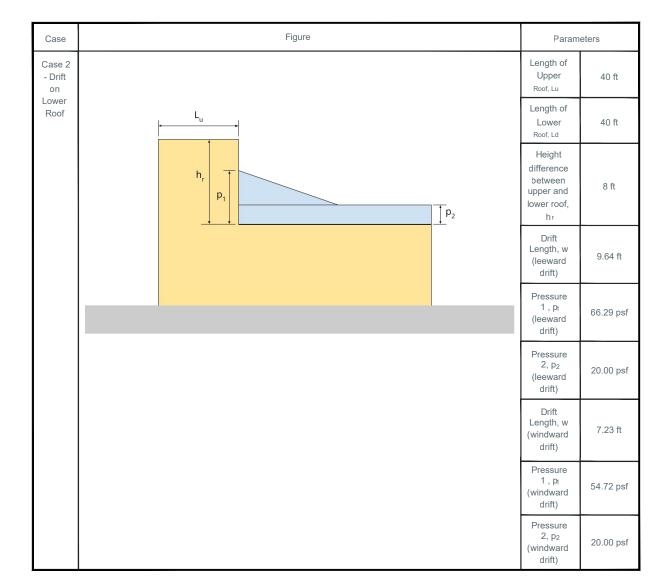




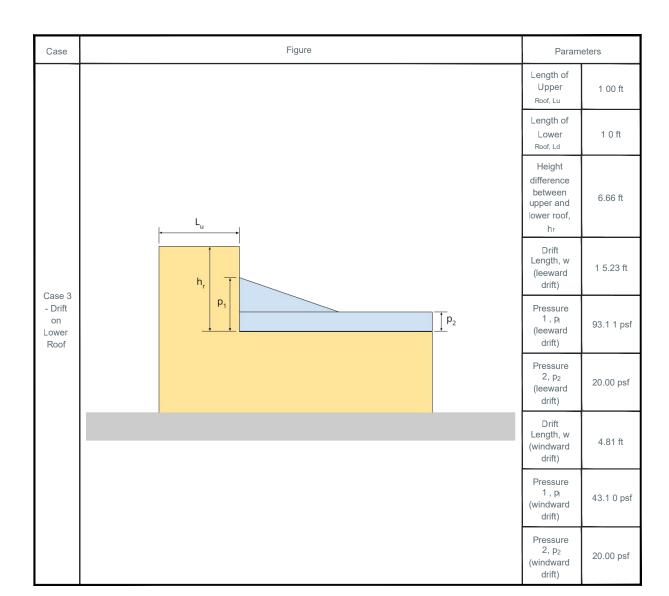




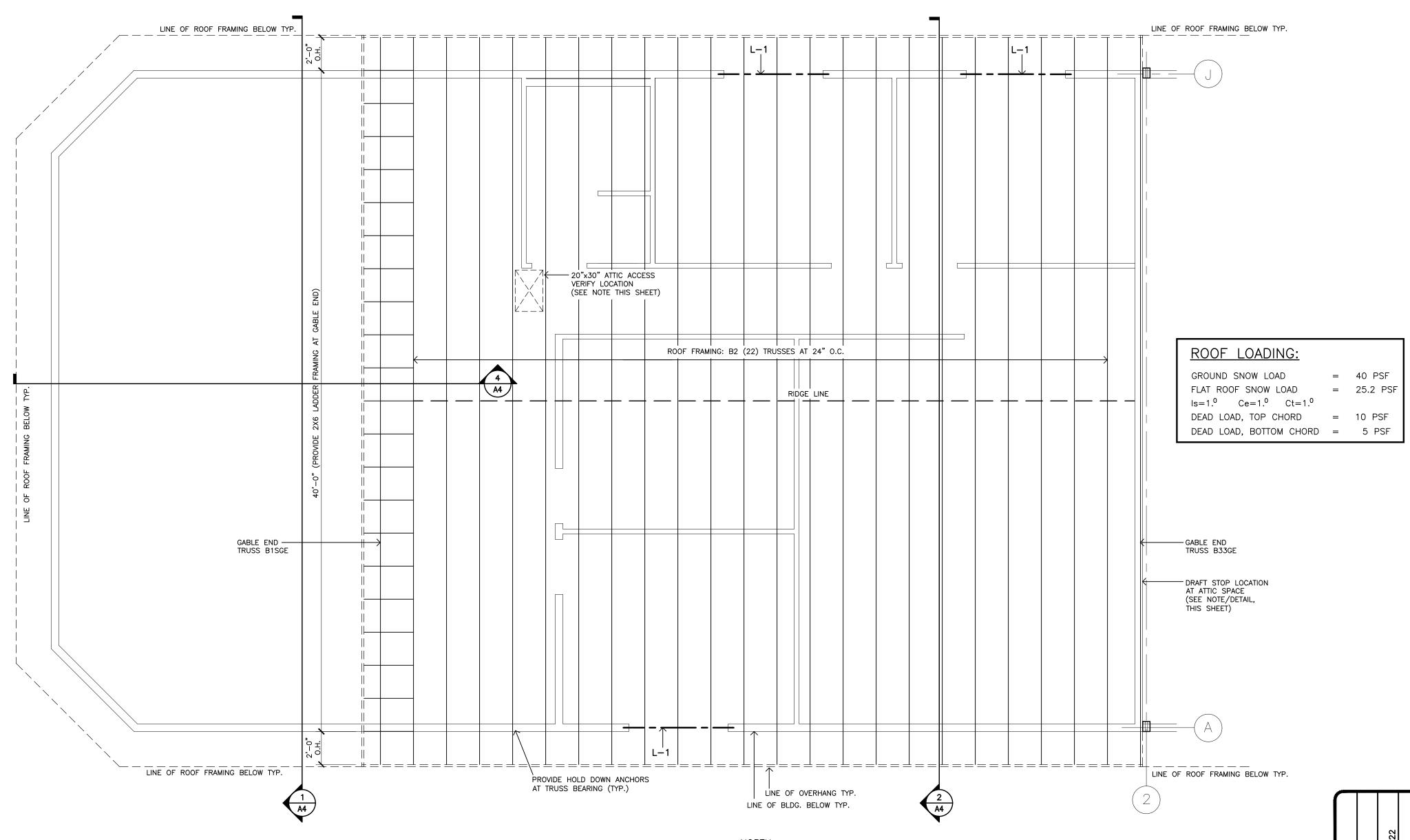
2 SNOW DRIFT AT HIGH ROOF/EAST WALL



3 SNOW DRIFT AT HIGH ROOF/LOW ROOF



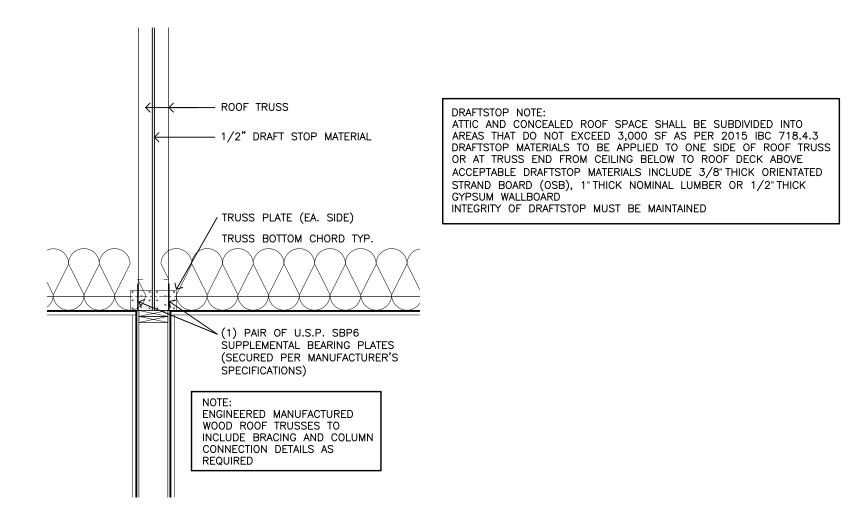
4 SNOW DRIFT AT HIGH ROOF/CANOPY ROOF



SECOND FLOOR ROOF FRAMING PLAN

STRUCTURAL SCHEDULE				
MARK	DESCRIPTION	REINFORCING/REMARKS		
L-1	(2) 2x10'S	DOOR/WINDOW LINTEL		

ATTIC ACCESS PANEL NOTE: ATTIC ACCESS PANELS TO BE NOT LESS THAN 20"BY 30" LOCATE SUCH THAT A HEADROOM OF NOT LESS THAN 30" SHALL BE PROVIDED IN THE ATTIC SPACE AT OR ABOVE THE ACCESS OPENING. A MINIMUM OF 30" CLEAR HEADROOM REQUIRED AT OR ABOVE THE ACCESS OPENING



5 DRAFTSTOP DETAIL

JIM WEBB, PE

Wind Load Report

Data	2. Parameters & Coefficients		
Gable	Topographic Factor (Kzt):	1.0	
115 mph	Directionality Factor (Kd):	.85	
С	Roof Angle (θ):	18.43 deg	
nclosed	Mean Roof Height (h):	23.33 ft.	
40 ft.	Ridge Height (hr):	26.67 ft.	
76 ft.	Pos. Internal Pressure (+GCpi):	+0.18	
20 ft.	Neg. Internal Pressure (-GCpi):	-0.18	
0 ft.	Velocity Pressure Exp. Coeff. (Kh	n): 0.93 @ z	
4 /12	Velocity Pressure (qh):	26.81 psf	
2 ft.	End Zone Width (a):	3.00 ft.	
1 ft.	Zone 2/2E Dist.:	20.00 ft.	
	115 mph C nclosed 40 ft. 76 ft. 20 ft. 0 ft. 4 /12 2 ft.	Gable 115 mph C Roof Angle (θ): Mean Roof Height (h): 40 ft. Ridge Height (hr): 76 ft. Pos. Internal Pressure (+GCpi): Neg. Internal Pressure (-GCpi): Velocity Pressure Exp. Coeff. (Kh. 4/12 2 ft. End Zone Width (a):	

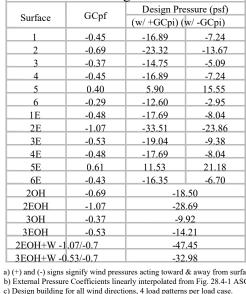
3. Design Assumptions and Notes 4. Design Loads

Code Standard:	ASCE 7-10	Top Chord Dead Load:	10 psf
Geometry: I	Regular-Shaped Bldg.	Bottom Chord Dead Load:	5 psf
Height Class:	Low-Rise Building	Truss/Rafter Spacing:	24 in. o/c
Matag			

4. Design Wind Pressures: MWFRS Envelope Procedure

a .c	GCpf	Design Pre	essure (psf)
Surface	ССРІ	(w/ +GCpi) (w/ -GCpi)
11	0.52	9.02	18.67
2	-0.69	-23.32	-13.67
3	-0.47	-17.39	-7.74
4	-0.42	-15.96	-6.31
1E	0.78	16.09	25.74
2E	-1.07	-33.51	-23.86
3E	-0.67	-22.88	-13.23
4E	-0.62	-21.40	-11.75
2OH	-0.69	-18.50	
2EOH -1.07		-28.69	
3ОН	-0.47	-12	56
3EOH -0.67		-18.05	
2OH+W	-0.69/-0.7	-36	.67
2EOH+W -	1.07/-0.7	-46	.85

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces. b) External Pressure Coefficients linearly interpolated from Fig. 28.4-1 ASCE 7-10. c) Design building for all wind directions, 4 load patterns per load case.
d) Total horizontal shear shall not be less than that by neglecting roof wind forces. e) Min. wind load for enclosed or partially enclosed bldg.: 16 psf wall, 8 psf roof. f) Design pressures are for strength design, multiply by 0.6 for ASD.

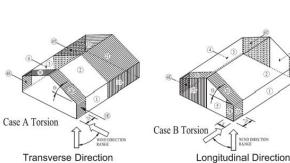


Load Case B: Longitudinal Direction

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces. b) External Pressure Coefficients linearly interpolated from Fig. 28.4-1 ASCE 7-10. c) Design building for all wind directions, 4 load patterns per load case. d) Total horizontal shear shall not be less than that by neglecting roof wind forces e) Min. wind load for enclosed or partially enclosed bldg.: 16 psf wall, 8 psf roof.
f) Design pressures are for strength design, multiply by 0.6 for ASD.

Torsional Load Cases					
Design Pressure (nsf)					
Surface L	oad Case	GCpf	(w/+GCpi)		
1T	A	-	2.25	4.67	
2T	A	_	-5.83	-3.42	
3T	A	_	-4.35	-1.93	
4T	A		-3.99	-1.58	
5T	В	-	1.47	3.89	
6T	В	_	-3.15	-0.74	

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces.
b) Pressures designated with a "T" are 25% of full design wind pressures.
c) Torsional loading shall apply to all 8 load patterns using the figures shown.



d) Design pressures are for strength design, multiply by 0.6 for ASD. e) Torsional Design Exceptions: One story bldg. with h \leq 30 ft, Two stories or less framed with light frame construction,

5. Wind Load Calculations

1.) Lateral Loads - Transverse Direction:

Lateral Loads on Roof Diaphragm with Positive Internal Pressure

LEEWARD ROOF	(3EOH)(OH _e)(tai	nθ) = 7.2 plf	(3OH)(OH _e)(tanθ) = 5.0 plf	
LEEWAR	(3EOH)(^W / ₂)(tanθ) = 72.2 plf	$(3E)(\frac{W}{2})(\tan\theta) = 91.5 \text{ plf}$	(3)(^W ₂)(tanθ) = 69.5 plf	(3OH)(₹)(tanθ) = 50.2 p(f
u.	(2EOH)(∰)(tanθ) =114.7 plf	$(2E)(\frac{W}{2})(\tan\theta) = 134.1 \text{ plf}$	(2)(₩/2)(tanθ) = 93.3 plf	$(2OH)(\frac{W}{2})(\tan\theta) = 74.0 \text{ plf}$
WINWARD	(2EOH+W)(OH _e)(t	anθ) = 18.7 plf	(20H+W)(OH _e)(tanθ) = 14.7 plf	
WALLS		(4E)(h _e /2) = 128.4 plf	(4)(h₀/2) = 95.8 plf	
4		(1E)(h _e /2) = 96.5 plf	(1)(h₀/2) = 54.1 plf	
				orași a
Ī	A			A. I
	-	— 2a = 6.00 ft. ——	L - 2a = _{70.00 ft} .	-

a) (-) signs signify wind lateral forces acting opposite to the direction of the arrows shown. b) Strength design values multiplied by 0.6 to obtain ASD values.

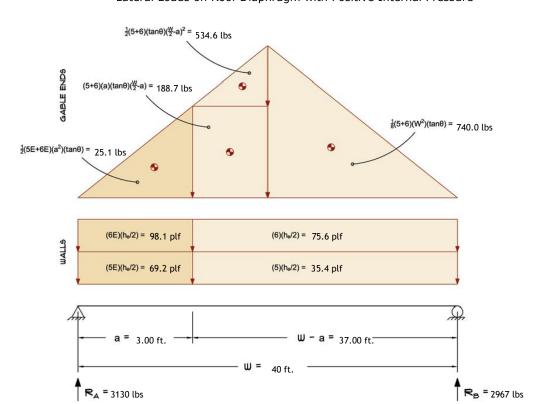
 $R_1 = 4686 \text{ lbs}$

	V	Vind Base	e Shear (ASD)			
	Load	Case A: T	ransverse Directi	on		
Load Case	Walls (lbs)	Roof (lbs)	Roof Overhangs (lbs) 7	otal Lateral Load (lbs) R	1 (lbs)	R2 (lbs)
Positive Internal Pressure	11842	-1918	-832	9093	4686	4407
Negative Internal Pressure	11842	-1918	-832	9093	4686	4407
Roof Pressure $= 0$	11842	0	0	11842	6128	5714
Min. Pressures (8 psf, 16 psf)	7296	2432	314	10042	5021	5021

a) Bottom half of wall neglected in tributary area calculations. b) Strength design values multiplied by 0.6 to obtain ASD values.

2.) Lateral Loads - Longitudinal Direction:

Lateral Loads on Roof Diaphragm with Positive Internal Pressure

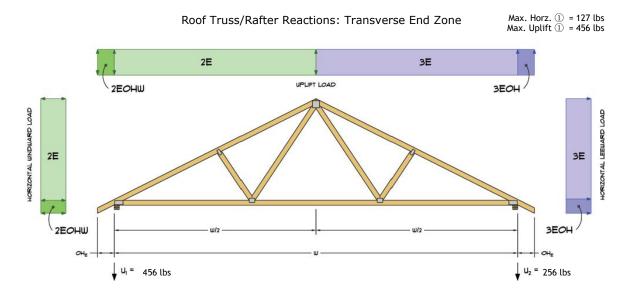


a) (-) signs signify wind lateral forces acting opposite to the direction of the arrows shown. b) Strength design values multiplied by 0.6 to obtain ASD values. c) Where the length of building (L) exceeds 4X the mean roof height (h), wind drag forces should additionally be considered.

a) Bottom half of wall neglected in tributary area calculations.
 b) Strength design values multiplied by 0.6 to obtain ASD values.

Wind Base Shear (ASD)						
	Load Ca	se B: Longitu	ıdinal Dire	ction		
Load Case	Walls (lbs)	Gable Ends (lbs)	Roof (lbs) To	otal Lateral Load (lbs) RA	(lbs)	RB (lbs)
Positive Internal Pressure	4609	1488	0	6097	3130	2967
Negative Internal Pressure	4609	1488	0	6097	3130	2967
Roof Pressure = 0	4609	1488	0	6097	3130	2967
Min. Pressures (8 psf, 16 psf)	3840	1280	0	5120	2560	2560

3.) Roof Truss Reactions:



a) Strength design values multiplied by 0.6 to obtain ASD values. b) Windward loads may be positive or negative depending on pitch of roof.

 $R_2 = 4407 \text{ lbs}$

	w/ Posi	itive Internal P	ressure			
Load Case	Horizontal Load (lbs)	Gross Uplift (lbs) N	et Uplift (lbs) U1	(lbs)	U2 (lbs)	
Transverse Int. Zone	67	1095	299	215	83	
Transverse End Zone	108	1509	713	456	256	
Longitudinal Int. Zone	75	982	185	155	30	
Longitudinal End Zone 127 1364 568 389 179						

d) Loads based on truss spacing calculated at 24" o/c.
e) Negative values for horizontal load indicate load acting in windward direction (tranverse load cases).

f) Negative values for uplift indicate net downward force (zero uplift).

Wind Load Report

2. Parameters & Coefficients Topographic Factor (Kzt): Roof Type: Gable Wind Speed (ult): 115 mph Directionality Factor (Kd): Exposure Category: Roof Angle (θ): 18.43 deg. Mean Roof Height (h): Enclosure Class: 14.50 ft. Building Width (W): Ridge Height (hr): 17.00 ft. Building Length (L): 40 ft. Pos. Internal Pressure (+GCpi): +0.18 Eave Height (he): 12 ft. Neg. Internal Pressure (-GCpi): -0.18 Foundation Height (hf): 0 ft. Velocity Pressure Exp. Coeff. (Kh): 0.85 @ z=h 4 /12 Velocity Pressure (qh): 24.43 psf Roof Pitch: Eave Overhang (OHe): 2 ft. End Zone Width (a): 3.00 ft. Gable Overhang (OHg): Zone 2/2E Dist.: 15.00 ft.

3. Design Assumptions and Notes 4. Design Loads

Code Standard	: ASCE 7-10	Top Chord Dead Load:	10 psf
Geometry:	Regular-Shaped Bldg.	Bottom Chord Dead Load:	5 psf
Height Class:	Low-Rise Building	Truss/Rafter Spacing: 24	in. o/c
NT. 4			

4. Design Wind Pressures: MWFRS Envelope Procedure

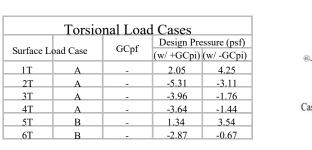
Loau C	ase A. IIa	ansverse D Design Pre	
Surface	GCpf	(w/+GCpi) (
1	0.52	8.22	17.01
2	-0.69	-21.25	-12.46
3	-0.47	-15.84	-7.05
4	-0.42	-14.54	-5.75
1E	0.78	14.66	23.46
2E	-1.07	-30.54	-21.74
3E	-0.67	-20.85	-12.05
4E	-0.62	-19.50	-10.70
20H	-0.69	-16	.86
2EOH	-1.07	-26	.14
30H	-0.47	-11	.45
3ЕОН	-0.67	-16	.45
2OH+W	-0.69/-0.7	-33	.96
2EOH+W -	1.07/-0.7	-43	.24

1. Site & Building Data

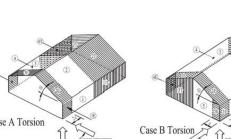
a) (+) and (-) signs signify wind pressures acting toward & away from surfaces. b) External Pressure Coefficients linearly interpolated from Fig. 28.4-1 ASCE 7-10. c) Design building for all wind directions, 4 load patterns per load case.
d) Total horizontal shear shall not be less than that by neglecting roof wind forces e) Min. wind load for enclosed or partially enclosed bldg.: 16 psf wall, 8 psf roof. f) Design pressures are for strength design, multiply by 0.6 for ASD.

Load Case B: Longitudinal Direction GCpf Design Pressure (psf) (w/+GCpi) (w/-GCpi)1 -0.45 -15.39 -6.60 2 -0.69 -21.25 -12.46 3 -0.37 -13.44 -4.64 4 -0.45 -15.39 -6.60 5 0.40 5.37 14.17 6 -0.29 -11.48 -2.69 1E -0.48 -16.12 -7.33 2E -1.07 -30.54 -21.74 3E -0.53 -17.34 -8.55 4E -0.48 -16.12 -7.33 5E 0.61 10.50 19.30 6E -0.43 -14.90 -6.11 2OH -0.69 -16.86 2EOH -1.07 -26.14 3OH -0.37 -9.04 3EOH -0.53 -12.95 -43.24 2EOH+W -1.07/-0.7 3EOH+W -0.53/-0.7 -30.05

a) (+) and (-) signs signify wind pressures acting toward & away from surfaces. b) External Pressure Coefficients linearly interpolated from Fig. 28.4-1 ASCE 7-10. c) Design building for all wind directions, 4 load patterns per load case. d) Total horizontal shear shall not be less than that by neglecting roof wind forces e) Min. wind load for enclosed or partially enclosed bldg.: 16 psf wall, 8 psf roof.
f) Design pressures are for strength design, multiply by 0.6 for ASD.



a) (+) and (-) signs signify wind pressures acting toward & away from surfaces.
b) Pressures designated with a "T" are 25% of full design wind pressures.
c) Torsional loading shall apply to all 8 load patterns using the figures shown. d) Design pressures are for strength design, multiply by 0.6 for ASD. e) Torsional Design Exceptions: One story bldg. with h ≤ 30 ft, Two stories or less framed with light frame construction, Two stories or less with flexible diaphragms.



Transverse Direction

2.) Lateral Loads - Longitudinal Direction:

5. Wind Load Calculations 1.) Lateral Loads - Transverse Direction:

Lateral Loads on Roof Diaphragm with Positive Internal Pressure

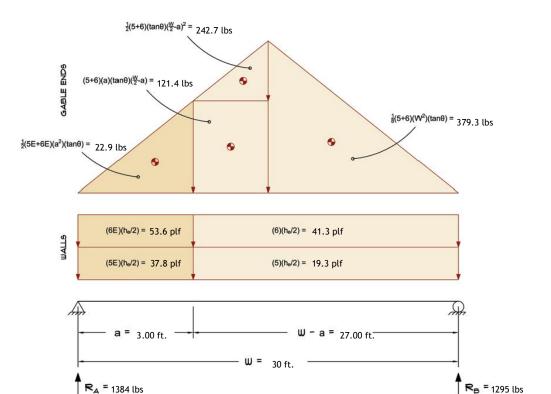
3	(3EOH)(OH _e)(tanθ) = 6.6 plf		(3OH)(OH _e)(tanθ) = 4.6 plf				
LEEWARD ROOF	(3EOH)(^W ₂)(tanθ) = 49.3 plf	(3E)(^W / ₂)(tanθ) = 62.5 plf	$(3)(\frac{W}{2})(\tan\theta) = 47.5 \text{ plf}$	(30H)(^W / ₂)(tanθ) = 34.3 p			
b 1	(2EOH)(\frac{W}{2})(\tan\theta) = 78.4 plf	(2E)(^W / ₂)(tanθ) = 91.6 plf	(2)(^W / ₂)(tanθ) = 63.8 plf	(20H)(^W / ₂)(tanθ) = 50.6 p			
WINWARD ROOF	(2EOH+W)(OH ₀)(tanθ) = 17.3 plf		(2OH+W)(OH _e)(tanθ) = 13.6 plf				
3 [
ALL9	•	(4E)(h₀/2) = 70.2 plf	$(4)(h_0/2) = 52.4 \text{ plf}$				
WALLS		$(4E)(h_0/2) = 70.2 \text{ plf}$ $(1E)(h_0/2) = 52.8 \text{ plf}$	$(4)(h_0/2) = 52.4 \text{ plf}$ $(1)(h_0/2) = 29.6 \text{ plf}$				
WALLS	A)	<u> </u>		A.			
MALLS		<u> </u>		<i>m</i>			

a) (-) signs signify wind lateral forces acting opposite to the direction of the arrows shown. b) Strength design values multiplied by 0.6 to obtain ASD values.

 $R_1 = 1241 \text{ lbs}$

	V	Vind Base	e Shear (ASD)			
	Load	Case A: T	ransverse Directi	on		
Load Case	Walls (lbs)	Roof (lbs)	Roof Overhangs (lbs) T	otal Lateral Load (lbs) I	R1 (lbs)	R2 (lbs)
Positive Internal Pressure	3524	-726	-435	2362	1241	1121
Negative Internal Pressure	3524	-726	-435	2362	1241	1121
Roof Pressure = 0	3524	0	0	3524	1867	1657
Min. Pressures (8 psf, 16 psf)	2304	960	182	3446	1723	1723

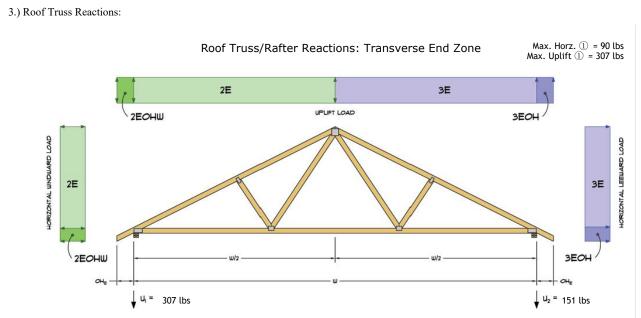
Lateral Loads on Roof Diaphragm with Positive Internal Pressure



a) (-) signs signify wind lateral forces acting opposite to the direction of the arrows shown. b) Strength design values multiplied by 0.6 to obtain ASD values. c) Where the length of building (L) exceeds 4X the mean roof height (h), wind drag forces should additionally be considered.

Wind Base Shear (ASD)								
Load Case B: Longitudinal Direction								
Load Case	Walls (lbs) Gable Ends (lbs) Roof (lbs) Total Lateral Load (lbs) RA (lbs)			RB (lbs)				
Positive Internal Pressure	1913	766	00	2679	1384	1295		
Negative Internal Pressure	1913	766	0	2679	1384	1295		
Roof Pressure = 0	1913	766	00	2679	1384	1295		
Min. Pressures (8 psf, 16 psf)	1728	720	0	2448	1224	1224		
	1728		0					

b) Strength design values multiplied by 0.6 to obtain ASD values.



a) Strength design values multiplied by 0.6 to obtain ASD values.

 $R_2 = 1121 \text{ lbs}$

Roof Truss/Rafter Reactions (ASD) w/ Positive Internal Pressure							
167	136	30					
458	307	151					
76	83	-7					
346	249	97					
	Net Uplift (lbs) U1 167 458 76	Net Uplift (lbs) U1 (lbs) 167					

d) Loads based on truss spacing calculated at 24" o/c.
e) Negative values for horizontal load indicate load acting in windward direction (tranverse load cases). f) Negative values for uplift indicate net downward force (zero uplift).

PE

JIM WEBB,